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DEVELOPMENT OF THE RADIATIVE
TRANSFER PORTION OF A 1-D
PHOTOCHEMICAL DIFFUSIVE STRATOSPHERIC MODEL

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This report summarizes the development and implementation of an advanced state-of-the-art computer code, the Chlorine Model Study Program (CMSP), which models the trace gas composition of the atmosphere from the surface to 80 km employing over sixty relevant chemical reactions and parameterizing vertical transport by a selected eddy diffusion profile.			
A significant feature is the computation of solar flux available for photolysis by a multiple scattering atmosphere including the effect of surface reflection.			

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20. ABSTRACT (cont)

→ Program documentation includes a complete listing of the code, a detailed flow chart, and several test case results in addition to a detailed program description and users guide. ↗

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1. Introduction

This report summarizes the implementation and further development of the Chlorine Model Study Program (CMSP) performed by Environmental Research & Technology, Inc. (ERT) under the sponsorship of the Electronic Systems Division, U.S.A.F. Systems Command, Hanscom AFB, Massachusetts.

The CMSP is an advanced state-of-the-art computer code which models the trace gas composition of the atmosphere from the surface to 80 km employing over sixty chemical reactions in addition to allowing for vertical transport parameterized by a selected set of eddy diffusion coefficients. In its original formulation, the model only computed photolysis for the one-way passage of solar radiation through the atmosphere (absorption only). In the present version the effects of multiple scattering and surface reflection have been incorporated into the radiative transfer section of the program thus allowing for more realistic simulation of the effects of injected pollutants into the atmosphere.

The text which follows constitutes a basic program description, documentation, and users guide. Section 2 discusses the theoretical basis of the model including the governing continuity and flux equations for the steady-state version in addition to the chemical system adopted. Section 3 provides a description of the development of the radiative transfer section including the technique employed to perform the multiple scattering calculation and some representative results (Appendix C). Section 4 constitutes a comprehensive program description utilizing a complete program listing (Appendix A) and a flow chart (Appendix B) to aid in the exposition of the detailed calculation. Finally, Section 5 is included as a basic users guide containing instructions for program implementation and execution.

2. Theoretical Basis

2.1 Governing Model Equations

The CMSP program is a 1-dimensional (vertical dependence), steady state (no time dependence) mathematical model of the trace gas chemical composition of the atmosphere from the surface to 80 km. Specifically, the species dealt with include odd oxygen (O, O_3), odd hydrogen (H, OH, HO_2, H_2O_2), odd nitrogen (NO, NO_2, HNO_3), and odd chlorine (Cl, HCl, ClO). Physical processes which determine the local abundances of these and other minor species include chemical kinetics, photochemistry, and turbulent transport. Radiative transfer is indirectly involved since it determines the number of photons available for photodissociation. (See Section 3).

The model is similar to those of Wofsy, McElroy and Sze (1975) and Sze and McElroy (1975) with several modifications. The governing continuity and diffusion equations are:

$$\frac{\partial \phi_i}{\partial Z} = P_i - L_i N f_i \quad (2-1)$$

and
$$\frac{\partial f_i}{\partial Z} = -\phi_i / KN \quad (2-2)$$

where ϕ_i is the vertical flux ($\text{cm}^{-2} \text{sec}^{-1}$), N the atmospheric total number density (cm^{-3}), K the eddy coefficients ($\text{cm}^2 \text{sec}^{-1}$) and P_i and L_i are respectively the local production ($\text{cm}^{-3} \text{sec}^{-1}$) and loss frequency (sec^{-1}), i denotes the i^{th} species, and f_i is the mixing ratio (v/v). Distinctions between long lived species (e.g. N_2O, CH_4, CF_2Cl_2) and short lived species (e.g. Cl, OH, NO) lead to enormous simplification in calculations.

For instance, the time constants for apportionment of ClX among various forms of odd chlorine ($Cl, ClO, HCl, ClOO, Cl_2$) are rapid compared to the time constant for vertical motion. Densities of individual ClX species

can be calculated with the equations of photochemical equilibrium, i.e.

$$P_i - L_i N f_i = 0 \text{ for each species} \quad (2-3)$$

Likewise, photochemical equilibrium can be applied to the short lived hydrogen species (H, OH, HO₂, H₂O₂), to NO_x (NO, NO₂, HNO₃), to O(³P) and to O(¹D). On the contrary, vertical flow is allowed for long-lived species such as CH₄, N₂O, CO, CF₂Cl₂, CFCI₃, and O₃ (below 30 km) and the total family concentrations for HO_x, NO_x, and Cl_x. In this case, equations (2-1, 2-2) must be solved simultaneously.

Equations (2-1) and (2-2) are coupled differential equations with two point boundary conditions. They are usually solved by using the conventional finite difference method or the shooting method. However, more efficient schemes have recently been developed to improve computational efficiency. The numerical approach utilized is based on a Riccati scheme developed by Sze (1973) and subsequently applied to investigations relating to the Venus (Sze and McElroy, 1975) and Earth's atmosphere. In essence, the Riccati scheme transforms (2-1) and (2-2) into a non-coupled system with a one point boundary condition. This technique greatly reduces the computational complexity of the problem and facilitates numerical solutions of differential equations of the type described here.

In the one-dimensional model, the crucial transport parameter is the vertical eddy diffusion coefficient K_{zz}. In the current model three options exist to vary the assumed K_{zz} profile to simulate measured data and perform sensitivity analyses. (See Section 4.3.2). The neutral atmosphere used in the calculation is summarized in Table 2-1 (a particular eddy diffusion profile is demonstrated). Photolysis processes for aeronomically significant molecules are summarized in Table 2-2. Computations of photodissociation rates (or J-values) are accomplished (See Section 3-1)

TABLE 2-1

ATMOSPHERIC MODEL

Altitude (km)	Eddy Diffusion Coefficient ($\text{cm}^2 \text{sec}^{-1}$)	Number Density (cm^{-3})	Temperature (°K)
0	1.4000E 05	2.4110E 19	304.58
2	1.4000E 05	2.1050E 19	289.56
4	1.4000E 05	1.6510E 19	277.87
6	1.4000E 05	1.3400E 19	266.52
8	1.4000E 05	1.0880E 19	252.41
10	4.2000E 04	8.7330E 18	238.39
11	4.2000E 04	6.9130E 18	224.42
14	4.2000E 04	5.9310E 18	210.50
16	3.6400E 03	4.1030E 18	203.15
18	4.6200E 03	2.8240E 18	207.38
20	5.8800E 03	2.0000E 18	211.75
22	7.4200E 03	1.4290E 18	215.94
24	9.2400E 03	1.0320E 18	219.20
26	1.1620E 04	7.4450E 17	223.84
28	1.4140E 04	5.4230E 17	227.83
30	1.8200E 04	3.9700E 17	231.79
32	2.2400E 04	2.9240E 17	235.74
34	2.8700E 04	2.1590E 17	240.40
36	3.5700E 04	1.6040E 17	245.14
38	4.4800E 04	1.1980E 17	249.88
40	5.6000E 04	8.9990E 16	254.62
42	7.0000E 04	6.7980E 16	259.35
44	8.9600E 04	5.1610E 16	264.08
46	1.1200E 05	3.9390E 16	268.80
48	1.4000E 05	3.0350E 16	272.15
50	1.7920E 05	2.3720E 16	272.15
52	2.2400E 05	1.8600E 16	271.14
54	2.8000E 05	1.4710E 16	267.21
56	3.5000E 05	1.1590E 16	263.28
58	4.3400E 05	9.1050E 15	259.36
60	5.3200E 05	7.1440E 15	254.79
62	7.0000E 05	5.6360E 15	247.35
64	8.6800E 05	4.4160E 15	239.91
66	1.0500E 06	3.4350E 15	232.47
68	1.3440E 06	2.6620E 15	225.04
70	1.6800E 06	2.0260E 15	217.61
72	2.1000E 06	1.5350E 15	210.19
74	2.6600E 06	1.1520E 15	202.77
76	3.3600E 06	8.5540E 14	195.36
78	4.2000E 06	6.2810E 14	187.95
80	5.3200E 06	4.5560E 14	180.54

TABLE 2-2
PHOTOLYSIS PROCESSES (sec^{-1})

J_1	$\text{O}_2 + h\nu \rightarrow 2 \text{O}$
J_2	$\text{O}_3 + h\nu \rightarrow \text{O}({}^1\text{D}) + \text{O}_2$
J_3	$\text{O}_3 + h\nu \rightarrow \text{O}({}^3\text{P}) + \text{O}_2$
J_4	$\text{H}_2\text{O} + h\nu \rightarrow \text{H} + \text{OH}$
J_5	$\text{N}_2\text{O} + h\nu \rightarrow \text{N}_2 + \text{O}$
J_6	$\text{CH}_4 + h\nu \rightarrow \text{CH}_3 + \text{H}$
J_7	$\text{CH}_3\text{Cl} + h\nu \rightarrow \text{CH}_3 + \text{Cl}$
J_8	$\text{CFCl}_3 + h\nu \rightarrow \text{CFCl}_2 + \text{Cl}$
J_9	$\text{CF}_2\text{Cl}_2 + h\nu \rightarrow \text{CF}_2\text{Cl} + \text{Cl}$
J_{10}	$\text{CCl}_4 + h\nu \rightarrow \text{CCl}_3 + \text{Cl}$
J_{11}	$\text{HCl} + h\nu \rightarrow \text{H} + \text{Cl}$
J_{12}	$\text{NO}_2 + h\nu \rightarrow \text{NO} + \text{O}$
J_{13}	$\text{NO}_3 + h\nu \rightarrow \text{NO} + \text{O}_2$
J_{14}	$\text{NO}_3 + h\nu \rightarrow \text{NO}_2 + \text{O}$
J_{15}	$\text{N}_2\text{O}_5 + h\nu \rightarrow \text{NO}_3 + \text{NO}_2$
J_{16}	$\text{HNO}_3 + h\nu \rightarrow \text{OH} + \text{NO}_2$
J_{17}	$\text{NO} + h\nu \rightarrow \text{N} + \text{O}$
J_{18}	$\text{H}_2\text{O}_2 + h\nu \rightarrow 2\text{OH}$
J_{19}	$\text{HO}_2 + h\nu \rightarrow \text{H} + \text{O}_2$
J_{20}	$\text{ClO} + h\nu \rightarrow \text{Cl} + \text{O}$
J_{21}	$\text{HOCl} + h\nu \rightarrow \text{OH} + \text{Cl}$
J_{22}	$\text{ClONO}_2 + h\nu \rightarrow \text{ClO} + \text{NO}_2$
J_{23}	$\text{H}_2\text{CO} + h\nu \rightarrow \text{H}_2 + \text{CO}$
J_{24}	$\text{H}_2\text{CO} + h\nu \rightarrow \text{H} + \text{HCO}$

using solar flux data obtained from the Handbook of Geophysics and Space Environments (1965). For the spectral region between 1750-3000A flux measurements were adopted from Detwiler, et. al. (1961). Below 1750A, the more recent data by Widing, et. al. (1970) are utilized. Computations are made using either a 24-hour averaged value of the solar flux or a single solar zenith angle (specified by ISWIT, Section 4.4). Table 2-3 contains the reactions and adopted rate constants for the relevant odd oxygen, hydrogen, nitrogen, and chlorine species. These rates are referenced to 80 km. Temperature dependence of the rate constants as a function of the temperature profile is given.

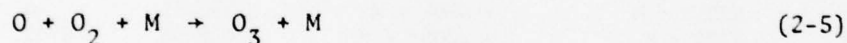
2.2 Summary of Relevant Stratospheric Chemistry

This section provides a brief review of the critical atmospheric species handled by the CMSP program.

The chemistry of atmospheric ozone was formulated by Chapman (1930). Chapman's model consists of four reactions involving only oxygen chemistry. He proposed that ozone is initiated by photolysis of O_2 in the Herzberg continuum below 2400 A, as



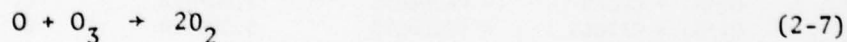
followed by the three body reaction



Ozone may be recycled by



followed by (2-5). Odd oxygen (O , O_3) is removed by



Using reactions (2-4) to (2-7), and assuming photochemical equilibrium conditions, ozone concentration may be expressed in a simple analytic form:

$$[O_3] = \left(\frac{J_1}{J_3} \right)^{1/2} \left(\frac{k_2}{k_4} \right)^{1/2} [O_2] [M]^{1/2} \quad (2-8)$$

TABLE 2-3

REACTION RATE
(AS A FUNCTION OF ALTITUDE, Z) = A
* EXP (B/TEMP (Z))

No.	REACTION	A	B
1	OH + CH3CL = CH2CL + H2O	1.66E-12	-1070.
2	H2O + O('D) = 2OH	2.35E-10	0.
3	CH4 + O('D) = CH3 + OH	1.40E-10	0.
4	H2 + O('D) = OH + H	1.00E-10	0.
5	H + O2 + M = HO2 + M	1.80E-32	340.
6	H + O3 = OH + O2	2.60E-11	0.
7	OH + O3 = HO2 + O2	2.30E-12	-1125.
8	OH + H2O2 = H2O + HO2	1.00E-11	-750.
9	HO2 + O3 = OH + 2O2	1.00E-13	-1525.
10	HO2 + O = OH + O2	1.00E-10	-250.
11	HO2 + NO = OH + NO2	1.10E-11	-1000.
12	HO2 + ClO = HClO + O2	0.0	0.
13	HO2 + HO2 = H2O2 + O2	5.00E-12	-500.
14	HO2 + OH = H2O + O2	2.00E-11	0.
15	HO2 + Cl = HCl + O2	3.00E-11	0.
16	H + HO2 = H2 + O2	1.00E-11	0.
17	H + HO2 = 2OH	4.20E-10	-950.
18	OH + CO = H + CO2	2.10E-13	-115.
19	OH + O = H + O2	1.00E-10	-250.
20	OH + HCl = H2O + Cl	2.00E-12	-313.
21	OH + CH4 = H2O + CH3	2.36E-12	-1710.
23	OH + HNO3 = H2O + NO3	1.00E-12	-600.
24	OH + OH = H2O + O	1.70E-12	0.
25	OH + H2 = H2O + H	6.70E-12	-2010.
26	Cl + H2 = HCl + H	5.70E-11	-2400.
27	Cl + H2O2 = HCl + HO2	6.00E-13	0.
28	ClO + NO2 + M = ClNO3 + M	3.80E-33	1055.
29	Cl + O3 = ClO + O2	2.70E-11	-257.
30	Cl + CH4 = HCl + CH3	7.29E-12	-1260.
31	ClO + O = Cl + O2	1.07E-10	-224.
32	ClO + NO = Cl + NO2	2.00E-11	0.
33	O + HCl = OH + Cl	0.0	0.
34	O + O2 + M = O3 + M	1.05E-34	520.
35	O + O3 = 2O2	1.30E-11	-2140.
36	NO2 + NO3 = N2O5*	1.00E-12	0.
38	N2O5* + M = N2O5 + M	3.70E-11	0.
39	N2O5 + M = N2O5* + M	9.00E-06	-9700.
40	NO + O3 = NO2 + O2	2.30E-12	-1450.
41	NO2 + O3 = NO3 + O2	1.20E-13	-2450.
42	NO2 + O = NO + O2	9.12E-12	0.
43	N2O + O('D) = N2 + O2	5.00E-11	0.
44	N2O + O('D) = 2NO	7.00E-11	0.
45	N + NO = N2 + O	2.00E-11	0.
46	N + O2 = NO + O	5.50E-12	-3200.
47	O('D) + CFCL3 = PRODUCTS	3.00E-10	0.
48	O('D) + CF2CL3 = PRODUCTS	3.00E-10	0.
49	O('D) + CH3CL = OH + CH2CL	0.0	0.
50	O('D) + CCL4 = PRODUCTS	0.0	0.
51	O('D) + M = O + M	2.00E-11	107.

Reactions Whose Rates Are Calculated By Different Formulae Are:

22	OH + NO2 + M = HNO3 + M	$R = 2.3E-13 * EXP(880./Temp.(Z)/(2.6E18 + M(Z)))$
37	N2O5* = NO2 + NO3	$R = 1.0E+8 * M(Z)/(2.6E19 * M(Z)) + 1.0E7$

where J_1 and J_3 are the photolysis rates for reaction (2-4) and (2-5) and k_2 and k_4 are the rate constants for reactions (2-5) and (2-7), respectively.

Equation (2-8) gives a good first order model of the vertical distribution of atmospheric ozone. It successfully predicts the ozone peak at around 25 km. However, it predicts too much ozone at all altitudes above 22 km, and it overestimates the total ozone abundance by about a factor of 2. Furthermore, Chapman's simple model does not include atmospheric transport processes and cannot account for the observed latitudinal distribution of ozone - low values at low latitudes and high values at high latitudes.

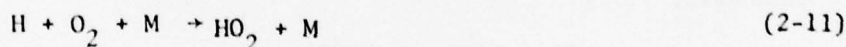
Bates and Nicolet (1950) first attempted to remove the discrepancies between observations and Chapman's theory by introducing catalytic hydrogen chemistry. (the HO_x family). Catalysis of odd oxygen recombination by hydrogen species (H, OH, HO_2) may take place either through



followed by



or through



followed by



These reactions are important above 50 km, and account for a reduction by about a factor of 2 to 3 in the concentration of ozone calculated by Equation (2-8).

Atmospheric odd hydrogen (H, OH, HO_2 , H_2O_2) is mainly formed by reactions involving H_2O molecules;



and



They are mainly removed by reactions

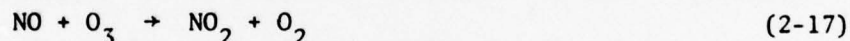


and



For a given H_2O concentration, the abundance of odd hydrogen is mainly controlled by reactions (2-13) to (2-16). Reaction (2-15) is the dominant loss process for odd hydrogen above 35 km.

The principal stratospheric sink for O_3 was not identified until 1970 when Crutzen (1970) and Johnston (1971) suggested that nitric oxide (NO) can catalytically recombine O and O_3 through the reaction



followed by



Oxides of nitrogen, NO_x (NO , NO_2 , NO_3 , N_2O_5 , HNO_3) are formed in the stratosphere by photochemical decomposition of N_2O (McElroy and McConnell, 1971):

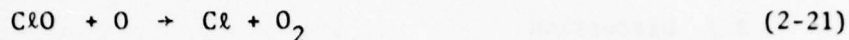


Nitrous oxide (N_2O) is mainly produced in soil as a by-product of the denitrification process, with some contribution from high temperature combustion processes.

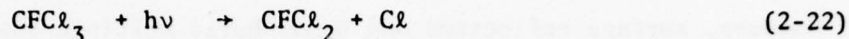
The possible importance of chlorine chemistry in the stratosphere was noted by Wofsy and McElroy (1974) and by Stolarski and Cicerone (1974). They suggested that free chlorine may play a role similar to NO_x in the recombination of O and O_3 through the reactions



followed by



A source of stratospheric Cl was not identified until Molina and Rowland (1974) suggested the photolysis of fluorocarbons (F-11, F-12) through the reactions



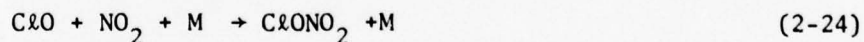
and



These reactions constitute the basis of the ClX family of the CMSP program.

Theoretical model calculations [Wofsy et. al. (1975), Crutzen (1974)] have shown that continued release of fluorocarbons (CFMs) at 1973 production rates might lead to approximately 7 to 12 percent ozone reduction in the year 2200. These results have led to the current concern regarding the effects of CFMs on stratospheric ozone.

Prior to 1976, it was thought that HCl was the only inert form of odd chlorine species. The chemistry of chlorine nitrate, ClONO_2 , was ignored until Rowland et. al. (1976) measured the absorption cross section of ClONO_2 , which suggested its appreciable life time (~ 1 day) in the mid-stratosphere. Chlorine nitrate is formed by a three body reaction



with a rate constant

$$k_{24} = 5.1 \times 10^{-33} \exp(-900/T)$$

Formation of ClONO_2 would tie up the active Cl and NO_x -species, and could lower the catalytic efficiency of both the ClX and NO_x cycles.

3. Development of the Radiative Transfer Section

3.1 Discussion

In the basic version of the CMSP program only the most elementary radiative transfer process, that of absorption by molecular oxygen and ozone, is incorporated within the calculation of photodissociation rates. However, surface reflection and atmospheric multiple scattering of incident solar radiation by molecules and aerosols can significantly enhance the photolysis rates of certain stratospheric species (Luther and Gelinas, 1976) and may have an appreciable effect on stratospheric photochemistry (Sze and Tripp, 1977).

The photodissociation rate (sec^{-1}) of species i at altitude z is given by:

$$J_i(t, z) = \int_{\lambda} \pi F_{\lambda}(t, z) \sigma_{\lambda, i} \phi_{\lambda, i} d\lambda \quad (3-1)$$

where

$\sigma_{\lambda, i}$ = absorption cross section of species i at wavelength λ (cm^2)

$\phi_{\lambda, i}$ = quantum yield of species i at wavelength λ (dimensionless)

$\pi F_{\lambda}(t, z)$ = flux at level z available for photodissociations at a time t ($\text{photons cm}^{-2} \text{sec}^{-1} \text{\AA}^{-1}$).

In the pure absorption model, the available photons are calculated based on attenuation of the direct solar beam by O_2 and O_3 or:

$$\pi F_{\lambda}(t, z) = \pi F_0 \exp [-\tau(z)/\mu_0] \quad (3-2)$$

where

πF_0 = unattenuated solar flux

μ_0 = cosine of the solar zenith angle

$$\tau(z) = \int_z^{\infty} \sum_i \sigma_{i, a} n_i(z) dz \quad (3-3)$$

$\sigma_{i, a}$: absorption cross section of species i . (cm^2)

n_i : local number of density of species i . (cm^{-3})

The flux depends on time through variation of the solar zenith angle with time of day:

$$\mu_0 = \cos \theta \cos \delta \cos \left(\frac{t}{240} \right) + \sin \theta \sin \delta \quad (3-4)$$

where

θ = latitude (deg.)

δ = solar declination angle (deg.)

t = local time (sec)

The single solar zenith angle photolysis rate is given by (3-1).

The 24 hour averaged photolysis rate is given by:

$$\bar{J}_i(z) = \frac{1}{86400} \int_0^{86400} J_i(t, z) dt \quad (3-5)$$

In order to account for the effects of multiple scattering, the radiative transfer equation:

$$\mu \frac{dI(\tau, \mu)}{d\tau} = I(\tau, \mu) - S(\tau, \mu) \quad (3-6)$$

must be solved at each level of the atmosphere for each frequency.

The flux available for photodissociation πF is then given by:

$$F(\tau) = 2 \int_{-1}^{+1} I(\tau, \mu) d\mu \quad (3-7)$$

In Eqn (3-6), $S(\tau, \mu)$ is the source function which obeys the integral equation:

$$\begin{aligned} S(\tau) = & \frac{\omega_0(\tau)}{4} F_0 \cdot \exp(-\tau/\mu_0) \\ & + \frac{\omega_0(\tau)}{2} \int_0^{\tau^*} S(t) E_1(|t-\tau|) dt \\ & + 2 \cdot \frac{\omega_0(\tau)}{2} \cdot R \cdot E_2(\tau^*-\tau) \int_0^{\tau^*} S(t) E_2(\tau^*-t) dt \end{aligned} \quad (3-8)$$

$$+ \frac{\omega_0(\tau)}{2} \cdot \mu_0 \cdot F_0 \cdot R \cdot E_2(\tau^* - \tau) \cdot \exp(-\tau^*/\mu_0)$$

where

$$E_n(x) = \int_0^1 \exp(-x/\mu) \mu^{(n-1)} \frac{d\mu}{\mu}$$

R = ground reflectivity

$$\tau^* = (\text{total}) \text{ optical depth} = \int_0^\infty \sum_i \sigma_i n_i(z) dz$$

and

ω_0 = single scattering albedo

$$\omega_0(z) = \frac{\sum_i \sigma_{s,i} n_i(z)}{\sum_i \sigma_{s,i} n_i(z) + \sum_i \sigma_{a,i} n_i(z)}$$

In Eqn (3-8) the optical depth τ is computed using the extinction cross section ($\sigma_i = \sigma_{s,i} + \sigma_{a,i}$) where $\sigma_{s,i}$ is the scattering cross section of species i as compared with the absorption cross section only in Eqn (3-3)

Sources of scattering opacity include both atmospheric gases (Rayleigh scattering) and polydisperse aerosol distributions (Mie scattering). Evaluation of the Rayleigh scattering cross section at each level is accomplished using (McClatchey, et. al., 1972)

$$\sigma_{s,\text{Rayleigh}}(z) = \left(9.807 \times 10^{-25} \nu^{-4} + 4.0117 \right) \frac{N(z)}{N(z=0)} \quad (3.9)$$

where: ν = frequency in wave numbers (cm^{-1})

$N(z)$ = total number density at level z (cm^{-3})

Aerosol models have been adopted from Shettle and Fenn (1976) which provides the wavelength dependence of the absorption and extinction cross sections for four characteristic aerosol models: maritime, urban, rural, and tropospheric. The first three are, strictly speaking, boundary layer models while the tropospheric model is more characteristic of the atmosphere above the boundary

layer. The altitude variation of the aerosol number densities (Table 3-1) is assumed to be the same for all models and is taken from Elterman (1968).

The surface is assumed to be Lambertian. The reflectivity (R) is defined as the ratio between the incoming and outgoing fluxes at the surface and the reflection is isotropic (i.e. no angle preference for the outgoing radiance). The reflected intensity at surface $I(\tau^*, \mu)$ can be written as

$$I(\tau^*, \mu) = 2 \cdot R \int_0^{\tau^*} S(t) E_2(\tau^* - t) dt \quad (3-10)$$

3.2 Implementation of the Variational-Iterative (VI) Technique

Once equation (3-8) is solved for the source function, the total flux available for photodissociation $\pi F(\tau)$ in the fully scattering case is given by:

$$\begin{aligned} F(\tau) = & F_0 \exp(-\tau/\mu_0) + 2 \int_0^{\tau^*} S(t) E_1(|t - \tau|) dt \\ & + 2 \mu_0 F_0 R E_2(\tau^* - t) \exp(-\tau^*/\mu_0) \\ & + 4 R \cdot E_2(\tau^* - t) \int_0^{\tau^*} S(t) E_2(\tau^* - t) dt \end{aligned} \quad (3-11)$$

The physical meaning of each term in Equation (3-11) is as follows:

- 1) the first term represents the attenuated direct beam. (This is the only term used in a pure absorption model).
- 2) the second term represents the diffuse radiation in the atmosphere due to scattering of the direct beam;
- 3) the third term represents the attenuated direct beam reflected from the surface with reflectivity R;
- 4) the fourth term represents the diffuse radiation due to scattering of the reflected beam.

This may be substituted into (3-1) to evaluate the photodissociation rates.

TABLE 3-1

ALTITUDE VARIATION OF AEROSOL NUMBER DENSITIES

Altitude (km)	Aerosol Number Density (cm^{-3})	Altitude (km)	Aerosol Number Density (cm^{-3})
0	2.8280E+03	42	7.9600E-02
2	5.3710E+02	44	5.7040E-02
4	1.1920E+02	46	2.8290E-02
6	6.3370E+01	48	2.0990E-02
8	6.7690E+01	50	1.0780E-02
10	5.6750E+01	52	5.5800E-03
12	5.5850E+01	54	4.1140E-03
14	5.1480E+01	56	2.0780E-03
16	4.5110E+01	58	1.4950E-03
18	4.3140E+01	60	7.7350E-04
20	2.6670E+01	62	4.0030E-04
22	1.4555E+01	64	2.8800E-04
24	8.1260E+00	66	1.4900E-04
26	5.7060E+00	68	1.0720E-04
28	3.5740E+00	70	5.5500E-05
30	2.2380E+00	72	2.1440E-05
32	1.1480E+00	74	1.3320E-05
34	8.2230E-01	76	5.1440E-06
36	4.2190E-01	78	3.1960E-06
38	3.0220E-01	80	1.2340E-06
40	1.5500E-01		

To solve the integral equation, (3-8), the variational-iterative technique introduced by Sze (1976) was used. This method, in essence, provides a direct way for constructing an approximate source function for equation (3-8) and allows for arbitrary inhomogeneity in the atmosphere. It has been shown by Burke and Sze (1977) that the variational-iterative approach requires relatively little computational time to achieve satisfactory accuracy in comparison to other standard methods.

In the variational-iterative technique, the approximated source function can be expressed as:

$$S_a(\tau) = U_a(\tau) \sqrt{\omega_0(\tau)}, \quad (3-12)$$

where

$$U_a(\tau) = \sum_i C_i V_i(\tau), \quad (3-13)$$

and $V_i(\tau)$ is trial function for the i th layer.

The total optical depth τ^* is divided into $(N-1)$ layers with an average single scattering albedo ω_j assigned to each layer j . The simplest piece-wise continuous trial functions are the step functions defined by

$$V_j(\tau) = \begin{cases} 1 & \tau_j \leq \tau \leq \tau_j + 1 \\ 0 & \tau < \tau_j; \tau > \tau_j + 1 \end{cases} \quad (3-14)$$

It can be shown (Sze, 1976) that the C_i are solutions to the following set of linear algebraic equations:

$$\sum_{j=1}^N M_{ij} C_j = f_i. \quad (3-15)$$

The M_{ij} are simply given by

$$M_{ij} = \delta_{ij} \Delta\tau_j - \frac{\sqrt{\omega_i \omega_j}}{2} \int_{\tau_i}^{\tau_i + 1} B_j(\tau) d\tau, \quad (3-16)$$

where

$$\delta_{ij} = \begin{cases} 1 & \text{for } i=j \\ 0 & \text{for } i \neq j, \end{cases}$$

$$B_j(\tau) = \int_{\tau_j}^{\tau_j+1} E_i(|\tau-t|) dt,$$

and f_i is

$$f_i = \frac{F_0}{4} \mu_0 \sqrt{\omega_i} [\exp(-\tau_i/\mu_0) - \exp(-\tau_{i+1}/\mu_0)]$$

The smoothed approximated source function including the ground reflection can be written as

$$\begin{aligned} S_1(\tau) = & \frac{\omega_0(\tau)}{4} F_0 \exp(-\tau/\mu_0) + \frac{\omega_0(\tau)N-1}{2} \sum_{j=1} C_j \sqrt{\omega_j} B_j(\tau) \\ & + \frac{\omega_0(\tau)}{2} \cdot R \cdot E_2(\tau^*-\tau) [2 \sum_{j=1}^{N-1} C_j \sqrt{\omega_j} D_j + \mu_0 \exp(-\tau^*/\mu_0)] \end{aligned} \quad (3-17)$$

where

$$D_j = \int_{\tau_j}^{\tau_j+1} E_2(\tau^*-t) dt$$

Subsequent iterations

$$\begin{aligned}
 S_{n+1}(\tau) = & \frac{\omega_o(\tau)}{4} F_o \exp(-\tau/\mu_o) + \frac{\omega_o(\tau)}{2} \int_0^{\tau_*} E_1(|\tau-t|) S_n(t) dt \\
 & + \frac{\omega_o(\tau)}{2} \cdot R \cdot E_2(\tau_*-\tau) \left[2 \int_0^{\tau_*} E_2(\tau_*-t) S_n(t) dt + \mu_o \exp(-\tau_*/\mu_o) \right]
 \end{aligned}
 \tag{3-18}$$

would bring the source function to the desired accuracy.

3.3 Results

The results of two relevant calculations using the models described in the previous sections are contained in Appendix C. (A complete description of the output format is given in Section 4.5.) The first set of profiles is for an absorption only model where net fluxes are calculated using Eqn. (3-2). The second set is for a complete multiple scattering calculation [using equation (3-11)] where a surface reflectivity of 0.2 is assumed. Both calculations use a single solar zenith angle given by $\cos^{-1}(.707)$.

Several comparisons can be made between the calculations. In particular, the effect of multiple scattering and surface reflection on the photodissociation rate of O_3 be seen. Figure 3-1 illustrates the percent increase in the value of CJ03 for the two cases cited. A second curve (for a surface reflectivity of 0.8) indicates that highly reflecting surfaces and/or large expanses of cloud deck may have a significant impact on stratospheric photochemistry.

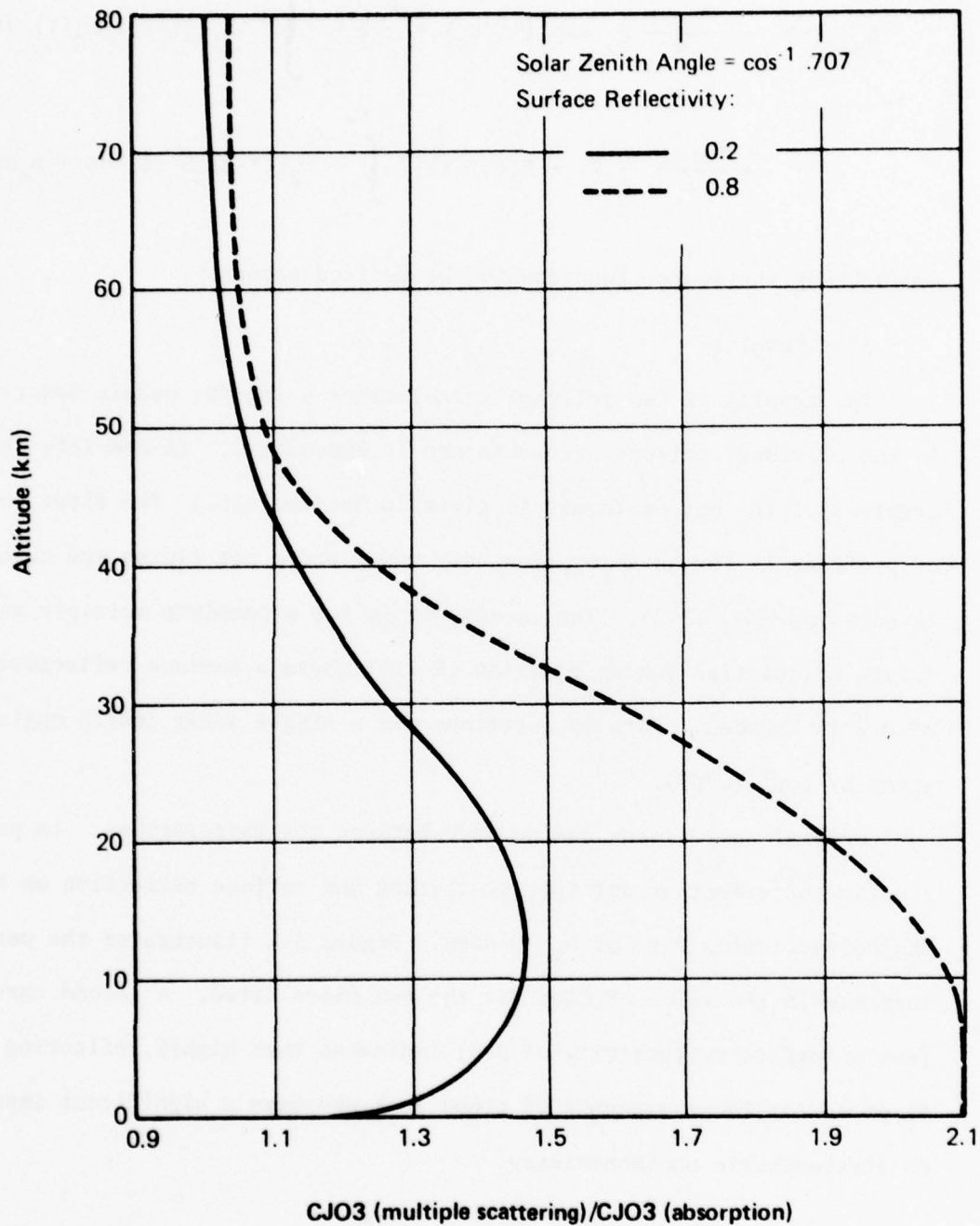


Figure 3-1 Percent Increase in Value of CJO3

4. Program Description

4.1 Summary

The Chlorine Model Study Program (CMSP) computer code consists of a main program (MAIN), forty subroutines, function subprograms, and a subprogram Block Data of initialization and model parameters. The primary function of the main program is to select one of two operational modes determined by "keywords" read from the input set (see Section 5). Specification of the keyword PARAMETER calls subroutine INPARM which establishes the initial constants for each case. The keyword "RUN" directs the main program to call subroutine PHOCHM which conducts the actual photochemical calculation for each case. A keyword of "ENDJOB" causes the program to terminate.

Since the sequence of program logic is somewhat complex due to the nature of the problem, this section provides a narrative description including considerable detail within many of the relevant subroutines. For clarity, housekeeping subroutines found in the program listing (Appendix A) are neither included in the flow chart (Appendix B) nor discussed further in this section. (These subroutines such as INPUT, PAGE, LINE, DAY, ERRM, etc. perform such functions as page turning and reading, line count, date writing, and error flagging.) The reader is urged to utilize the program listing and flow chart in following through this program description.

Table 4-1 provides a schematic view of the CMSP logic which may be helpful. Here the most important subroutines are listed according to their calling order and priority within the program. Priority is designated by levels: Level 0 is assigned to the MAIN program, while numerically higher levels are more distant from the MAIN program. A level 3 subroutine, for example, will return to a level 2 subroutine and may call a level 4 subroutine. The overall function of each block of coding is designated

TABLE 4-1

SCHEMATIC PRESENTATION OF THE CHLORINE

MODEL STUDY PROGRAM COMPUTER CODE

Level 0	Level 1	Level 2	Level 3	Level 4	Function
MAIN					
	ALTGEN				
	INPARM				
		WEIGHT			
		QSCATT			Initialize
		CPHI1			
		SETUP			
			EDC1/EDC2		
		RCONST			
	PHOCHM				
		SETUP2			
		RJITER			
			COLDEN		
			COMPJ		Compute J Values
				COMTAU	
				OMEGA	
				VIM	
		INITAL			
			PCLOX		
			PNOX		
				QUAD	"Short-Lived" Species
		SOLVE			
			JACOB		
				QUAD	
			LINEQN		
			PNOX		
		CFLOW			
			RINTER		
			CSPEC		
				CXL	
				COEF	
				TRIDIA	"Long-Lived Species"
			REPCN		
				PNOX	
				PCLOX	
			RINTER		
			SETUP 2		

at the right of the table. For example, PHOCHM (Level 1) calls RJITER (Level 2) and its higher level subroutines which compute photodissociation rates (so-called "J" values).

4.2 Initialization: BLOCK DATA

Although not contained explicitly within the flow chart, the BLOCK DATA section constitutes a significant source of input data and contains many of the run parameters which are required for model calculations. These data are introduced by DATA statements which are made accessible to the user subroutines by means of labeled COMMON statements. Table 4-2 lists the important model variables contained within BLOCK DATA including species mixing ratio or number density profiles, rate constant data, photodissociation cross section and rate values, and model atmosphere. Additionally, the corresponding labeled COMMON name is given. Values are compiled into their respective array locations based on their dependence on altitude or wavelength. Quantities characterizing the atmospheric model such as temperature (TEMP) and mixing ratios (H, OH, etc.) are given as level values at 2 km intervals from the surface to 80 km. Wavelength dependent quantities such as the solar flux (FL) and photodissociation cross sections (QO2, QO3 etc.) are digitized at wavelengths given by the array WL such that WL(1) is the wavelength at which the cross section of O_2 is QO2(1), etc.

In addition to vertical profiles and wavelength dependent spectra, BLOCK DATA also contains a large number of default values for branching parameters and other initial conditions specifiable for a particular case such as the boundary conditions on the fluxes or mixing ratios of certain species. These BLOCK DATA default values may be changed by utilizing the NAMELIST \$INPUT (see Section 4.3.2) if desired, otherwise the default values are used. A complete description of these data is given in Section 5.2.

TABLE 4-2
BLOCK DATA SUPPLIED VALUES AND LABELED COMMON NAMES

<u>Labeled Common Name</u>	<u>Variable Name</u>	<u>Identity</u>	<u>Units</u>
MODEL	TEMP	temperature	$^{\circ}\text{K}$
	DM	total number density	cm^{-3}
	DID	$\text{O}({}^1\text{D})$ number density	cm^{-3}
	DA23	aerosol number density	cm^{-3}
RATES	RA	first rate constant	$\text{cm}^{3n}\text{sec}^{-1}$
	RB	second rate constant	$^{\circ}\text{K}$
RLOW	RN20	mixing ratio of N_2O at bottom	v/v
	RNOX	flux of NO_x at bottom	$\text{cm}^{-2}\text{sec}^{-1}$
	RCH4	mixing ratio of CH_4 at bottom	v/v
	RF11	flux of flourocarbon 11	$\text{cm}^{-2}\text{sec}^{-1}$
	RF12	flux of flourocarbon 12	$\text{cm}^{-2}\text{sec}^{-1}$
	RCH3C	mixing ratio of CH_3Cl at bottom	v/v
	RCLX	mixing ratio of Cl_x at bottom	v/v
	RCCL4	flux of CCl_4 at bottom	$\text{cm}^{-2}\text{sec}^{-1}$
	RO3	mixing ratio of O_3 at bottom	v/v
SOLCON	WL	wavelength	\AA
	FL	solar flux	$\text{cm}^{-2}\text{sec}^{-1}$
	QO2	photodissociation cross section O_2	cm^2
	QO3	photodissociation cross section O_3	cm^2
SOLCN1	QCF2	photodissociation cross section CF_2Cl_2	cm^2
	QCF3	photodissociation cross section CFCI_3	cm^2
	QCCL4	photodissociation cross section CCl_4	cm^2
	QCH3C	photodissociation cross section CH_3Cl	cm^2
	QCLNO3	photodissociation cross section ClONO_2	cm^2
	QN20	photodissociation cross section N_2O	cm^2
	QHNO3	photodissociation cross section HNO_3	cm^2
	QH202	photodissociation cross section H_2O_2	cm^2
	QN205	photodissociation cross section N_2O_5	cm^2
	QHCL	photodissociation cross section HCl	cm^2
	QHOCL	photodissociation cross section HOCl	cm^2
	QNO2	photodissociation cross section NO_2	cm^2
	QH20	photodissociation cross section H_2O	cm^2

TABLE 4-2 (Continued)
BLOCK DATA SUPPLIED VALUES AND LABELED COMMON NAMES

<u>Labeled Common Name</u>	<u>Variable Name</u>	<u>Identity</u>	<u>Units</u>
SPECIE	H	H number density	cm ⁻³
	OH	OH number density	cm ⁻³
	HO2	HO ₂ number density	cm ⁻³
	H2O2	H ₂ O ₂ number density	cm ⁻³
	O3	O ₃ number density	cm ⁻³
	O	O number density	cm ⁻³
	NO	NO number density	cm ⁻³
	NO2	NO ₂ number density	cm ⁻³
	HNO3	HNO ₃ number density	cm ⁻³
	NOX	NO _x mixing ratio	v/v
	CO	CO mixing ratio	v/v
	CH4	CH ₄ mixing ratio	v/v
	H2O	H ₂ O mixing ratio	v/v
	H2	H ₂ mixing ratio	v/v
	CLX	Clx mixing ratio	v/v
PHRATE	JHCL	photodissociation rate HCl	sec ⁻¹
	JCH4	photodissociation rate CH ₄	sec ⁻¹
	JN2O	photodissociation rate N ₂ O	sec ⁻¹
	JN2O5	photodissociation rate N ₂ O ₅	sec ⁻¹
	JHNO3	photodissociation rate HNO ₂	sec ⁻¹
	JH2O2	photodissociation rate H ₂ O ₂	sec ⁻¹
	JNO2	photodissociation rate NO ₂	sec ⁻¹
	JCF2	photodissociation rate CF ₂ Cl ₂	sec ⁻¹
	JCF3	photodissociation rate CFC1 ₃	sec ⁻¹
	JH2O	photodissociation rate H ₂ O	sec ⁻¹
	JO3	photodissociation rate O ₃	sec ⁻¹
	JO2	photodissociation rate O ₂	sec ⁻¹
	JHOCL	photodissociation rate HOCl	sec ⁻¹

4.3 Initialization Subroutines: ALTGEN, INPARM

4.3.1 Subroutine ALTGEN

Upon entering the MAIN program, subroutine ALTGEN is called. The primary function of this code is to fill the array ALT which is contained in labeled COMMON, MODEL and gives the altitude of each level in 2 km (2.0×10^5 cm) increments from 0.0 to 80.0 km. However, ALTGEN also provides revised solar flux data (overriding the values specified in BLOCK DATA) in the 1900 to 2250 \AA wavelength region and photodissociation cross sections for chlorine nitrate. Additionally, the aerosol model number density distribution with height is specified by the parameter IAERO[= 0 (23 km) or = 1 (5 km)] and the integrated total number density of molecules DMINT, and aerosols DAINTE are computed above a given level. These integrated densities are later used in the evaluation of optical depth. After ALTGEN is called control is returned to MAIN.

4.3.2 Subroutine INPARM

The keyword PARAMETERS read from the input set directs the program to call subroutine INPARM. INPARM establishes the basic input parameters required to run the model calculation. This is accomplished both by direct modification of previously stored values in BLOCK DATA and by calling higher level subroutines to perform additional computations on the basic input set. A NAMELIST statement is provided which may be used (see Section 5) to change the values of any of the formatted parameters from the default values.

For example, ISWIT which determines whether a single sun angle (=0) or a 24 hour average (=1) is used in the J-value computation may be changed from the default value (1) to zero by using the NAMELIST \$INPUT. The subroutine listing (Appendix A) illustrates which parameters may be changed.

Certain basic calculations are performed by calling subroutines WEIGHT, QSCATT, CPHI1, SETUP, and RCONST.

Subroutine WEIGHT computes the length of the day using the parameters LAT and DEL. The day is then divided into twelve equal time intervals (one hour at equinox) and the cosine of the solar zenith angle is computed at the midpoint of these intervals. Six values (those on either side of noon are equal) of the reciprocal of the cosine of the solar zenith angle are stored in array A. These are used to compute the 24 hour average model in subroutine COMTAU (Section 4.4.1).

Subroutine QSCATT computes the Rayleigh scattering coefficient QRAY, aerosol extinction coefficient QAE, and aerosol absorption coefficient QAA at the surface ($z=0$) as a function of wavelength. A particular aerosol size distribution is specified by the parameter ISIZE which selects one of four given models or a user's own model. (See Section 5.3). These values are later used in subroutine OMEGA to compute optical depth and the single scattering albedo profile when multiple scattering is considered.

Subroutine CPHI1 allows a quantum yield PHI1 to be introduced into the evaluation of the photodissociation rate for ClONO_2 . Furthermore, it may be given one value P11 for wavelengths WL(1) to WL(I1), inclusive, and a second value P22 from WL(I1+1) to the upper wavelength limit. Default values in BLOCK DATA are I1 = 59, P11 = P22 = 1.0, so that the quantum yield is unity.

Subroutine SETUP establishes the eddy coefficient model to be used and operates on the basic 41 level model atmosphere data. Upon entering the subroutine, Hunten's eddy coefficients are read into array EK by a DATA statement. If NEDDY is zero, these values are used.

I NEDDY is either one or two, subroutine EDC1 or EDC2, respectively, is called which substitutes either Chang's or an analytic form for these values. NEDDY has a default value of zero and may be changed in the NAMELIST \$INPUT. A factor FKK (default value - 1.0) may be specified to multiply any of these profiles by a constant value. The basic model atmosphere data (TEMP, DM, and EK) are then interpolated to produce arrays (CTEMP, CDM, and CEK) of 81 levels of 1 km thickness from the data arrays containing 41 levels of 2 km thickness. These results are printed out at 2 km intervals.

Subroutine RCONST calculates the reaction rates of each of the chemical reactions as a function of temperature at the 81 levels of the atmosphere. The required input consists of the model atmosphere temperature profile and the first and second Arrhenius rate constants RA and RB from BLOCK DATA or NAMELIST \$INPUT. For each reaction I and atmospheric level J the reaction rate RATE is given by:

$$\text{RATE}(I,J) = \text{RA}(I) * \text{EXP}(\text{RB}(I)/\text{CTEMP}(J))$$

Rates are computed explicitly for reactions which do not obey the above relation. A table of reactions and rate constant information is printed. (see listing, Appendix A). After execution of RCONST control reverts to INPARM which returns to MAIN.

4.4 Main Calculation: PHOCHM

As indicated in the flow chart the keyword RUN calls the subroutine PHOCHM. PHOCHM controls the remainder of the calculation for a particular case and may be considered as the main program for most purposes.

As PHOCHM is entered the steady state version is selected by specifying FT = 0., FA = 2., FB = 0. and FM = 0. (these values will be used by subroutine COEF in performing the long-lived species calculations. (see 4.4.3).

The functions performed within PHOCHM may be divided into three areas:

(a) computation of photodissociation rates; (b) calculations for short-lived species (no diffusion); and (c) calculations for long-lived species (vertical diffusion). Most evaluations are made external to PHOCHM by calling appropriate higher level subroutines.

4.4.1 Subroutine RJITER: Computation of Photodissociation Rates

Subroutine RJITER functions as a calling program to facilitate the calculation of photodissociation rates at each atmospheric level. Its two arguments ISWIT and ISCATT are carried in COMMON to PHOCHM and specify the nature of the time averaging (single solar zenith angle vs. 24 hour average) and whether multiple scattering is considered, respectively. The upper limit for the wavelength integration IU is set in RJITER. For the absorption only model, the integration stops at 4025⁰A and the contributions to the dissociation of O₃ from the visible are included as a constant factor PJ03. (set in BLOCK DATA). When multiple scattering is considered, however, the integration is extended through the visible region.

RJITER calls subroutine COLDEN which computes the column densities of ozone from a given level to the top of the atmosphere. These values, DO3INT, are used in the computation of optical depth.

Subroutine COMPJ called from RJITER performs the actual wavelength integration. The specific details of the calculation depend on the parameters ISWIT and ISCATT. For the simplest case ISWIT = 0, ISCATT = 0, a fixed solar zenith angle GMU = .707 is used and the number of photons cm⁻²sec⁻¹ available for photodissociation at a particular level is based on simple attenuation of the direct solar beam by O₂ and O₃ above the level. That is, optical depth TAU is computed as:

$$\text{TAU} = \text{QO3} * \text{DO3INT} + \text{QO2} * \text{DMINT} * \text{P02}$$
 and DMINT is the integrated total number density.

J values are then computed in a straightforward manner by taking the product of available flux ($= FL * EXP (-TAU/GMU)$), cross section (Q02, Q03, QHC1, etc.), and quantum yield if required (PH11) at a given wavelength and integrating over the wavelength interval. Flux is reduced by a factor of 0.5 (RDF) for the single angle calculation to account for night and day.

When ISWIT = 1 and a 24 hour average model is required, the transmissivity from the top of the atmosphere to a given level is weighted by calling a subroutine COMTAU which uses the array of coefficients A computed by WEIGHT to simulate the variation of solar zenith angle over a day. The subroutine COMTAU essentially performs the calculation:

$$TRAN (24 \text{ hr average}) = \frac{1}{24} \sum_{I=1}^{12} EXP (-TAU * A (I))$$

When a multiple scattering calculation is desired (ISCATT = 1) two additional subroutines OMEGA and VIM are utilized. (see Section 3 for details of the scattering model). OMEGA computes optical depth from a given level to space as the sum of both attenuation (molecular and aerosol) and scattering (aerosol and Rayleigh). Aerosol absorption and extinction and Rayleigh scattering coefficients QAA, QAE, QRAY are carried in COMMON from subroutine QSCATT. Additionally, a single scattering albedo profile as a function of level is computed. An interpolation scheme creates a single scattering albedo profile as a function of optical depth which is input to subroutine VIM which performs a variational-iterative method multiple scattering calculation and returns the net flux available for photodissociation at a given optical depth normalized to the solar flux. This mean intensity includes contributions from the attenuated direct solar beam (absorption only case) and diffuse contributions reflected from the surface and scattered by molecules and aerosol particles. The surface reflectivity REF is contained in NAMELIST.

Subroutine OMEGA uses its knowledge of the altitude variation of optical depth to reinterpolate the net flux vs. optical depth profile to a net flux at altitude level profile. These values are placed in array F and returned to COMPJ for integration into the J value calculation. Subroutine VIM calls its own family of higher order subroutines which function somewhat independently of the overall CMSP code. A schematic presentation of the VIM subroutine heirarchy is presented in Table 4-3 in relation to the total CMSP sequence.

In order to account for the desired time averaging, OMEGA must be called for each GMU desired. Therefore, if a 24 hour average model is required (ISWIT = 1), OMEGA is called for each GMU using the solar zenith angles computed by WEIGHT (= 1/A) and averaging over 24 hours as was done for the absorption only case.

4.4.2 Subroutines INITAL, SOLVE: Short-lived Species

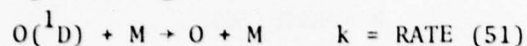
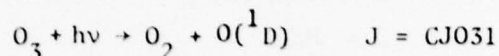
After photodissociation rates based on the first guess ozone concentrations are returned to PHOCHM by RJITER, calculations of the species concentration profiles begin. As noted in Table 4.1 the PHOCHM code sequence from this point can be divided into segments handling the short-lived species and the long-lived species. An iteration counter I is incremented by statement 10 in PHOCHM after initialization to zero. This index keeps account of the number of times the program is executed to reach convergence. An upper limit of 50 iterations is assigned. For all iterations after the first the old OH and O₃ profiles (OLDOH,003) are saved for convergence testing before being recomputed. The computed photodissociation rates of O₂, O₃, HNO₃, H₂O₂, and N₂O₅ are substituted for the BLOCK DATA values at each level and the concentration profile of

TABLE 4-3 SCHEMATIC PRESENTATION OF SUBROUTINE VIM SEQUENCE

```

MAIN
  PHOCHM
    RJITER
      COMPJ
        OMEGA
          VIM
            RMATRI
            LINEQN
            SG
            S11
            SE
            S1NT
            E
            E2
            E3
  
```


$O(^1D)$, DID, is computed based on equilibrium between the reactions;



this yields the relationship:

$$DID = CJ031 * O_3 / \text{RATE}(51) * DM$$

at each level.

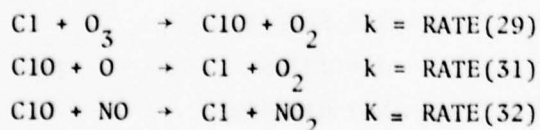
The calculation continues with a DO loop from statement 60 to statement 100 in PHOCHM. For each level in the atmosphere concentrations of the short-lived species are computed using the INITIAL and SOLVE subroutines. At a given level, INITIAL sets up a non-linear system of simultaneous equations in four variables: $Y(1) = H$, $Y(2) = OH$, $Y(3) = HO_2$, and $Y(4) = O_3$. The Y array gives the concentration of these four species at a given level. (Note: O_3 is short-lived above 30 km and long-lived below 30 km.)

Initial concentrations of CO , O_2 , H_2 , CH_4 , ClX , NO_x , H_2O , OH , and HO_2 are first evaluated from input profiles. On subsequent iterations the computed values are used. For example, mixing ratio is converted to number density by multiplying by the total number density. An iteration counter (J) is set to monitor convergence and subroutine PCLOX is called.

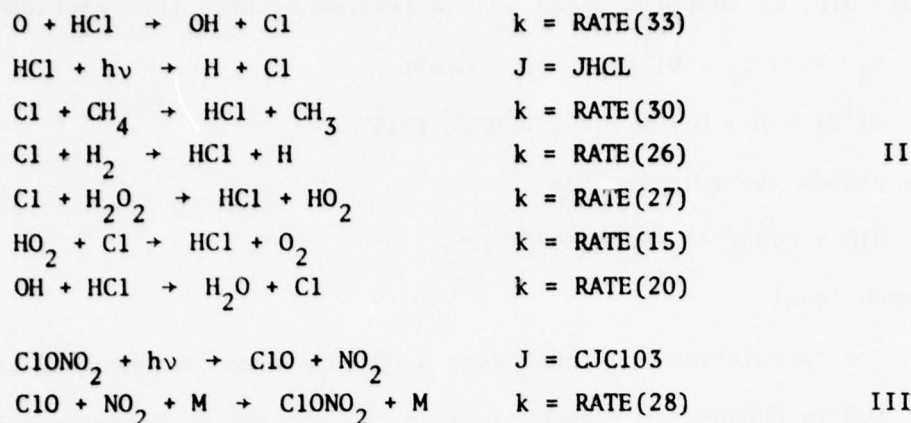
Subroutine PCLOX computes the level concentrations of CL, CLO, and HCL by assuming equilibrium of production and loss mechanisms. The following ratios are computed:

$$\begin{aligned} RRC1 &= CLO/CL & I \\ RRC2 &= HCL/CL & II \\ RRC3A &= CLNO_3/CLO & III \\ RRC3B &= CLNO_3/CL = RRC3A * RRC1 \end{aligned}$$

the corresponding reaction schemes assuming steady state at each level are:



I

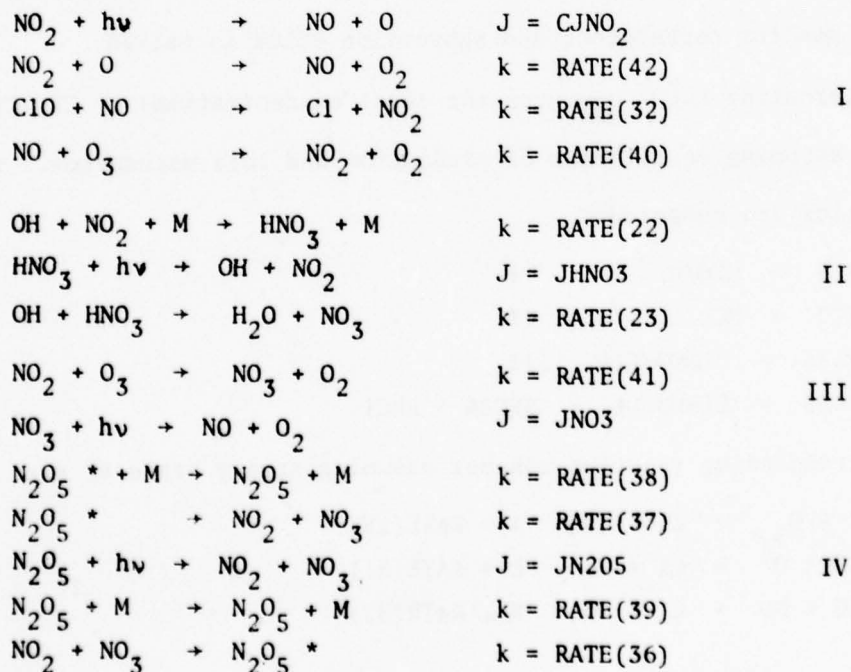


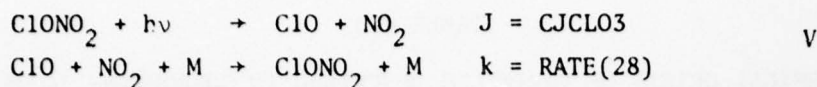
After PCLOX returns to INITIAL, PNOX is called and an analogous computation of the level values of NO, NO₂, HNO₃, NO₃, N₂O₅, and CLNO₃ is made.

The following ratios are computed:

$RR1 = NO/NO_2$	I
$RR2 = HNO_3/NO_2$	II
$RR3 = NO_3/NO_2$	III
$RR4 = N_2O_5/NO_2 * NO_2$	IV
$RR9 = CLNO_3/NO_2$	V

Reaction schemes determining these ratios assuming steady state at each level of the atmosphere are:





In the course of its calculation PNOX calls subroutine QUAD which solves the quadratic equation. PNOX returns control to INITIAL where a convergence test is made based on comparison of the old and new values of NO, NO₂, and HNO₃. If convergence occurs (within approximately 0.5%), INITIAL is exited and returns to PHOCHM.

PHOCHM calls subroutine SOLVE which organizes the solution of the chemical system for the short-lived species concentrations at a given level. Basically, the quantities Y (N), N = 1,4 are solved for using the convergent values returned from PNOX and PCLOX for the odd nitrogen and odd chlorine species, respectively. An iteration counter KK is established and the previous values of H, OH, HO₂, and O₃ are saved for convergence testing. Subroutine SOLVE calls subroutine JACOB which organizes the coefficients of the system of chemical equations and calculates certain relevant production and loss terms. Production and loss terms are designated by double alphabetic variable names with a single subscript, while system coefficients to be solved by LINEQN are stored in the doubly subscripted array, A. Total production terms for a given species are subscripted variables PP while loss (sink) terms are subscripted variables SS. Table 4.4 presents a key to the variables defined in JACOB, identifying each by the corresponding reactions. Note that below 30 km O₃ is treated as a long-lived species, while at or above 30 km its equilibrium chemistry is treated explicitly. Subroutine JACOB returns to SOLVE where the net imbalance:

$$B(J,4) = PP(J) - SS(J)$$

is computed for H, OH, and HO₂ in addition to the cumulative error:

TABLE 4-4

CHEMICAL ORIGIN OF VARIABLES DESCRIBED IN SUBROUTINE JACOB

Variable	Definition	Reaction	
ALP	O/O_3	$O + O_2 + M \rightarrow O_3 + M$ $O_3 + h\nu \rightarrow O_2 + O$	$k = \text{RATE}(34)$ $J = JO3$
AA(1)	Production of H	$H_2 + O(^1D) \rightarrow OH + H$ $H_2O + h\nu \rightarrow OH + H$	$k = \text{RATE}(4)$ $J = JH20$
AA(2)		$OH + O \rightarrow H + O_2$	$k = \text{RATE}(19)$
AA(3)		$OH + CO \rightarrow H + CO_2$	$k = \text{RATE}(18)$
AA(4)		$OH + CH_4 \rightarrow H_2O + CH_3$	$k = \text{RATE}(21)$
AA(5)		$OH + H_2 \rightarrow H_2O + H$	$k = \text{RATE}(25)$
$PP(1) = AA(1) + AA(2) + AA(3) + AA(4) + AA(5)$			
BB(1)	Loss of H	$H + O_2 + M \rightarrow HO_2 + M$	$k = \text{RATE}(5)$
BB(2)		$H + O_3 \rightarrow OH + O_2$	$k = \text{RATE}(6)$
BB(3)		$H + HO_2 \rightarrow H_2 + O_2$ $\rightarrow 2OH$	$k = \text{RATE}(16)$ $k = \text{RATE}(17)$
$SS(1) = BB(1) + BB(2) + BB(3)$			
CC(1)	Production of OH	$H_2O + O(^1D) \rightarrow 2OH$	$k = \text{RATE}(2)$
CC(2)		$CH_4 + O(^1D) \rightarrow CH_3 + OH$	$k = \text{RATE}(3)$
CC(3)		$O + HO_2 \rightarrow OH + O_2$	$k = \text{RATE}(10)$
CC(4)		$HO_2 + O_3 \rightarrow OH + 2O_2$	$k = \text{RATE}(9)$
CC(5)		$NO + HO_2 \rightarrow NO_2 + OH$	$k = \text{RATE}(11)$
CC(6)		$H_2O_2 + h\nu \rightarrow 2OH$	$J = JH202$
CC(7)		$H + O_3 \rightarrow O_2 + OH$	$k = \text{RATE}(6)$
CC(8)		$HNO_3 + h\nu \rightarrow NO_2 + OH$	$J = JHNO3$
CC(9)		$H + HO_2 \rightarrow 2OH$	$k = \text{RATE}(17)$
$CC(10) = AA(1)$			
$PP(2) = CC(1) + CC(2) + CC(3) + CC(4) + CC(5) + CC(6) + CC(7) + CC(8) + CC(9) + CC(10)$			
DD(1)	Loss of OH	$OH + O_3 \rightarrow O_2 + HO_2$	$k = \text{RATE}(7)$
DD(2)		$H_2O_2 + OH \rightarrow H_2O + HO_2$	$k = \text{RATE}(8)$
DD(3)		$HO_2 + OH \rightarrow H_2O + O_2$	$k = \text{RATE}(14)$
$DD(4) = AA(3)$			
$DD(5) = AA(2)$			

TABLE 4-4 (Continued)

CHEMICAL ORIGIN OF VARIABLES DESCRIBED IN SUBROUTINE JACOB

<u>Variable</u>	<u>Definition</u>	<u>Reaction</u>	
DD(6)		$\text{OH} + \text{HCl} \rightarrow \text{H}_2\text{O} + \text{Cl}$	$k = \text{RATE}(20)$
DD(7)		$\text{OH} + \text{CH}_4 \rightarrow \text{CH}_3 + \text{H}_2\text{O}$	$k = \text{RATE}(21)$
DD(8)		$\text{OH} + \text{NO}_2 + \text{M} \rightarrow \text{HNO}_3 + \text{M}$	$k = \text{RATE}(22)$
DD(9)		$\text{HNO}_3 + \text{OH} \rightarrow \text{H}_2\text{O} + \text{NO}_3$	$k = \text{RATE}(23)$
DD(10)		$\text{OH} + \text{OH} \rightarrow \text{H}_2\text{O} + \text{O}$	$k = \text{RATE}(24)$
DD(11)		$\text{OH} + \text{H}_2 \rightarrow \text{H}_2\text{O} + \text{H}$	$k = \text{RATE}(25)$
$\text{SS}(2) = \text{DD}(1) + \text{DD}(2) + \text{DD}(3) + \text{DD}(4) + \text{DD}(5) + \text{DD}(6) + \text{DD}(7) + \text{DD}(8) + \text{DD}(9) + \text{DD}(10) + \text{DD}(11)$			
EE(1)	Production of HO_2	$\text{H} + \text{O}_2 + \text{M} \rightarrow \text{HO}_2 + \text{M}$	$k = \text{RATE}(5)$
EE(2)		$\text{OH} + \text{O}_3 \rightarrow \text{HO}_2 + \text{O}_2$	$k = \text{RATE}(7)$
EE(3)		$\text{Cl} + \text{H}_2\text{O}_2 \rightarrow \text{ClO} + \text{H}_2\text{O}$	$k = \text{RATE}(27)$
EE(4)	$= \text{DD}(2)$		
$\text{PP}(3) = \text{EE}(1) + \text{EE}(2) + \text{EE}(3) + \text{EE}(4)$			
GG(1)	Loss of HO_2	$\text{HO}_2 + \text{O}_3 \rightarrow \text{OH} + 2\text{O}_2$	$k = \text{RATE}(9)$
GG(2)	$= \text{CC}(3)$		
GG(3)	$= \text{CC}(5)$		
GG(4)		$\text{ClO} + \text{HO}_2 \rightarrow \text{HClO} + \text{O}_2$	$k = \text{RATE}(12)$
GG(5)		$\text{HO}_2 + \text{HO}_2 \rightarrow \text{H}_2\text{O}_2 + \text{O}_2$	$k = \text{RATE}(13)$
GG(6)	$= \text{DD}(3)$		
GG(7)		$\text{Cl} + \text{HO}_2 \rightarrow \text{HCl} + \text{O}_2$	$k = \text{RATE}(15)$
GG(8)	$= \text{BB}(3)$		
$\text{SS}(3) = \text{GG}(1) + \text{GG}(2) + \text{GG}(3) + \text{GG}(4) + \text{GG}(5) + \text{GG}(6) + \text{GG}(7) + \text{GG}(8)$			
PP(4)	Production of O	$\text{O}_2 + h\nu \rightarrow 2\text{O}$	$J = J02$
HH(1)	$= \text{BB}(2)$ Loss of Odd O		
HH(2)	$= \text{DD}(1)$		
HH(3)	$= \text{CC}(4)$		
HH(4)	$= \text{CC}(3)$		
HH(5)	$= \text{AA}(2)$		
HH(6)		$\text{NO}_2 + \text{O} \rightarrow \text{NO} + \text{O}_2$	$k = \text{RATE}(42)$
HH(7)		$\text{ClO} + \text{O} \rightarrow \text{Cl} + \text{O}_2$	$k = \text{RATE}(31)$
HH(8)		$\text{O} + \text{O}_3 \rightarrow 2\text{O}_2$	$k = \text{RATE}(35)$

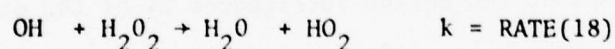
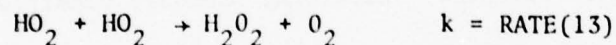
TABLE 4-4 (Continued)

CHEMICAL ORIGIN OF VARIABLES DESCRIBED IN SUBROUTINE JACOB

<u>Variable</u>	<u>Definition</u>	<u>Reaction</u>	
$SS(4) = HH(1) + HH(2) + HH(3) + HH(4) + HH(5) + HH(6) + HH(7) + HH(8)$			
COEFFICIENTS OF SYSTEM OF EQUATIONS			
$A(1,1) = - SS(1)/y(1)$			
$A(1,2) = (AA(2) + AA(3) + AA(4) + AA(5))/y(2)$			
$A(1,3) = -BB(3)/y(3)$			
$A(2,1) = (CC(7) + CC(9))/y(1)$			
$A(2,2) = -(SS(2) + DD(10))/y(2)$			
$A(2,3) = (CC(3) + CC(4) + CC(5) + CC(9) -DD(3))/y(3)$			
$A(3,1) = (EE(1) -GG(8))/y(1)$			
$A(3,2) = (EE(2) + EE(4) -GG(6))/y(2)$			
$A(3,3) = -(SS(3) + GG(5))/y(3)$			
At levels < 30 km $y(4) = 03(k)$			
At levels \geq 30 km:			
T1	Loss of O	$NO_2 + O \rightarrow NO + O_2$	$k = RATE(42)$
T2		$OH + O \rightarrow O_2 + H$	$k = RATE(19)$
T3		$HO_2 + O \rightarrow OH + O_2$	$k = RATE(10)$
T4		$O + ClO \rightarrow Cl + O_2$	$k = RATE(31)$
TT1 = (T1 +T2 + T3 + T4) ALP			
T5	Loss of O ₃	$H + O_3 \rightarrow OH + O_2$	$k = RATE(6)$
T6		$OH + O_3 \rightarrow HO_2 + O_2$	$k = RATE(7)$
T7		$HO_2 + O_3 \rightarrow OH + 2O_2$	$k = RATE(9)$
T8		$NO_2 + O_3 \rightarrow NO_3 + O_2$	$k = RATE(41)$
TT2 = T5 + T6 + T7 + T8			
B1 = TT1 + TT2			

$$ERR = \sum_{N=1}^3 \left(\frac{PP(N) - SS(N)}{SS(N)} \right)^2$$

Logical function LINEQN is called to solve the system of equations B where B(J,I) for J,I = 1,3 are the A(I,J) computed in JACOB using Gaussian elimination. If the matrix of coefficients is singular, values of H, OH, and HO₂ are scaled by a factor of 0.9 to remove the singularity and the calculation is repeated from the call to subroutine JACOB in statement 1 (This is permitted up to three times). If the parameter ERR is not less than 10⁻⁵ the concentrations are corrected by the magnitude of the net imbalance and the calculation is repeated from statement 1. (A maximum of 20 iterations are permitted.) If neither of the above error conditions occurs, the equilibrium concentrations of H, OH, HO₂ and O₃ have been found. The O concentration is computed using the parameter ALP from JACOB and the H₂O₂ concentration follows from the set of reactions:



$$H2O2 = RATE(13) * HO2 * HO2 / (RATE(8) * OH + JH2O2)$$

Subroutines PNOX and PCLOX are called to compute the apportionment of nitrogen and chlorine species. Finally, the old and new values of H, OH, HO₂, and O₃ are compared. If the solutions do not compare within 1/2%, the calculation is repeated. If the solution is found, however, subroutine JACOB is called again to recompute the production and loss terms given by its coefficients (for printing purposes at final solution). Subroutine SOLVE then returns the PHOCHM. This sequence is repeated for each 2 km level in the atmosphere.

4.4.3 Subroutine CFLOW: Long-lived Species

At this stage in the calculation, concentration profiles have been computed for the short-lived species, that is the individual members of the HO_x , NO_x and ClX families, which are consistent with calculated J-values and input profiles for the long-lived species. Upon returning to PHOCHM, the values of O_3 are saved for comparison and subroutine CFLOW is called to accomplish the evaluation of profiles for the long-lived species: N_2O , HO_x , NO_x , ClX , CH_4 , and O_3 below 30 km. In these cases (as discussed in Section 2) it is not adequate to equate production and loss processes at each level. These species, on the contrary, have longer chemical lifetimes and their profiles must be consistent both with chemical sources and sinks at each level and the gradient of vertical flux parameterized in terms of the eddy diffusion coefficient profile. The resultant equation which must be solved for the mixing ratio f_i as a function of z is of second order with coefficients given by the vertical profiles of both production and loss and the eddy coefficients. Therefore, boundary conditions at the top (designated U) and at the bottom (designated L) of the atmosphere must be specified. Certain basic coefficients are evaluated in entry SETUP 2 of subroutine SETUP (Section 4.3.2) which is called at the beginning of PHOCHM. These arrays are essentially the product NK which appears in the definition of vertical flux (equation 2.2) or in coding: $\text{CEK(I)} * \text{CDM(I)}$. Also, at the beginning of PHOCHM are definitions for the factors PPL , PPU , and QQU which are used to specify lower and upper boundary conditions. The program offers the versatility of specifying either flux (proportional to $\frac{df_i}{dz}$) or mixing ratio (i.e. f_i) boundary conditions, the basic relationship being in the form:

$$P_{L,U} \frac{df_i}{dz} + Q_{L,U} f_i = R_{L,U}$$

where f_i is the mixing ratio of the i th species at the lower (L) or upper (U) boundary. For example, if a fixed mixing ratio is to be specified at both boundaries, then $P_{L,U} = 0$, $Q_{L,U} = 1$ and $f_i = R_{L,U}$ where $R_{L,U}$ is the mixing ratio of the i th species at the lower and upper boundaries, respectively.

All of the cases in the program (subroutine CFLOW) use: $P_U = 1$, $Q_U = QQU * XL(N)$, $R_U = 0$. where $QQU = 6.0E + 05 / CEK(N) * CDM(N)$, $XL(N)$ is the loss frequency of level N , and $N = 81$ is the uppermost level or:

$$\frac{df_i}{dz} = Q_U f_i$$

for the upper boundary condition. The corresponding lower boundary condition is given by specifying R_L as either mixing ratio or flux:

(a) R_L (flux): $Q_L = 0.$, $P_L = PPL = -CEK(1) * CDM(1)$:

$$P_L \frac{df_i}{dz} = R_K$$

(b) R_L (mixing ratio): $Q_L = 1$, $P_L = 0$:

$$f_i = R_L$$

After CFLOW is called by PHOCHM, a series of layer interpolations is accomplished using subroutine RINTER for the species: DID, OH, HO2, NO2, NO, O3, CLO, CL, H, and H2O and photodissociation rates: CJN20, CJCF3, CJCF2, CJCH3C, CJO2, CJO3, and CJCCL4. RINTER increases the vertical resolution from 2 km to 1 km using square root interpolation. The next sequence in CFLOW is a series of subroutine calls to CSPEC, each of which provides the calculation of the flow dependent (but time independent) vertical profile of a particular species. A test on the magnitude of the specified lower boundary condition (given in BLOCK DATA or namelist; see Section 4.2, TABLE 4.2 LABELLED COMMON: RLOW) determines whether flux or mixing ratio has been specified (i.e. a value greater than 1.0 is a flux while one less than 1.0 is a mixing ratio.) The appropriate boundary condition parameter is then set ($Q = 0$. for flux; $Q = 1$. for mixing ratio) for the CSPEC calculation

The order in which the individual long-lived species are handled is as follows: N_2O , NO_x , CH_4 , $F11$, $F12$, CH_3Cl , CCl_4 , ClX , and H_2 . The arguments of subroutine CSPEC (see program listing, Appendix A) relate to the previous boundary conditions discussion and are in order: (P_U , R_U , P_L , Q_L , $RLOW$, DFP , XL , CXL). As noted above, the upper boundary conditions require $P_U = 1.$ and $R_U = 0.$ As can be seen from the listing, the first two arguments are 1. and 0., respectively. The quantity P_L is set equal to PPL (defined in (a) above) and CSPEC changes this to zero if Q_L is equal to one (for fixed lower boundary mixing ratio). The next argument is the lower boundary condition value (either flux or mixing ratio as given by Q_L). The term DFP is the time dependent term which is set equal to zero for the steady state case (in each CXL subroutine). XL is the loss frequency returned and CXL is a family of subroutines ($CXL1$, $CXL2$, etc.) which computes the level-by-level production PR and loss frequency and returns these values to CSPEC. As a reference, Table 4.5 identifies the particular species dependent reaction schemes relevant to each CXL subroutine. Next, CSPEC calls subroutine COEF which utilizes the level production and loss frequency data and the particular type of boundary conditions specified to compute the necessary coefficients to solve the system of equations resulting for a given species. The arrays AA(I) and T(I) used here can be found in SETUP2. Once, the relevant coefficients are evaluated, the system is solved by subroutine TRIDIA which computes the mixing ratio (X_i) profile for each species i. Finally, CSPEC calculates the net production and loss and returns this value (XL) to CFLOW:

$$XL = PR - XL * X$$

This procedure is carried out for each long-lived species with two exceptions. There is a convergence test for the solution of the NO_x profile

TABLE 4-5

SUBROUTINE FAMILY CXL

<u>Subroutine</u>	<u>Species</u>	<u>Production</u>	<u>Loss</u>
CXL1	N ₂ O	From Surface	$\text{N}_2\text{O} + \text{O}(^1\text{D}) \rightarrow \text{N}_2 + \text{O}_2$ $\rightarrow 2\text{NO}$
CXL2	NO _x	$\text{N}_2\text{O} + \text{O}(^1\text{D}) \rightarrow 2\text{NO}$	$\text{N}_2\text{O} + h\nu \rightarrow \text{N}_2 + \text{O}$ $\text{NO} + h\nu \rightarrow \text{N} + \text{O}$ $\text{N} + \text{NO} \rightarrow \text{N}_2 + \text{O}$
CXL3	CH ₄	From Surface	$\text{CH}_4 + \text{O}(^1\text{D}) \rightarrow \text{CH}_3 + \text{OH}$ $\text{CH}_4 + \text{OH} \rightarrow \text{CH}_3 + \text{CH}_3 + \text{H}_2\text{O}$ $\text{CH}_4 + \text{Cl} \rightarrow \text{CH}_3 + \text{HCl}$
CXL4	CFC1 ₃	From Surface	$\text{CFC1}_3 + h\nu \rightarrow \text{CFC1}_2 + \text{Cl}$ $\text{CFC1}_3 + \text{O}(^1\text{D}) \rightarrow \text{PRODUCTS}$
CXL5	CF ₂ Cl ₂	From Surface	$\text{CF}_2\text{Cl}_2 + h\nu \rightarrow \text{CF}_2\text{Cl} + \text{Cl}$ $\text{CF}_2\text{Cl}_2 + \text{O}(^1\text{D}) \rightarrow \text{PRODUCTS}$
CXL6	CH ₃ Cl	From Surface	$\text{CH}_3\text{Cl} + h\nu \rightarrow \text{CH}_3 + \text{Cl}$ $\text{CH}_3\text{Cl} + \text{OH} \rightarrow \text{CH}_2\text{Cl} + \text{H}_2\text{O}$
CXL7	ClX	$\text{CFC1}_3 + h\nu \rightarrow \text{CFC1}_2 + \text{Cl}$ $\text{CF}_2\text{Cl}_2 + h\nu \rightarrow \text{CF}_2\text{Cl} + \text{Cl}$ $\text{CH}_3\text{Cl} + h\nu \rightarrow \text{CH}_3 + \text{Cl}$ $\text{CCl}_4 + h\nu \rightarrow \text{CCl}_3 + \text{Cl}$	
CXL8	O ₃	$\text{O}_2 + h\nu \rightarrow 2\text{O}$ $\text{HO}_2 + \text{NO} \rightarrow \text{OH} + \text{NO}_2$	$\text{HO}_2 + \text{O}_3 \rightarrow \text{OH} + 2\text{O}_2$ $\text{OH} + \text{O}_3 \rightarrow \text{HO}_2 + \text{O}_2$ $\text{NO}_2 + \text{O} \rightarrow \text{NO} + \text{O}_2$ $\text{HO}_2 + \text{O} \rightarrow \text{OH} + \text{O}_2$ $\text{OH} + \text{O} \rightarrow \text{H} + \text{O}_2$ $\text{ClO} + \text{O} \rightarrow \text{Cl} + \text{O}_2$ $\text{O} + \text{O}_3 \rightarrow 2\text{O}_2$ $\text{NO}_2 + \text{O}_3 \rightarrow \text{NO}_3 + \text{O}_2$
CXL9	CCl ₄	From Surface	$\text{CCl}_4 + h\nu \rightarrow \text{CCl}_3 + \text{Cl}$
CXL11	H ₂	$\text{H}_2\text{O} + \text{O}(^1\text{D}) \rightarrow 2\text{OH}$ $\text{H} + \text{HO}_2 \rightarrow \text{H}_2 + \text{O}_2$	$\text{Cl} + \text{H}_2 \rightarrow \text{HCl} + \text{H}$ $\text{OH} + \text{H}_2 \rightarrow \text{H}_2\text{O} + \text{H}$ $\text{H}_2 + \text{O}(^1\text{D}) \rightarrow \text{OH} + \text{H}$

above level 40 (39 km) where the mixing ratio profile for NO_x is given by X2. Additionally, the calculations for O3 are limited to the region from the surface to 30 km above which it is considered short-lived. There is also a convergence test for O3 whose mixing ratio profile is given by X8. If convergence is reached, subroutine REPCN is called which repeats the calculation of NO_x and ClX apportionment using the new O3 values below 30 km by calling PNOX and PC1OX. The values of ClO and NO2 are compared and if they have not converged, the O3 computations are repeated using the new ClX, NOX values. If convergence is reached, the values of the concentration profiles are computed from the resultant mixing ratios for NOX, CH4, CLX, H2, and O3 ($z \leq 30$ km), and control is returned to PHOCHM.

4.4.4 Final Convergence Testing

After return from CFLOW, the calculation is complete except for final verification of convergence. First, the previous O3 values from the short-lived calculation and those resulting from the long-lived calculation are averaged for a new profile. This is to help quicker convergence. Second, previous J values are saved since new ones (consistent with the new species profiles) will be computed for comparison. RJITER is called to accomplish this.

The final comparison is made level by level between previous and new JO3 and OH values. An accuracy of 1/10% is accepted in the latter. If not achieved, the program is directed back to statement 10 in PHOCHM which increments the iteration index by one and restarts the calculation. After successful accomplishment of the desired accuracy, the program computes the integrated O3 density (O3INT) and the integrated odd O loss from levels 9-36 (by calling O3LINT). Finally, the major output subroutine PRINTX is called before the program is terminated.

4.5 Subroutine PRINTX: Output Profiles

Before terminating a particular run PHOCHM calls subroutine PRINTX. For each case run, thirteen pages of results are generated. (There are also a few pages of input parameters to identify the case printed out. See sample test cases Appendix C.) The beginning of the output is identifiable by the keyword RUN printed on a separate page.

Pages 1 and 2 of the output print J-values used in the final iteration of PHOCHM. They are headed with the note: "LAST ITERATION = I" where I is the final iteration index from PHOCHM. Page 1 gives the vertical profiles of the J values: CJ02, CJ03, CJCF2, CJCF3, CJ031 and in addition gives the O_3 number density, integrated O_3 , integrated total number density, and the OH number density for the previous iteration. Page 2 gives the profiles of the J values: CJCL03, CJN20, CJHNO3, CJH202, CJN205, CHCCL4, and CJCH3CL.

Pages 3-4 labelled "LAST ITERATION + 1" refer to results for the computation of J values using the final program results. Page 5 contains number densities of H, OH, HO2, H2O2, O, $O(^1D)$, and $O(^1S)$ in addition to the integrated O_3 density (HOX and odd oxygen families). Page 6 contains number densities of NO, NO2, HNO3, NO3, N2O5, and NOX (NOX family). Page 7 contains number densities and mixing ratios for CL, CLO, HCL, CLNO3, and CLX (CLX family).

Beginning on page 8 are level profiles of production and loss rates for particular reactions defined in PHOCHM and subroutine JACOB. (ref. Table 4-4). Page 8 in particular describes processes concerned with production and loss of odd oxygen. At the bottom of the page the integrated values of these rates are presented (they were calculated by O3LINT in PHOCHM). Page 9 gives the rates for reactives producing odd hydrogen in addition to the reaction $Cl + CH_4$. Page 10 gives the complementary losses of odd hydrogen.

Page 11 contains a listing of mixing ratio profiles for N₂O, NO_x, CH₄, FC11, FC12, CH₃C, CLX and CCL₄ and H₂. At the bottom of this page integrated fluxes for these long-lived species are provided by integrating the net production and loss terms from subroutines CXL using by a trapezoidal rule (subroutine TRAP). These should not differ substantially from the initial flux lower boundary conditions. Page 12 gives the mixing ratio of oxygen and the number densities of FC11, FC12, CH₃CL, CCL₄, and CLX. Page 13 continues with N₂O, NO_x, and CH₄.

If the keyword PARAMETERS appears next in the input stream to initialize constants for the next case to continue, the program is entered and the calculation repeated for the new case. However, the keyword ENDJOB will cause the program to print "NORMAL JOB END" and it will then terminate.

5. Users Guide

5.1 Program Initiation

The input deck required to initiate a model calculation using the CMSP program is relatively simple due to its modular, self-contained nature. As discussed in Section 4.2, the basic vertical profiles, wavelength dependent spectra, and rate constants required for the calculation are incorporated within BLOCK DATA and, consequently, need not be specified for each case (unless a change is desired.) Table 5-1 illustrates the configuration of the input deck which consists for the most part of keywords specification and a title to identify the output for the case run. For added versatility, however, the user can take advantage of the NAMELIST provision of subroutine INPARM in order to modify any of the listed (Table 5.2) variables for a particular case. For a single model run including one card of NAMELIST changes, a total of eight input cards are necessary. Note that multiple cases may be run by stacking cards 3-6 for each new case before the ENDJOB card.

5.2 Default Parameter Values

In addition to listing the parameters which may be changed during input by the NAMELIST provision, Table 5-2 provides the current BLOCK DATA provided default values and subroutine location of primary utilization for each variable. Generally, these parameters may be divided into two subgroups: (1) branching parameters which control the type of calculation being made, and (2) run variables which are input data to the calculation.

The primary branching parameters are: INSWIT, ISCAT, NEDDY, and ISIZE. These have been discussed in Section 4 under the headings of their respective subroutines.

The various run variables include rate constants (RA, RB), profile multiplicative constants (FCL, FH20, etc.), boundary condition data (RN20, RF11, etc.), and multiple scattering factors (=1.0, they are not used)

5.3 Aerosol Model Specification

As discussed in Section 3.1, the user may select one of four internal aerosol models by specifying the parameter ISIZE which chooses a set of optical constants (extinction and absorption coefficients) in subroutine QSCATT (Section 4.3.2). An additional provision allows the user to substitute another size distribution by using ISIZE = 5 and adding the necessary extinction QE(5,J) and absorption QA(5,J) coefficients as a function of wavelength ALAM(J) within the subroutine. The height distribution specified by IAERO (Table 3-1) will be utilized for either IAERO = 0 (23 km visibility) or IAERO = 1 (5 km visibility). This parameter is set in subroutine ALTGEN (Section 4.3.1). The height distribution may be changed by amending the BLOCK DATA array DA23.

TABLE 5-1

CMSP INPUT DECK CONFIGURATION

<u>Card Number</u>	<u>Description</u>	<u>Columns Used</u>
1	the word TITLE	1-5
2	any title desired	1-80
3	the word PARAMETERS	1-10
4	\$ INPUT	beginning in column 2
4a	as many cards as	
4b	necessary to input,	
.	in NAMELIST format	
.	any constants which	
.	differ from the de-	
.	fault values set in	
.	BLOCK DATA	
5	\$ END	beginning in column 2
6	the work RUN	1-3
.	(cards 3-6 may be repeated for any number of	
.	runs with changed constants)	
Last Card	the word ENDJOB	1-6

TABLE 5-2

PARAMETERS WHICH MAY BE SPECIFIED IN NAMELIST

Name	BLOCK DATA Default Value	Subroutine Used
FCL	1.0	INITAL
FCLNO3	1.0	PNOX
FH20	1.0	INITAL
FNO	1.0	(not used)
FKK	1.0	SETUP
I1	59	CPH11
P11	1.0	CPH11
P22	1.0	CPH11
PJO3	1.80×10^{-4}	JACOB
FJ	1.0	CXL
FJFC	1.0	CXL
TL	3.15×10^{13}	CXL
RN20	2.50×10^{-7}	CSPEC
RNOX	2.00×10^{10}	CSPEC
RCH4	1.50×10^{-6}	CSPEC
RF11	9.30×10^6	CSPEC
RF12	1.30×10^7	CSPEC
RCH3C	1.50×10^{-9}	CSPEC
RCLX	1.00×10^{10}	CSPEC
RCCL4	1.30×10^{-10}	CSPEC
NEDDY	0	SETUP
RO3	3.00×10^{-8}	CSPEC
SCNO2	1.0	PNOX
SCCLO3	1.0	COMPJ
SCH202	1.0	COMPJ
SCN205	1.0	COMPJ
PH20	0	CXL11
RH2	5.00×10^{-7}	CSPEC
LAT	30.	WEIGHT
DEL	0.	WEIGHT
JNO3	1.3×10^{-2}	PNOX
RA	} BLOCK DATA	RCONST
RB		RCONST
ISWIT	1	RJITER
ISIZE	4	QSCATT
ISCATT	1	RJITER
REF	0.2	VIM

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APPENDIX A
PROGRAM LISTING

PROGRAM MAIN(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT)	000100
.....	000110
.....CHLORINE MODEL STUDY PROGRAM - VERSION 5	000120
.....	000130
.....MAIN ROUTINE..READS KEYWORDS, CALLS SUBROUTINES	000140
.....	000150
.....VERSION 5.1	000160
.....E.R.T., INC.	000170
.....LEVEL 771001	000180
.....N.D.SZE, N.TPIOP, R.G. ISAACS, W.K. MURKE	000190
.....	000200
.....	000210
.....	000220
REAL TTTL(11),TITLE(6)	000230
INTEGER KEYS(10), XT(13)	000240
COMMON /HFA/ TITLE,ICONE,VERS,LEVEL,DATE,IRUN,NPAGE,NLOG	000250
*****	000260
DATA KEYS/41TTTL,3HRUN/	000270
.....	000280
.....	000290
ICONE=117	000310
VERS=5.1	000320
LEVEL=771001	000330
CALL DAY	000340
.....	000350
.....READ KEYWORDS	000360
.....	000370
100 CALL INPUT(KEYS,10,IC,IFORM,XT,<WN>),RETURNS(999)	000380
GO TO (200,250,700), KWN	000390
.....	000400
.....TITLE - TITLE FOR OUTPUT - INITIALIZE RUN	000410
.....	000420
200 READ(10,1) TTTL	000430
WRITE (6,3) TTTL	000440
CALL ALTGEN	000450
GO TO 100	000460
.....	000470
.....STEADY-STATE CALCULATIONS	000480
.....	000490
250 CALL PHOCHM	000500
GO TO 100	000510
.....	000520
700 GO TO 100	000530
.....	000540
999 WRITE (6,4)	000550
.....	000560
STOP	000570
1 FORMAT(10A8)	000580
3 FORMAT(//T10,10A8)	000590
4 FORMAT(//T10,* NORMAL JOB END.*)	000600
.....	000610
END	000620
SUBROUTINE ALTGEN	000630
.....	000640
.....CHLORINE MODEL STUDY PROGRAM	000650
.....	000660
.....SUBROUTINE ALTGEN - FILLS UP ALT(-) ARRAY	000670
.....	000680
.....VERSION 4.0	000690
.....E.R.T., INC.	000700
.....LEVEL 770214	000710
.....L.PEKRY, N.TPIOP	000720
.....	000730

COMMON /INTDEN/ DO3INT(41),DMINT(41),DAINT(41)	000730
COMMON /MODEL/ ALT(41),TEMP(41),DM(41),DIU(41),DA23(41)	000740
COMMON /SOLCON/ WL(100),FL(100),QO2(100),QO3(100)	000750
COMMON /SOLCON1/ QCF2(100),QCF3(100),QCCL4(100),QCH3C(100),	000750
X QCLNO3(100),QN2O(100),QHNO3(100),QM2O2(100),QN2O5(100),	000770
Y Q4CL(100),QH2CL(100),QNO2(100),QH2O(100)	000790
REAL DA05(3)	000790
DATA DA05/1.378E04,1.844E03,2.453E02/	000900
+++++	000310
ALT(1)=0.0	000320
DO 10 I=2,41	000930
10 ALT(I)=ALT(I-1)+2.0E5	000340
	000950
FL(29) = 1.09E+12	000960
FL(30) = 2.40E+12	000970
FL(31) = 3.75E+12	000980
FL(32) = 5.70E+12	000990
FL(33) = 1.47E+13	000300
FL(34) = 2.09E+13	000310
FL(35) = 2.59E+13	000320
FL(36) = 3.20E+13	000330
	000340
QC_NO3(33) = 3.48E-18	000350
QC_NO3(34) = 3.75E-18	000360
QC_NO3(35) = 3.76E-18	000370
QC_NO3(36) = 3.07E-18	000380
QC_NO3(37) = 2.31E-18	000390
QC_NO3(38) = 1.60E-18	001000
QC_NO3(39) = 1.18E-18	001010
QC_NO3(40) = 9.54E-19	001020
QC_NO3(41) = 6.57E-19	001030
QC_NO3(42) = 5.09E-19	001040
QC_NO3(43) = 5.09E-19	001050
QC_NO3(44) = 4.07E-19	001060
QC_NO3(45) = 3.28E-19	001070
QC_NO3(46) = 2.61E-19	001080
QC_NO3(47) = 2.02E-19	001090
QC_NO3(48) = 1.45E-19	001100
QC_NO3(49) = 1.05E-19	001110
QC_NO3(50) = 7.34E-20	001120
QC_NO3(51) = 5.10E-20	001130
QC_NO3(52) = 3.90E-20	001140
QC_NO3(53) = 2.89E-20	001150
QC_NO3(54) = 2.02E-20	001160
QC_NO3(55) = 1.49E-20	001170
QC_NO3(56) = 1.07E-20	001180
QC_NO3(57) = 9.00E-21	001190
QC_NO3(58) = 5.10E-21	001200
QC_NO3(59) = 4.80E-21	001210
QC_NO3(60) = 3.80E-21	001220
QC_NO3(61) = 3.20E-21	001230
QC_NO3(62) = 2.90E-21	001240
QC_NO3(63) = 2.60E-21	001250
QC_NO3(64) = 2.30E-21	001260
QC_NO3(65) = 2.10E-21	001270
QC_NO3(66) = 1.90E-21	001280
QC_NO3(67) = 1.70E-21	001290
QC_NO3(68) = 1.50E-21	001300
QC_NO3(69) = 1.30E-21	001310
QC_NO3(70) = 1.10E-21	001320
QC_NO3(71) = 9.7E-22	001330
QC_NO3(72) = 4.0E-21	001340
	001350
	001360
AEROSOL HEIGHT MODEL IAERO=0(23KM), =1(5KM)	001370
COMPUTE INTEGRATED AEROSOL DEFENSITY	001380

	IAERO=0	001390
	IF(IAERO.EQ.0)GO TO 16	001400
	DO 15 J=1,3	001410
15	DA23(J)=DA05(J)	001420
16	NT = 41	001430
	DAINT(NT)=DA23(NT)*3.78E05	001440
	NTM1 = NT - 1	001450
	DELZ = 2.0E05	001460
	DMINT(NT) = DM(NT) * 5.0E05	001470
	DO 20 J = 1,NTM1	001480
	I = NT - J	001490
	IP1 = I + 1	001500
	DAINT(I)=DAINT(IP1)+(DA23(IP1)+DA23(I))*DELZ*.5	001510
20	DMINT(I) = DMINT(IP1) + (DM(IP1) + DM(I)) * DELZ*.5	001520
		001530
	CALL PAGE	001540
		001550
	WRITE (6,601)	001560
	WRITE (6,602) (J,WL(J),FL(J),Q02(J),Q03(J),QCF2(J),QCF3(J),	001570
1	QCCL4(J),QCH3C(J),J=1,99)	001580
	CALL PAGE	001590
	WRITE (6,603)	001600
	WRITE (6,604) (J,WL(J),FL(J),QCLN03(J),QN20(J),QHN03(J),QM202(J),	001610
1	QN205(J),J=1,99)	001620
		001630
601	FORMAT(1H0,12X,*WL*,11X,*FL*,10X,*Q02*,10X,*Q03*,10X,*QCF2*, 9X,	001640
1	*QCF3*, 8X,*QCCL4*, 8X,*QCH3C*/)	001650
602	FORMAT (1H ,I5,1P8E13.4)	001660
603	FORMAT (1H0,12X,*WL*,11X,*FL*, 3X,*QCLN03*, 8X,*QN20*, 8X,*QM202*,	001670
1	8X,*QN205*/)	001680
604	FORMAT (1H ,I5,1P7E13.4)	001690
		001700
	RETURN	001710
	END	001720
	SUBROUTINE INPARM	001730
		001740
	001750
	C.....CMS04 - CHLORINE MODEL STUDY PROGRAM	001760
		001770
	C.....SUBROUTINE INPARM - READS AND WRITES RUN VARIABLES	001780
		001790
	C.....VERSION 4.0 LEVEL 770214	001800
	C.....E.R.T.,INC. N.TRIPP	001810
		001820
	001830
		001840
	COMMON /EDDY/ FKK,I1,P11,P22,NEJ0Y	001850
	COMMON /MSCAT/ SCN02,SCCL03,SCH202,SCN205	001860
	COMMON /MO_4YD/ XH(81),XH20(81),PH20,RH2,X11(81)	001870
	COMMON /PARM/ ISMIT,ISTEP,ISTOP,TLOOP,ITPRN,ISIZE,ISCAT	001880
	REAL JN03	001890
	COMMON /RATES/ RATE(65,81),RA(65),RB(65),JN03,PJ03	001900
	COMMON /SFACT/ FCL,FH20,FCLN03,FNO	001910
	COMMON /RLOW/ RN20,RNOX,RCH4,RF11,RF12,RCH32,RCLX,RCCL4,R03	001920
	COMMON /SPEC04/ FJ,FJFC,TL	001930
	REAL LAT	001940
	COMMON /MT/ A(6),DL,LAT,DEL	001950
	COMMON /PARA/ U0,N,N1,N2,NN,NNP1,REF	001960
		001970
	NAMES LIST /INPUT/ FCL,FCLN03,FH20,FNO,FKK,I1,P11,P22,PJ03,ISMIT,	001980
1	FJ,FJFC,TL,RN20,RNOX,RCH4,RF11,RF12,RCH3C,RCLX,RCCL4,	001990
2	NEJ0Y,R03,SCN02,SCCL03,SCH202,SCN205,PH20,RH2,LAT,DEL,JN03,RA,RB	002000
3	,ISIZE,ISCAT,REF	002010
	READ (5,INPUT)	002020
		002030
	CALL PAGE	002040


```

      IF (ISMIT.EQ.0) WRITE(6,510) ISMIT                                002050
510  FORMAT (1H0,3X, *FIXED SUN ANGLE MODEL - IS4ITCH =*,I2)          002060
      IF (ISMIT.EQ.1) WRITE(6,511) ISMIT                                002070
511  FORMAT (1H0,3X,*24 HOUR AVERAGED) MODEL - IS4ITCH =*,I2)        002080
C                                                                           002090
      CALL WEIGHT                                                         002100
      WRITE (6,514) LAT,DEL,A,DL                                         002110
514  FORMAT (1H0/4X,*COMTAU FACTORS FOR THIS RUNI*/4X,*FOR LATITUDE =* 002120
1,F5.1,* & SOLAR DECLINATION =*,F6.1,3X,*A*S =*,6(F5.4,*,*)/        002130
2 55X,*DL =*,F9.1,* SECS.*)                                             002140
      IF (ISCATT.EQ.0) GO TO 10                                           002150
      WRITE(6,520) ISCATT                                                002160
520  FORMAT(1H0/,4X,*MULTIPLE SCATTERING CALCULATION, ISCATT=*,I2)    002170
      CALL PAGE                                                           002180
      CALL QSCATT                                                         002190
10  CONTINUE                                                             002200
C                                                                           002210
      WRITE (6,504)                                                       002220
504  FORMAT (1H0/4X,*FLUXES AND MIXING RATIOS FOR THIS RUNI*)          002230
      WRITE (6,505) RN20,RNOX,RCH4,RFL1,RF12,RCH3,RCLX,RCL4,R03,RH2    002240
506  FORMAT (1H0,3X,*RN20 =*,1PE9.2,2X,*RNOX =*,E9.2,2X, *RCH4 =*,E9.2,002250
1      2X,*RF11 =*,E9.2,2X,*RF12 =*,E9.2,2X,*RCH3C =*,E9.2,002260
2      2X,*RCLX =*,E9.2/ 4X,*RCCL4 =*,E9.2,2X,*R03= *,E9.2,002270
3      2X,*RH2 =*,E9.2)                                                 002280
      WRITE (6,505) JN03,PJ03,PH20                                       002290
505  FORMAT (1H0/4X,*JN03 =*,1PE9.2,4X,*PJ03 =*,E9.2,4X,*PH20 =*,E9.2) 002300
C                                                                           002310
      WRITE (6,500)                                                       002320
500  FORMAT (1H0/4X,*S-FACTORS FOR THIS RUNI*)                         002330
      WRITE (6,501) FCL,FCLN03,FH20,FNO                                002340
501  FORMAT(1H0,3X,*FCL =*,F5.2,2X,*FCLN03 =*,F5.2,2X,*FH20 =*,F5.2, 002350
1 2X,*FNO =*,F5.2)                                                       002360
C                                                                           002370
      WRITE (6,512)                                                       002380
512  FORMAT (1H0/,4X,*MULTIPLE SCATTERING FACTORS FOR THIS RUNI*)     002390
      WRITE (6,513) SCN02,SCCL03,SCN202,SCN205                         002400
513  FORMAT (1H0,3X,*SCN02 =*,F5.2,2X,*SCC.03 =*,F5.2,2X,*SCH202 =*, 002410
1 F5.2,2X,*SCN205 =*,F5.2)                                             002420
C                                                                           002430
      CALL CPHI1 (P11,P22,I1)                                           002440
C                                                                           002450
      CALL SETUP (STEP,31)                                               002460
C                                                                           002470
      CALL RCONST                                                         002480
      RETURN                                                             002490
      END                                                                002500
      SUBROUTINE SETUP (STEP,N)                                           002510
C.....CHS03 - CHLORINE MODEL STUDY PROGRAM                             002520
C                                                                           002530
C.....CHS03 - CHLORINE MODEL STUDY PROGRAM                             002540
C                                                                           002550
C SUBROUTINE SETUP TO TRANSFER RAW DATA WITH 41 LEVELS TO A SET OF    002560
C NEW DATA WITH 81 LEVELS                                             002570
C ENTRY SETUP2 TO COMPUTE CERTAIN BASIC COEFFICIENTS                   002580
C                                                                           002590
C.....VERSION 3.2              LEVEL 761222                             002600
C.....F.R.F.,INC.              N.O.SIZE, N.TRI*P                       002610
C                                                                           002620
C.....CHS03 - CHLORINE MODEL STUDY PROGRAM                             002630
C                                                                           002640
      COMMON /COEF1/AA(81),BB(81),CC(81),DL(81),DU(81),U(81)          002650
      COMMON /EDDY/ FKK,I1,P11,P22,NEJDY                                002660
      COMMON /MODEL/ ALT(41),TEMP(41),DH(41),DID(41),DA23(41)          002670
      COMMON /NDATA/ CEK(81),CDM(81),CTEMP(81),CDA(81)                 002680
      COMMON /TFCIR/ FT,FA,FB,FH                                         002690
      REAL EK(41),E(81)                                                  002700

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3 HUNTER'S EDDY DIFFUSION COEFFICIENTS (MODIFIED) - UP TO 50 KMS. 002710
  DATA EK/10.00,10.00,10.00,10.00,10.00,3.00,3.00,3.00,0.26,0.33, 002720
  10.42,0.53,0.66,0.83,1.01,1.30,1.60,2.05,2.55,3.20,4.00,5.00,6.40, 002730
  28.00,10.00,12.80,16.00,20.00,25.00,31.00,38.00,50.00,62.00,75.00, 002740
  396.00,120.00,150.00,190.00,240.00,300.00,380.00/ 002750
  IF (NEDDY.E1.1) CALL EDC1 (EK) 002760
  IF (NEDDY.E1.2) CALL EDC2 (EK) 002770
  DO 10 I=1,41 002780
  J=2*I-1 002790
  CEK(J)=EK(I)*1.0E 4*FKK 002800
  CDM(J)=DM(I) 002810
  CDA(J)=DA23(I) 002820
10 CTEMP(J)=TEMP(I) 002830
  DO 15 I=1,40 002840
  J=2*I 002850
  IP1=I+1 002860
  CEK(J)=SQRT(EK(I)*EK(IP1))*1.0E 4*FKK 002870
  CDM(J)=SQRT(DM(I)*DM(IP1)) 002880
  CDA(J)=SQRT(DA23(I)*DA23(IP1)) 002890
15 CTEMP(J)=SQRT(TEMP(I)*TEMP(IP1)) 002900
  CALL PAGE 002910
  IF (NEDDY.E1.0) WRITE (6,60) FKK 002920
  IF (NEDDY.E1.1) WRITE (6,61) FKK 002930
  IF (NEDDY.E1.2) WRITE (6,62) FKK 002940
  WRITE (6,65) 002950
  WRITE (6,65) (I,ALT(I),CEK(2*I-1),CDM(2*I-1),CTEMP(2*I-1), 002960
  1 CDA(2*I-1),I=1,41) 002970
60 FORMAT (1H0,9X,*FKK =*,F5.2,*, FACTOR MULTIPLYING HUNTER'S EDDY DI 002980
  1FFJSION COEFFICIENTS*) 002990
61 FORMAT (1H0,9X,*FKK =*,F5.2,*, FACTOR MULTIPLYING ANALYTIC EDDY DI 003000
  1FFJSION COEFFICIENTS*) 003010
62 FORMAT (1H0,9X,*FKK =*,F5.2,*, FACTOR MULTIPLYING CLANG 'S EDDY DI 003020
  1FFJSION COEFFICIENTS*) 003030
65 FORMAT (1H0/10X,*ALT*,10X,*EK*,13X,*DM*,11X,*TEMP*,13X,*DA*/) 003040
66 FORMAT (2X,I2,0PF11.0,1P2E15.4,0PF11.2,1PE15.4) 003050
  RETURN 003060
C 003070
  ENTRY SETUP2 003080
  NM1=N-1 003090
  NM2=N-2 003100
  DT=3.15576E7*STEP 003110
  DO 32 I=1,N 003120
  E(I)=CEK(I)*CDM(I) 003130
32 U(I)=0.5E-10*DT/CDM(I) 003140
  DO 33 I=2,N+1 003150
33 CC(I)=SQRT(E(I+1)*E(I)) 003160
  DO 34 I=2,N+2 003170
34 BB(I+1)=CC(I) 003180
  BB(2)=SQRT(E(2)*E(1)) 003190
  DO 35 I=2,N+1 003200
35 AA(I)=CC(I)+BB(I) 003210
  DO 40 I=2,N+1 003220
  DL(I)=U(I)*BB(I)*FA 003230
40 DU(I)=U(I)*CC(I)*FA 003240
  RETURN 003250
  END 003260
  SUBROUTINE WEIGHT 003270
3 ..... 003280
3 ..... 003290
3.....CHS03 - CHLORINE MODEL STUDY PROGRAM 003300
C ..... 003310
3.....VERSION 3.3 LEVEL 770201 003320
C.....E.R.T.,INC. N.D.SZE, N.TRI>P 003330
C ..... 003340
C ..... 003350
3 ..... 003360

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REAL LAT	003370
COMMON /WT/ A(6),DL,LAT,DEL	003380
DIMENSION T(6)	003390
DATA DTOR,RTOD/.01745329,57.29579/	003400
C	003410
LAT = LAT * DTOR	003420
DEL = DEL * DTOR	003430
X1 = COS(LAT) * COS(DEL)	003440
X2 = SIN(LAT) * SIN(DEL)	003450
DDL = ACOS(-TAN(LAT)*TAN(DEL))	003460
DDL = 240. * DDL * RTOD	003470
DT = DDL/6.	003480
DO 10 I = 1,6	003490
T(I) = DT/2. + (I-1)*DT	003500
T(I) = (T(I)/240.) * DTOR	003510
COSANG = X1*COS(T(I)) + X2	003520
10 A(I) = 1.0/COSANG	003530
DL = 2.*DDL	003540
LAT = LAT * RTOD	003550
DEL = DEL * RTOD	003560
RETURN	003570
END	003580
SUBROUTINE CP4I1 (P11,P22,I1)	003590
COMMON /PHIS/ PHI1(100)	003600
C	003610
DO 10 J = 1,I1	003620
10 PHI1(J) = P11	003630
C	003640
I11 = I1 + 1	003650
DO 20 J = I11,72	003660
20 PHI1(J) = P22	003670
C	003680
RETURN	003690
END	003700
SUBROUTINE EDC1 (EK)	003710
C	003720
C ANALYTIC EDDY DIFFUSION COEFFICIENTS (* 1.E-4)	003730
DIMENSION E(41)	003740
DO 10 I=1,5	003750
10 EK(I)=10.	003760
EK(6)=3.	003770
EK(7)=3.	003780
EK(8)=3.	003790
DO 20 I=9,41	003800
20 EK(I)=.35*EXP((2*(I-1)-14)/9.55)	003810
RETURN	003820
END	003830
SUBROUTINE EDC2 (EK)	003840
C	003850
C CHANG'S EDDY DIFFUSION COEFFICIENTS - UP TO 50 KMS.(* 1.E-4)	003860
C	003870
DIMENSION E(41),CK(41)	003880
DATA CK/6*30.,	003890
1 1.0,1.2,.97,.74,.60,.50,.42,.39,.37,.37,.39,.42,.50,.61,.80,	003900
2 1.1,1.5,2.2,3.3,5.4,9.2,17.,29.,49.,90.,155.,9*230./	003910
C	003920
DO 10 I = 1,41	003930
10 EK(I) = CK(I)	003940
RETURN	003950
END	003960
SUBROUTINE RCONST	003970
C.....	003980
C.....	003990
C.....CMS04 - CHLORINE MODEL STUDY PROGRAM	004000
C	004010
C.....SUBROUTINE RCONST - CALCULATES REACTION RATES FOR PROGRAM	004020

CVERSION 4.0	LEVEL 770214	004030
CE.R.T., INC.	N.O.SZE, N.TRIPP	004040
C		004050
C		004060
C		004070
C		004080
	COMMON /NDATA/ CEK(81),CDM(81),CTEMP(81),CDA(81)		004090
	REAL JN03		004100
	COMMON /RATES/ RATE(65,81),RA(65),RB(65),JN03,PJ03		004110
	DIMENSION REACT1(7,9),REACT2(7,9),REACT3(7,9),		004120
1	REACT4(7,9),REACT5(7,9),REACT6(7,9),REACTS(7,63)		004130
	EQUIVALENCE (REACTS(1,1),REACT1(1,1)),		004140
1	(REACTS(1,10),REACT2(1,1)),		004150
2	(REACTS(1,19),REACT3(1,1)),		004160
3	(REACTS(1,28),REACT4(1,1)),		004170
4	(REACTS(1,37),REACT5(1,1)),		004180
5	(REACTS(1,46),REACT6(1,1))		004190
	DATA REACT1/4H0H +,4H CH3,4HCL ,4H =,4H CH2,4HCL +,4H H2O,		004200
2	4H2O ,4H+ O(,4H'D) ,4H =,4H 2OH,4H ,4H ,		004210
3	4HCH4 ,4H+ O(,4H'D) ,4H =,4H CH3,4H + 3,4HH ,		004220
4	4HH2 +,4H O(,4H'D) ,4H =,4H 2H ,4H+ 1 ,4H ,		004230
5	4HH + ,4H02 +,4H M ,4H =,4H 102,4H + 1,4H ,		004240
6	4HH + ,4H03 ,4H ,4H =,4H 2H ,4H+ 22,4H ,		004250
7	4H0H +,4H 03 ,4H ,4H =,4H 102,4H + 3,4H2 ,		004260
8	4H0H +,4H H2O,4H2 ,4H =,4H 120,4H + 1,4H02 ,		004270
9	4H02 ,4H+ 03,4H ,4H =,4H 2H ,4H+ 23,4H2 /		004280
	DATA REACT2/4HH02 ,4H+ O ,4H ,4H =,4H 2H ,4H+ 22,4H ,		004290
2	4HH02 ,4H+ NO,4H ,4H =,4H 2H ,4H+ 13,4H2 ,		004300
3	4HH02 ,4H+ CL,4H0 ,4H =,4H 1CL,4H0 + ,4H02 ,		004310
4	4HH02 ,4H+ HO,4H2 ,4H =,4H 120,4H2 + ,4H02 ,		004320
5	4HH02 ,4H+ OH,4H ,4H =,4H 120,4H + 3,4H2 ,		004330
6	4HH02 ,4H+ CL,4H ,4H =,4H HCL,4H + 3,4H2 ,		004340
7	4HH + ,4HH02 ,4H ,4H =,4H 12 ,4H+ 22,4H ,		004350
8	4HH + ,4HH02 ,4H ,4H =,4H 20H,4H ,4H ,		004360
9	4H0H +,4H CO ,4H ,4H =,4H 1 +,4H CO2,4H /		004370
	DATA REACT3/4H0H +,4H O ,4H ,4H =,4H 1 +,4H O2 ,4H ,		004380
2	4H0H +,4H HCL,4H ,4H =,4H 120,4H + 3,4H2 ,		004390
3	4H0H +,4H CH4,4H ,4H =,4H 120,4H + 3,4HH3 ,		004400
4	4H0H +,4H NO2,4H + 1,4H =,4H 1NO,4H3 + ,4HH ,		004410
5	4H0H +,4H HNO,4H3 ,4H =,4H 120,4H + 1,4H03 ,		004420
6	4H0H +,4H OH ,4H ,4H =,4H 120,4H + 3,4H ,		004430
7	4H0H +,4H H2 ,4H ,4H =,4H 120,4H + 1,4H ,		004440
8	4HCL +,4H H2 ,4H ,4H =,4H 1CL,4H + 1,4H ,		004450
9	4HCL +,4H H2O,4H2 ,4H =,4H HCL,4H + 1,4H02 /		004460
	DATA REACT4/4HCL +,4H NO,4H2 + ,4HH =,4H 2LN,4H03 +,4H M ,		004470
2	4HCL +,4H 03 ,4H ,4H =,4H 2LO,4H + 3,4H2 ,		004480
3	4HCL +,4H CH4,4H ,4H =,4H 1CL,4H + 3,4HH3 ,		004490
4	4HCL +,4H O ,4H ,4H =,4H 2L ,4H+ 22,4H ,		004500
5	4HCL +,4H NO,4H ,4H =,4H 2L ,4H+ 13,4H2 ,		004510
6	4H0 + ,4HHCL ,4H ,4H =,4H 2H ,4H+ 2L,4H ,		004520
7	4H0 + ,4H02 +,4H M ,4H =,4H 23 ,4H+ 1 ,4H ,		004530
8	4H0 + ,4H03 ,4H ,4H =,4H 202,4H ,4H ,		004540
9	4H02 ,4H+ NO,4H3 ,4H =,4H 120,4H5 ,4H /		004550
	DATA REACT5/4H2O5,4H* ,4H ,4H =,4H 102,4H + 1,4H03 ,		004560
2	4H2O5,4H* + ,4HH ,4H =,4H 120,4H5 + ,4HH ,		004570
3	4H2O5,4H + M,4H ,4H =,4H 120,4H5 + ,4H M ,		004580
4	4HNO +,4H 03 ,4H ,4H =,4H 102,4H + 3,4H2 ,		004590
5	4HNO2 ,4H+ 03,4H ,4H =,4H 103,4H + 3,4H2 ,		004600
6	4HNO2 ,4H+ O ,4H ,4H =,4H 10 ,4H+ 22,4H ,		004610
7	4H2O ,4H+ O(,4H'D) ,4H =,4H 12 ,4H+ 22,4H ,		004620
8	4H2O ,4H+ O(,4H'D) ,4H =,4H 2NO,4H ,4H ,		004630
9	4HH + ,4HNO ,4H ,4H =,4H 12 ,4H+ 3 ,4H /		004640
	DATA REACT6/4H + ,4H02 ,4H ,4H =,4H 10 ,4H+ 3 ,4H ,		004650
2	4H0(,4H'D) + ,4HCFCL,4H3 =,4H PRO,4H0UCL,4H5 ,		004660
3	4H0(,4H'D) + ,4HCFCL,4H3 =,4H PRO,4H0UCL,4H5 ,		004670
4	4H0(,4H'D) + ,4HCH3C,4H2L =,4H 2H ,4H+ 24,4H2C. ,		004680


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5          4H0(*0,4H) + ,4HCCL4,4H =,4H PRO,4HDOCT,4HS , 004690
6          4H0(*0,4H) + ,4HM ,4H =,4H J +,4H M ,4H , 004700
A 21*1H / 004710
C 004720
C SET UP RATES ARRAY FOR 65 REACTIONS 004730
DO 10 I = 1,65 004740
DO 10 J = 1,81 004750
10 RATE (I,J) = RA(I) * EXP(RB(I)/TEMP(J)) 004760
C 004770
C RE-CALCULATE RATE CONSTANTS THAT DO NOT FIT ABOVE FORMULA 004780
DO 20 J = 1,81 004790
RATE(22,J) = 2.3E-13*EXP(880./TEMP(J))/(2.6E16+CON(J)) 004800
RATE(37,J) = 1.0E+08*CON(J)/(2.6E19+CON(J)) + 1.0E7 004810
20 CONTINUE 004820
C 004830
C PRINT OUT ALL REACTIONS AND RATE CONSTANTS A & B 004840
CALL PAGE 004850
WRITE (6,600) 004860
600 FORMAT (1H0,3X,*REACTION RATE (AS A FUNCTION OF ALTITUDE, Z) = A * 004870
1,11*,* EXP(3/TEMP(Z))*/4X,*NO.*,15X,*REACTION*,17X,*A*,11X,*B*/) 004880
C 004890
DO 30 I = 1,21 004900
30 WRITE (6,601) I,(REACTS(N,I),N=1,7),RA(I),R3(I) 004910
601 FORMAT (1H ,15,4X,7A4,1PE13.2,03F11.0) 004920
DO 40 I = 23,36 004930
40 WRITE (6,601) I,(REACTS(N,I),N=1,7),RA(I),R3(I) 004940
DO 50 I = 39,51 004950
50 WRITE (6,601) I,(REACTS(N,I),N=1,7),RA(I),R3(I) 004960
C 004970
C PRINT EXCEPTIONAL CASES 004980
WRITE (6,602) (REACTS(N,22),N=1,7) 004990
1, (REACTS(N,37),N=1,7) 005000
602 FORMAT (1H0,3X,*REACTIONS WHOSE RATES ARE CALCULATED BY DIFFERENT 005010
1 FORMULAE ARE:*/
2 4X,*22*,4X,7A4,5X,*R = 2.3E-13*,1H*, 005020
3 *EXP(880./TEMP(Z))/(2.6E16 + M(Z))*/ 005030
4 4X,*37*,4X,7A4,5X,*R = 1.0E+08*,1H*, 005040
5 *M(Z)/(2.6E19+M(Z)) + 1.0E7*/ 005050
RETURN 005060
END 005070
SUBROUTINE PHOCHM 005080
005090
005100
005110
005120
005130
005140
005150
005160
005170
005180
005190
005200
005210
005220
005230
005240
005250
005260
005270
005280
005290
005300
005310
005320
005330
005340

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X	JCF3, JHCL, JH202, JH00L	005350
	COMMON /PHRATE/ J02(41), J03(41), JH20(41), JH22(41), JH20(41),	005360
X	JH205(41), JHNO3(41), JCH4(41), JCF2(41), JCF3(41), JHCL(41), JH202(41)	005370
Y	, JHJCL(41)	005380
	COMMON /PRORATE/ AA(10), BB(10), CC(10), DD(11), EE(10), GG(10), HH(10)	005390
	REAL JN03	005400
	COMMON /RATES/ RATE(65,81), RA(63), RB(65), JN03, PJ03	005410
	COMMON /SOLCON/ WL(100), FL(100), J02(100), Q03(100)	005420
	REAL NO, NO2, NOX, NO3, N205	005430
	COMMON /SPECIE/ H(41), OH(41), H02(41), H202(41), O3(41), O(41), NO(41),	005440
1	NO2(41), HNO3(41), NOX(41), CO(41), O2(41), CH4(41), H20(41), H2(41),	005450
2	CL(41), CL0(41), HCL(41), CLX(41), DCLX(41), NO3(41), N205(41),	005460
3	CLNO3(41)	005470
	COMMON /PRODS/ P0DDH(7,41), S0DDH(3,41), O3INT(41), CLCH4(41),	005480
1	YY(9), HHH(3,41)	005490
	DIMENSION O003(41)	005500
		005510
	COMMON /TECTR/ FT, FA, FB, FM	005520
S.S.	FT=0, FA=2, FB=0, FM=0; T.O. FT=1, FA=1, FB=1, FM=1	005530
		005540
	LOGICAL NEXT	005550
	DATA NEXT/.FALSE./	005560
	FT = 0.	005570
	FA = 2.	005580
	FB = 0.	005590
	FM = 0.	005600
	N1 = 31	005610
	LL = 1	005620
	LLJ = 41	005630
	N = 81	005640
	STEP = 1.	005650
	M = 1	005660
	HX = 6.0E+5	005670
	EPS = .001	005680
	EPS1 = .01	005690
	CALL SETUP2 (STEP, N)	005700
	QQJ = HX / (CEK(4) * CDM(N))	005710
	PPL = -CEK(1) * CDM(1)	005720
	PPJ = -CEK(4) * CDM(N)	005730
	CALL RJITER (ISWIT, ISCAT)	005740
		005750
	I = 0	005760
10	I = I + 1	005770
	IF (I.GT.50) GO TO 501	005780
	IF (I.EQ.1) GO TO 30	005790
	DO 12 J = LLL, LLU	005800
	OLD0H(J) = OH(J)	005810
	O03(J) = O3(J)	005820
12	CONTINUE	005830
30	DO 40 J = LLL, LLU	005840
	L = 2 * J - 1	005850
	J02(J) = CJ02(J)	005860
	J03(J) = CJ03(J)	005870
	JHNO3(J) = CJHNO3(J)	005880
	JH202(J) = CJH202(J)	005890
	JH205(J) = CJH205(J)	005900
	DIO(J) = CJ031(J) * O3(J) / (RATE(51, L) * DM(J))	005910
40	CONTINUE	005920
60	DO 100 K = LLL, LLU	005930
	L = 2 * K - 1	005940
	CALL INITAL(K, Y, I, NEXT)	005950
	CALL SOLVE (K, ALP, Y, N1)	005960
	DO 300 J = 1, 9	005970
300	HHH(J, K) = HH(J)	005980
	HHH(9, K) = PP(4)	005990
	P0DDH(1, K) = AA(1) * 2.	006000

POJDM(2,K) = CC(1)	006010
POJDM(3,K) = CC(2)	006020
POJDM(4,K) = CC(8)	006030
POJDM(5,K) = AA(3)	006040
POJDM(6,K) = CC(5)	006050
POJDM(7,K) = CC(6)	006060
CLDM4(K) = RATE(30,L) * CL(K) * CH4(K)	006070
SOJDM(1,K) = DD(2) * 2.	006080
SODDM(2,K) = DD(3)*2.	006090
DO 305 J = 3,7	006100
305 SOJDM(J,K) = DD(J+3)	006110
SODDM(8,K) = 2.0 * RATE(16,L) * H(K) * H02((006120
SOJDM(9,K) = GG(7)	006130
100 CONTINUE	006140
C	006150
DO 108 K = LLL,LLU	006160
108 ODJ3(K) = O3(K)	006170
CALL CFLOW (N1,I)	006180
DO 110 K = LLL,LLU	006190
110 O3(K) = (O3(K) + ODO3(K))/2.	006200
C	006210
DO 20 J = LLL,LLU	006220
OJ2(J) = CJ02(J)	006230
OJ3(J) = CJ03(J)	006240
OJCF2(J) = CJCF2(J)	006250
OJCF3(J) = CJCF3(J)	006260
OJGCL4(J) = CJGCL4(J)	006270
OJCH3C(J) = CJCH3C(J)	006280
OJGLO3(J) = CJGLO3(J)	006290
OJN20(J) = CJN20(J)	006300
OJHNO3(J) = CJHNO3(J)	006310
OJH202(J) = CJH202(J)	006320
OJ031(J) = CJ031(J)	006330
OJN205(J) = CJN205(J)	006340
OD3INT(J) = O03INT(J)	006350
20 CONTINUE	006360
CALL RJITER (ISWIT,ISCATT)	006370
IF (I.EQ.1) GO TO 10	006380
C	006390
DO 50 J = LLL,LLU	006400
E = ABS((CJ03(J) - OJ03(J))/CJ03(J))	006410
IF (E.GE.EPS) GO TO 10	006420
E1 = ABS((OH(J) - OLDON(J))/OH(J))	006430
IF (E1.GE.EPS1) GO TO 10	006440
50 CONTINUE	006450
502 CONTINUE	006460
CALL O3LINT (HHH,YY,9,36)	006470
O3INT(LLU) = O3(LLU)*5.0E5	006480
LLUML = LLJ - LLL	006490
DO 310 K = 1,LLUML	006500
J = LLU - K	006510
JP1 = J + 1	006520
310 O3INT(J) = O3INT(JP1) + (O3(JP1) + O3(J))*1.E5	006530
CALL PRINTX (I,LLL,LLU)	006540
NEXT=.TRUE.	006550
RETURN	006560
C	006570
501 I = I - 1	006580
WRITE (6,601) I	006590
601 FORMAT (1H0/10X,*DID NOT CONVERGE IN*,I4,* ITERATIONS*)	006600
GO TO 502	006610
C	006620
END	006630
SUBROUTINE RJITER (ISWIT,ISCATT)	006640
C.....	006650
C	006660


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C.....CMS03 - CHLORINE MODEL STUDY PROGRAM                                006670
C                                                                           006680
C.....VERSION 3.3          LEVEL 770201                                006690
C.....E.R.T.,INC.          N.D.SZ, N.TRIPP                             006700
C                                                                           006710
C.....006720
COMMON /RATES/RATE(65,81),RA(65),RB(65),JN03,PJ03                        006730
C                                                                           006740
NT = 41                                                                    006750
HAV = 5.0E05                                                                006760
IL = 1                                                                      006770
IU = 72                                                                    006780
IF (ISCATT.EQ.1) IU=99                                                       006790
IF (ISCATT.EQ.1) PJ03=0.0                                                    006800
RDF = 1.0                                                                    006810
IF (ISMIT.EQ.0) RDF = 0.5                                                    006820
GMJ = .707                                                                    006830
CALL GOLDEN (NT,HAV)                                                         006840
CALL COMPJ (IL,IU,GMU,RDF,NT,ISMIT,ISCATT)                                006850
RETURN                                                                        006860
END                                                                           006870
SUBROUTINE GOLDEN(NT,HAV)                                                    006880
C                                                                           006890
C THIS ROUTINE COMPUTES COLUMN DENSITIES OF OZONE                        006900
C                                                                           006910
NT IS THE INDEX NUMBER OF THE TOP LAYER                                     006920
HAV IS THE AVERAGE SCALE HEIGHT OF TOP LAYER                             006930
C                                                                           006940
REAL NO,NO2,NOX,NO3,N2O5                                                    006950
COMMON /SPECIE/ H(41),OH(41),HO2(41),H2O2(41),O3(41),O(41),NO(41),      006960
1 NO2(41),HNO3(41),NOX(41),CO(41),O2(41),CH4(41),H2O(41),H2(41),        006970
2 CL(41),CLO(41),HCL(41),CLX(41),DCLX(41),NO3(41),N2O5(41),            006980
3 CLNO3(41)                                                                  006990
COMMON /MODEL/ALT(41),TEMP(41),DM(41),DIO(41),DA23(41)                  007000
COMMON /INFOEN/DO3INT(41),DMINT(41),DAINT(41)                            007010
C                                                                           007020
NTM1 = NT - 1                                                                007030
DELZ = 2.0E05                                                                007040
DO3INT(NT) = O3(NT) * HAV                                                    007050
DO 10 J = 1,NTM1                                                            007060
I = NT - J                                                                    007070
IP1 = I + 1                                                                    007080
10 DO3INT(I) = DO3INT(IP1) + ( O3(IP1) + O3(I) ) * DELZ*.5              007090
RETURN                                                                        007100
END                                                                           007110
SUBROUTINE COMPJ (IL,IU,GMU,RDF,NT,ISMIT,ISCATT)                          007120
C.....007130
C.....CMS03 - CHLORINE MODEL STUDY PROGRAM                                007140
C                                                                           007150
C.....VERSION 3.3          LEVEL 770201                                007160
C.....E.R.T.,INC.          N.D.SZ, N.TRIPP                             007170
C                                                                           007180
C.....007190
C.....007200
C THIS ROUTINE COMPUTES J-VALUES, IL = LOWER LIMIT, IU = UPPER LIMIT    007210
C                                                                           007220
GMJ = SOLAR ZENITH ANGLE                                                    007230
RDF = FLUX REDUCTION FACTOR                                                 007240
NT = INDEX NUMBER OF TOP LAYER                                              007250
ISMIT = SWITCH USED IN COMPUTING TRAN FROM TAU                            007260
ISCATT = SWITCH FOR ABSORBING OR SCATTERING MODEL                         007270
COMMON /MODEL/ALT(41),TEMP(41),DM(41),DIO(41),DA23(41)                  007280
COMMON /INFOEN/ DO3INT(41),DMINT(41),DAINT(41)                            007290
COMMON /JVAL/ CJ02(50),CJ03(50),CJCF2(50),CJCF3(50),CJCCL4(50),        007300
1 CJCH3C(50),CJCLO3(50),CJN2O(50),CJHNO3(50)                            007310
2 CJH2O2(50),CJO3I(50),CJN2O5(50)                                         007320

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	COMMON /MSCAT/ SCN02,SCCL03,SCN202,SCN205	007330
	COMMON /PHIS/ PHI1(100)	007340
	REAL JO2,JO3,JH20,JN02,JN20,JN205,JHN03,JCH4,JCF2,	007350
	X JCF3,JHCL,JH202,JHCL	007360
	COMMON /PHRAT/ JO2(41),JO3(41),JH20(41),JN20(41),JN205(41),	007370
	X JN205(41),JHN03(41),JCH4(41),JCF2(41),JCF3(41),JHCL(41),	007380
	Y JH202(41),JHCL(41)	007390
	COMMON /SOLCON/ WL(100),FL(100),Q02(100),Q03(100)	007400
	COMMON /SOLCON1/ QCF2(100),QCF3(100),QCCL4(100),QCH3(100),	007410
	X QCLN03(100),QN20(100),QHNO3(100),QH202(100),QN205(100),	007420
	Y QHCL(100),JHCL(100),QNO2(100),QH20(100)	007430
	REAL LAT	007440
	COMMON /WT/ A(6),DL,LAT,DEL	007450
	COMMON/SCA/FAINT(100),F(41,100),FAV(41,100),FLUX(41)	007460
	DIMENSION PHI(100)	007470
C		007480
C	COMPUTE COLUMN DENSITIES, STORED IN DD3INT,DMINT,	007490
C	COMPUTED IN SUBROUTINE COLDEN	007500
C	IF ISWITCH THEN FIX GMU FOR INTEGRAL ELSE CALL COMPTAU	007510
C	IF ISCAT DO MULTIPLE SCATTERING CALCULATION AND	007520
C	WEIGHT FLUX FACTORS IF ISWIT	007530
	PO2 = 0.21	007540
	IF(ISCATT.EQ.0)GO TO 50	007550
	IF(ISWIT.EQ.0)GO TO 60	007560
	DO 65 I=1,NT	007570
	DO 66 J=IL,IU	007580
	FAV(I,J)=0.0	007590
	F(I,J)=0.0	007600
66	CONTINUE	007610
65	CONTINUE	007620
	DO 70 KK=1,5	007630
	GMU=1./A(KK)	007640
	CALL OMEGA(NT,IL,IU,GMU)	007650
	DO 80 I=1,NT	007660
	DO 90 J=IL,IU	007670
	FAV(I,J)=FAV(I,J)*F(I,J)	007680
90	CONTINUE	007690
80	CONTINUE	007700
70	CONTINUE	007710
	DO 75 I=1,NT	007720
	DO 76 J=IL,IU	007730
	F(I,J)=FAV(I,J)*DL*2./1036800.	007740
76	CONTINUE	007750
75	CONTINUE	007760
	GO TO 50	007770
60	CALL OMEGA(NT,IL,IU,GMU)	007780
50	CONTINUE	007790
	DO 10 I=1,NT	007800
	TEMP2 = 0.0	007810
	TEMP3 = 0.0	007820
	TEMP4 = 0.0	007830
	TEMP5 = 0.0	007840
	TEMP6 = 0.0	007850
	TEMP7 = 0.0	007860
	TEMP8 = 0.	007870
	TEMP9 = 0.	007880
	TEMP10 = 0.	007890
	TEMP11 = 0.	007900
	TEMP12 = 0.	007910
	TEMP13=0.	007920
	TEMP14=0.	007930
	TEMP15=0.	007940
	TEMP16=0.	007950
	DO 20 J = I.,IU	007960
	IF(ISCATT.EQ.1)GO TO 7	007970
	TAJ = Q03(J)*DD3INT(I) + Q02(J)*DMINT(I)*PO2	007980

IF (ISMIT.GT.0) GO TO 100	007390
TAU = -TAU/5MU	008800
IF (TAU.GE.-150.) GO TO 5	008010
TRAN = 0.	008020
GO TO 6	008030
5 TRAN = EXP(TAU)	008040
GO TO 6	008050
100 CALL COMTAU (TAU,TRAN)	008060
TRAN = TRAN*(DL/1036800.)	008070
GO TO 6	008080
7 TRAN=F(I,J)	008090
6 TEMP2 = TEMP2 + FL(J)*Q02(J)*TRAN	008100
TEMP3 = TEMP3 + FL(J)*Q03(J)*TRAN	008110
TEMP4 = TEMP4 + FL(J)*QCF2(J)*TRAN	008120
TEMP5 = TEMP5 + FL(J)*QCF3(J)*TRAN	008130
TEMP6 = TEMP6 + FL(J)*QCCL4(J)*TRAN	008140
TEMP7 = TEMP7 + FL(J)*QCH3C(J)*TRAN	008150
TEMP8 = TEMP8 + FL(J)*QCLN03(J)*TRAN*PHI1(J)	008160
TEMP9 = TEMP9 + FL(J)*QN20(J)*TRAN	008170
TEMP10 = TEMP10 + FL(J)*QHN03(J)*TRAN	008180
TEMP11 = TEMP11 + FL(J)*QH202(J)*TRAN	008190
TEMP12 = TEMP12 + FL(J)*QN205(J)*TRAN	008200
TEMP13 = TEMP13 + FL(J)*QHCL(J)*TRAN	008210
TEMP14 = TEMP14 + FL(J)*QHOC(L)*TRAN	008220
TEMP15 = TEMP15 + FL(J)*QN02(J)*TRAN	008230
TEMP16 = TEMP16 + FL(J)*QH20(J)*TRAN	008240
20 CONTINUE	008250
CJ02(I) = TEMP2*RDF	008260
CJ03(I) = TEMP3*RDF	008270
CJCF2(I) = TEMP4*RDF	008280
CJCF3(I) = TEMP5*RDF	008290
CJCCL4(I) = TEMP6*RDF	008300
CJCH3C(I) = TEMP7*RDF	008310
CJCLO3(I) = TEMP8*RDF*SCCLO3	008320
CJN20(I) = TEMP9*RDF	008330
CJHN03(I) = TEMP10*RDF	008340
CJH202(I) = TEMP11*RDF*SCH202	008350
CJN205(I) = TEMP12*RDF*SCN205	008360
JHCL(I) = TEMP13*RDF	008370
JHOC(L) = TEMP14*RDF	008380
JN02(I) = TEMP15*RDF	008390
JH20(I) = TEMP16*RDF	008400
10 CONTINUE	008410
PHI(53) = .7	008420
PHI(54) = .05	008430
DO 30 I = 1,NT	008440
TEMP31 = 0.	008450
DO 40 J = IL,54	008460
IF (ISCATT.EQ.1) GO TO 110	008470
TAJ = Q03(J)*DO3INT(I) + Q02(J)*DNINT(I)*P02	008480
IF (ISMIT.GT. 0) GO TO 25	008490
TAU=-TAU/GMJ	008500
IF (TAU.GE. -150.) GO TO 24	008510
TRAN=0.	008520
GO TO 27	008530
24 TRAN=EXP(TAU)	008540
GO TO 27	008550
25 CALL COMTAU (TAU,TRAN)	008560
TRAN = TRAN*(DL/1036800.)	008570
GO TO 27	008580
110 TRAN=F(I,J)	008590
27 IF (J.GT.52) GO TO 40	008600
PHI(J) = 1.0	008610
40 TEMP31 = TEMP31 + FL(J)*PHI(J)*Q03(J)*TRAN	008620
30 CJ031(I) = TEMP31*RDF	008630
LLL=1	008640

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LLJ=NT                                008650
WRITE (6,1601)                        008660
WRITE (6,602) (ALT(J),CJ02(J),CJ03(J),CJCF2(J),CJCF3(J),CJ031(J), 008670
1 JHCL(J), JH0CL(J),JN02(J),JH20(J), J=LLL,LLU) 008680
WRITE (6,1603)                        008690
WRITE (6,604) (ALT(J),CJCLO3(J),CJN20(J),CJHNO3(J),CJH207(J), 008700
1 CJN205(J),CJCCL4(J),CJCH3C(J),J=LLL,LLU) 008710
1601 FORMAT (1H0,5X,*LAST ITERATION + 1* // 5X,*ALT*,5X,*CJ02*, 7X, 008720
1 *CJ03*, 6X,*CJCF2*, 6X,*CJCF3*,6X,*CJ031*,5X,* JHCL*,5X, 008730
2 * JH0CL*,5X,* JN02*,6X,* JH20*//) 008740
602 FORMAT (1H ,0PF9.0, 1P09E11.3) 008750
1603 FORMAT (1H0,5X,*LAST ITERATION + 1*// 008760
A 6X,*ALT*,5X,*CJCLO3*,5X,*CJN20*, 008770
1 6X,*CJHNO3*,5X,*CJH207*,5X,*CJN205*,5X,*CJCCL4*,4X,*CJCH3CL*//) 008780
604 FORMAT (1H ,0PF9.0, 1P07E11.3) 008790
RETURN 008800
END 008810
SUBROUTINE CONTAU (TAU,TRAN) 008820
C ..... 008830
C ..... 008840
C.....CMS03 - CHLORINE MODEL STUDY PROGRAM 008850
C ..... 008860
C.....VERSION 3.3 LEVEL 770201 008870
C.....F.R.T.,INC. N.D.SZE, N.TRIPP 008880
C ..... 008890
C ..... 008900
C ..... 008910
REAL LAT 008920
COMMON /MT/ A(6),DL,LAT,DEL 008930
IF (TAU.GT.1.E-3) GO TO 10 008940
TRAN = DL/3600. 008950
RETURN 008960
C ..... 008970
10 TRAN = 0.0 008980
IF (TAU.GT.50.0) RETURN 008990
T = -TAU * A(1) 009000
C ..... 009010
TEST FOR UNDERFLOW 009010
IF (T.LT.-100.0) RETURN 009020
TRAN = EXP(T) * 2.0 009030
T = -TAU * A(2) 009040
IF (T.LT.-100.0) RETURN 009050
TRAN = TRAN + 2.0 * EXP(T) 009060
T = -TAU * A(3) 009070
IF (T.LT.-100.) RETURN 009080
TRAN = TRAN + 2.0 * EXP(T) 009090
T = -TAU * A(4) 009100
IF (T.LT.-100.) RETURN 009110
TRAN = TRAN + 2.0 * EXP(T) 009120
T = -TAU * A(5) 009130
IF (T.LT.-100.) RETURN 009140
TRAN = TRAN + 2.0 * EXP(T) 009150
T = -TAU * A(6) 009160
IF (T.LT.-100.) RETURN 009170
TRAN = TRAN + 2.0 * EXP(T) 009180
RETURN 009190
END 009200
SUBROUTINE INITAL (K,Y,II,NEXT) 009210
C ..... 009220
DIMENSION Y(10),RR(3) 009230
REAL NO,NO2,NOX,NO3,N2O5 009240
COMMON /SPECIE/ H(41),OH(41),HO2(41),H2O2(41),O3(41),O(41),NO(41), 009250
1 NO2(41),HNO3(41),NOX(41),CO(41),O2(41),CH4(41),H2O(41),H2(41), 009260
2 CL(41),CL3(41),HCL(41),CLX(41),OCLX(41),NO3(41),N2O5(41), 009270
3 C.NO3(41) 009280
COMMON /MODEL/ALT(41),TEMP(41),JH(41),DIO(41),DA23(41) 009290
COMMON /SFACT/ FCL.FH2O.FCLNO3.FNO 009300

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	LOGICAL NEXT	009310
		009320
	IF(NEXT) GO TO 10	009330
	IF (II.GT.1) GO TO 10	009340
	FCJ = 1.0	009350
	CO(K) = CO(K) * DM(K) * FCO	009360
	O2(K) = 0.2 * DM(K)	009370
	H2(K) = 0.5E-5 * DM(K)	009380
	CH4(K) = CH4(K) * DM(K)	009390
	DCLX(K) = CLX(K) * FCL	009400
	CLX(K) = CLX(K) * DM(K) * FCL	009410
	H2O(K) = H2O(K) * DM(K) * FH2O	009420
	NOX(K) = NOX(K) * DM(K)	009430
	OH(K) = OH(K) * 1.1	009440
	H2O2(K) = H2O2(K) * 1.1	009450
10	Y(1) = H(K)	009460
	Y(2) = OH(K)	009470
	Y(3) = H2O2(K)	009480
	Y(4) = O3(K)	009490
	J=0	009500
20	J=J+1	009510
	IF(J.GT.10) GO TO 50	009520
	TNO=NO(K)	009530
	TNO2=NO2(K)	009540
	THNO3=HNO3(K)	009550
	CALL PCLOX (K)	009560
	CALL PNOX(K)	009570
	RR(1)=TNO/NO(K)	009580
	RR(2)=TNO2/NO2(K)	009590
	RR(3)=THNO3/HNO3(K)	009600
	DO 25 M=1,3	009610
	IF(RR(M).GT.1.005.OR.RR(M).LT.0.995)GO TO 20	009620
25	CONTINUE	009630
	RETN	009640
50	J=J-1	009650
	WRITE(6,650)J	009660
650	FORMAT(1H0,5X,'DID NOT CONVERGE IN INITIAL IN ',I3,' TIMES')	009670
	STOP	009680
	END	009690
	SUBROUTINE PCLOX (K)	009700
		009710
	COMMON /JVA./ CJ02(50),CJ03(50),CJCF2(50),CJCF3(50),CJCCL4(50),	009720
1	CJCH3C(50),CJCLO3(50),CJN20(50),CJHNO3(50)	009730
2	, CJH202(50),CJ031(50),CJN205(50)	009740
	COMMON /MODFL/ALT(41),TEMP(41),DM(41),DID(41),DA23(41)	009750
	REAL J02, J03, JH20, JN02, JN20, JN205, JHNO3, JCH4, JCF2,	009760
X	JCF3, JHCL, JH2O2, JHOCL	009770
	COMMON /PHRATE/ J02(41),J03(41),JH20(41),JN22(41),JN20(41),	009780
X	JN205(41),JHNO3(41),JCH4(41),JCF2(41),JCF3(41),JHCL(41),JH2O2(41)	009790
Y	,JHOCL(41)	009800
	REAL JN03	009810
	COMMON /RATES/ RATE(65,81),RA(65),RB(65),JN03,PJ03	009820
	COMMON /SFACT/ FCL,FH2O,FCLNO3,FNO	009830
	REAL NO,NO2,NOX,NO3,N205	009840
	COMMON /SPECIE/ H(41),OH(41),H2O(41),H2O2(41),O3(41),O(41),NO(41),	009850
1	NO2(41),HNO3(41),NOX(41),CO(41),O2(41),CH4(41),H2O(41),H2(41),	009860
2	CL(41),CLO(41),HCL(41),CLX(41),DCLX(41),NO3(41),N2O5(41),	009870
3	CLNO3(41)	009880
		009890
	L = 2*K - 1	009900
	RRC1 = (CLO)/(CL)	009910
	RRC1 = RATE(23,L)*J3(K)/(RATE(31,L)*O(K) + RATE(32,L)*NO(K))	009920
	RRC2 = (HCL)/(CL)	009930
	RRC2 = (RATE(30,L)*CH4(K) + RATE(26,L)*H2(K) + RATE(15,L)*H2O2(K) +	009940
1	RATE(27,L)*H2O2(K))/(RATE(20,L)*OH(K) + RATE(33,L)*J(K) + JHCL(K))	009950
	RRC3A = (CLNO3)/(CLO)	009960


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C   RRC3B = (CLN03)/(CL)                                009370
RRC3A= RATE(25,L)*NO2(K)*FCLN03*DM(K)/CJCL03(K)         009380
RRC3B = RRC3A * RRC1                                     009390
C   CLX = CL + CLD + HCL                                  010000
CL(K) = CLX(K)/(1. + RRC1 + RRC2 + RRC3B)                010010
CLO(K) = RRC1*CL(K)                                       010020
HC(K) = RRC2*CL(K)                                       010030
RETURN                                                    010040
END                                                       010050
SUBROUTINE PNOX (K)                                       010060
C                                                       010070
COMMON /JVAL/ CJ02(50),CJ03(50),CJCF2(50),CJCF3(50),CJCCL4(50), 010080
1   CJCH3C(50),CJCL03(50),CJN20(50),CJHN03(50)          010090
2, CJH202(50),CJ031(50),CJN205(50)                     010100
COMMON /MODEL/ALT(41),TEMP(41),M(41),DID(41),DA23(41)    010110
COMMON /MSCAT/ SCN02,SCCL03,SCN202,SCN205               010120
REAL J02, J03, JH20, JN02, JN20, JN205, JHN03, JCH4, JCF2, 010130
X   JCF3, JHCL, JH202, JHCL                               010140
COMMON /PHRATE/ J02(41),J03(41),JH20(41),JN02(41),JN20(41), 010150
X   JN205(41),JHN03(41),JCH4(41),JCF2(41),JCF3(41),JHC(41),JH202(41) 010160
Y   ,JHCL(41)                                             010170
REAL JN03                                                 010180
COMMON /RATES/ RATE(65,81),RA(65),RB(65),JN03,PJ03     010190
COMMON /SFACT/ FCL,FH20,FCLN03,FNO                     010200
REAL NO,NO2,NOX,NO3,N205                                010210
COMMON /SPECIE/ M(41),OH(41),H02(41),H202(41),O3(41),O(41),NO(41), 010220
1   NO2(41),HNO3(41),NOX(41),CO(41),O2(41),CH4(41),H2O(41),H2(41), 010230
2   CL(41),CLO(41),HCL(41),CLX(41),DCLX(41),NO3(41),N205(41), 010240
3   C_N03(41)                                             010250
C                                                       010260
L = 2*K - 1                                              010270
C   RR1 = (NO)/(NO2)                                       010280
CJN02 = JN02(K) * SCN02                                  010290
RR1 = (CJN02+RATE(42,L)*O(K))/(RATE(32,L)*CLO(K)+RATE(40,L)*O3(K)) 010300
C   RR2 = (HNO3)/(NO2)                                     010310
RR2 = RATE(22,L)*OH(K)*DM(K)/(JHN03(K)+RATE(23,L)*OH(K)) 010320
C   RR3 = (NO3)/(NO2)                                      010330
RR3 = RATE(41,L)*O3(K)/JN03                              010340
C   RR4 = (N205)/(NO2)**2                                  010350
RR6 = RATE(38,L)*DM(K)/(RATE(37,L)+RATE(38,L)*DM(K))    010360
RR7 = RATE(37,L)/(RATE(37,L)+RATE(38,L)*DM(K))          010370
RR4 = RATE(36,L)*RR6/(RR7*RATE(39,L)+JN205(K))          010380
RR4 = RR3*RR4                                             010390
C   RR9 = (CLN03)/(NO2)                                    010400
RR9 = RATE(28,L)*CLO(K)*FCLN03*DM(K)/CJCL03(K)         010410
A = 2.0*RR4                                              010420
B = 1. + RR1 + RR2 + RR3 + RR9                          010430
C = NOX(K)                                                010440
CALL QUAD (A,B,C,X)                                       010450
NO2(K) = X                                                010460
NO(K) = X * RR1                                           010470
HNO3(K) = X * RR2                                          010480
NO3(K) = X * RR3                                           010490
N205(K) = X*X * RR4                                       010500
CLN03(K) = X * RR9                                        010510
10 RETURN                                                010520
END                                                       010530
SUBROUTINE QUAD(A,B,C,X)                                  010540
C   SOLVE EQ. A*X*X+B*X = C                               010550
DD=4.*A*C/(B*B)                                          010560
IF (DD .GT. .01) GO TO 10                               010570
X= B*(.5*DD-.125*DD*DD)                                  010580
X=X/(2.*A)                                                010590
RETURN                                                    010600
10 X= -B+SQRT(B*B+4.*A*C)                                  010610
X=X/(2.*A)                                                010620

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RETURN	010630
END	010640
SUBROUTINE SOLVE (K,ALP,Y,N1)	010650
C.....	010660
C.....	010670
C.....CMS 04 - CHLORINE MODEL STUDY PROGRAM	010680
C.....	010690
C.....SUBROUTINE SOLVE - ORGANIZES SOLUTION OF CHEMICAL SYSTEM	010700
C.....	010710
C.....VERSION 4.0 LEVEL 770214	010720
C.....E.R.T.,INC. N. D. SZE , N. TRIPP	010730
C.....	010740
C.....	010750
C.....	010760
REAL B	010770
COMMON /MATRIX/ B(20,21)	010780
COMMON /NETPRO/ PP(4),SS(4)	010790
REAL JO2, JO3, JH20, JNO2, JN20, JN205, JHN23, JCH4, JCF2,	010800
X JCF3, JHCL, JH22, JHCL	010810
COMMON /PHRATE/ JO2(41),JO3(41),JH20(41),JN20(41),JN205(41),	010820
X JN205(41),JHN23(41),JCH4(41),JCF2(41),JCF3(41),JHCL(41),JH22(41)	010830
Y , JHCL(41)	010840
REAL JNO3	010850
COMMON /RATES/ RATE(65,81),RA(65),RB(65),JNO3,PJO3	010860
REAL NO,NO2,NOX,NO3,N2O5	010870
COMMON /SPECIE/ H(41),OH(41),HO2(41),H2O2(41),O3(41),O(41),NO(41),	010880
1 NO2(41),HN23(41),NOX(41),CO(41),O2(41),CH4(41),H2O(41),H2(41),	010890
2 CL(41),CLO(41),HCL(41),CLX(41),DCLX(41),NO3(41),N2O5(41),	010900
3 CLNO3(41)	010910
DIMENSION Y(10), Y0(10)	010920
LOGICAL LINEQN	010930
C.....	010940
L = 2*K - 1	010950
WASH = 1.65E-6	010960
IF (K.GE.9) WASH = 0.0	010970
KKK = 0	010980
KK = 1	010990
N = 3	011000
NP1 = N + 1	011010
5 DO 10 J = 1, NP1	011020
10 Y0(J) = Y(J)	011030
I = 1	011040
C.....	011050
1 CALL JACOB (K,ALP,Y,N1)	011060
ERR = 0.	011070
DO 20 J = 1, N	011080
B(J, NP1) = PP(J) - SS(J)	011090
ERR = ERR + (B(J, NP1)/SS(J))**2	011100
20 CONTINUE	011110
C.....	011120
IF (LINEQN(N)) GO TO 50	011130
IF (ABS(ERR).LE.1.E-05) GO TO 100	011140
DO 55 J = 1, N	011150
55 Y(J) = Y(J) - B(J, NP1)	011160
I = I + 1	011170
IF (I.GT.20) GO TO 101	011180
GO TO 1	011190
C.....	011200
100 CONTINUE	011210
KK = KK + 1	011220
H(K) = Y(1)	011230
OH(K) = Y(2)	011240
HO2(K) = Y(3)	011250
O3(K) = Y(4)	011260
O(K) = ALP*Y(4)	011270
H2O2(K) = RATE(13,L)*Y(3)*Y(3)/(RATE(8,L)*Y(2)+JH2O2(K)+WASH)	011280

CALL PCLOX (K)	011290
CALL PNOX(K)	011300
IF (KK.GE.50) GO TO 145	011310
DO 75 II = 1,4	011320
IF ((YO(II)/Y(II)).LT.0.995) GO TO 5	011330
IF ((YO(II)/Y(II)).GT.1.005) GO TO 5	011340
75 CONTINUE	011350
CALL JACOB (K,ALP,Y,N1)	011360
RETURN	011370
145 WRITE (6,151)	011380
151 FORMAT (/," KK EQUAL TO 50 - SUBROUTINE SOLVE"/)	011390
RETURN	011400
50 WRITE (6,155) K	011410
155 FORMAT (/," MATRIX SINGULAR LEVEL = ",I3,")	011420
KKK = KKK + 1	011430
IF (KKK.GE.3) RETURN	011440
DO 501 J = 1,N	011450
501 Y(J) = 0.9*Y(J)	011460
GO TO 1	011470
101 WRITE (6,152)	011480
152 FORMAT (/," DOES NOT CONVERGE - SUBROUTINE SOLVE"/)	011490
RETURN	011500
END	011510
SUBROUTINE JACOB (K,ALP,Y,N1)	011520
.....	011530
.....CMS04 - CHLORINE MODEL STUDY PROGRAM	011540
.....SUBROUTINE JACOB - FORMS JACOBIAN OF CHEMICAL SYSTEM	011550
.....VERSION 4.0 LEVEL 770214	011560
.....E.R.T.,INC. N. D. SZE , N. TRIPP	011570
.....	011580
.....	011590
DIMENSION Y(10)	011600
REAL A	011610
COMMON /MATRIX/ A(20,21)	011620
COMMON /MODEL/ALT(41),TEMP(41),JM(41),DID(41),DA23(41)	011630
COMMON /NETPRD/ PP(4),SS(4)	011640
REAL JO2, J03, JH20, JN02, JN205, JHNO3, JCH4, JCF2,	011650
X JCF3, JHCL, JH202, JH0CL	011660
COMMON /PHRATE/ JO2(41),J03(41),JH20(41),JN02(41),JH205(41),	011670
X JHNO3(41),JCH4(41),JCF2(41),JCF3(41),JHCL(41),JH202(41)	011680
Y, JH0CL(41)	011690
COMMON /PRORATE/ AA(10),BB(10),CC(10),DD(11),EE(10),GG(10),HH(10)	011700
REAL JN03	011710
COMMON /RATES/ RATE(65,81),RA(65),RB(65),JN03,PJ03	011720
REAL NO,N02,NOX,N03,N205	011730
COMMON /SPECIE/ H(41),OH(41),H02(41),H202(41),O3(41),O(41),NO(41),	011740
1 N02(41),HNO3(41),NOX(41),CO(41),O2(41),CH4(41),H2O(41),H2(41),	011750
2 CL(41),CLO(41),HCL(41),CLX(41),DCLX(41),N03(41),N205(41),	011760
3 C,N03(41)	011770
L = 2*K - 1	011780
ALP = (J03(K) + PJ03)/(RATE(34,.) * O2(K) * OH(K))	011790
AA(1) = RATE(4,L) * DID(K) * H2(K) + JH20(K) * H2(K)	011800
AA(2) = RATE(19,L) * ALP * Y(4) * Y(2)	011810
AA(3) = RATE(18,L) * Y(2) * CO(K)	011820
AA(4) = RATE(21,L) * CH4(K) * Y(2)	011830
AA(5) = RATE(25,L) * Y(2) * H2(K)	011840
5 PP(1) = AA(1) + AA(2) + AA(3) + AA(4) + AA(5)	011850
BB(1) = RATE(5,L) * O2(K) * OH(K) * Y(1)	011860
BB(2) = RATE(6,L) * Y(4) * Y(1)	011870
BB(3) = (RATE(16,L) + RATE(17,L)) * Y(3) * Y(1)	011880

9	SS(1) = BB(1) + BB(2) + BB(3)	011350
10	A(1,1) = -SS(1)/Y(1)	011360
11	A(1,2) = (AA(2) + AA(3) + AA(4) + AA(5))/Y(2)	011370
12	A(1,3) = -BB(3)/Y(3)	011380
	CC(1) = 2.0*RATE(2,L)*DID(K)*H2O(K)	011390
	CC(2) = 2.0*RATE(3,L)*DID(K)*CH4(K)	012000
	CC(3) = RATE(10,L)*Y(4)*ALP*Y(3)	012010
	CC(4) = RATE(9,L)*Y(4)*Y(3)	012020
	CC(5) = RATE(11,L)*NO(K)*Y(3)	012030
19	CC(6) = 2.0*JH2O2(K)*H2O2(K)	012040
	CC(7) = RATE(5,L)*Y(1)*Y(4)	012050
21	CC(8) = JHNO3(K) * HNO3(K)	012060
	CC(9) = 2.0*RATE(17,L)*Y(1)*Y(3)	012070
	CC(10) = AA(1)	012080
23	PP(2) = CC(1)+CC(2)+CC(3)+CC(4)+CC(5)+CC(6)+CC(7)+CC(8)+CC(9)	012090
	1 + CC(10)	012100
	DD(1) = RATE(7,L)*Y(4)*Y(2)	012110
	DD(2) = RATE(8,L)*H2O2(K)*Y(2)	012120
	DD(3) = RATE(14,L)*Y(3)*Y(2)	012130
27	DD(4) = AA(3)	012140
28	DD(5) = AA(2)	012150
	DD(6) = RATE(20,L)*HCL(K)*Y(2)	012160
	DD(7) = RATE(21,L)*CH4(K)*Y(2)	012170
	DD(8) = RATE(22,L)*NO2(K)*DH(K)*Y(2)	012180
	DD(9) = RATE(23,L)*HNO3(K)*Y(2)	012190
	DD(10) = 2.0*RATE(24,L)*Y(2)*Y(2)	012200
	DD(11) = AA(5)	012210
34	SS(2) = DD(1)+DD(2)+DD(3)+DD(4)+DD(5)+DD(6)+DD(7)+DD(8)+DD(9)+DD(10)	012220
	1 + DD(11)	012230
35	A(2,1) = (CC(7) + CC(9))/Y(1)	012240
36	A(2,2) = -(SS(2) + DD(10))/Y(2)	012250
37	A(2,3) = (CC(3)+CC(4)+CC(5)+CC(6)-DD(3))/Y(3)	012260
39	EE(1) = BB(1)	012270
40	EE(2) = DD(1)	012280
	EE(3) = RATE(27,L)*CL(K)*H2O2(K)	012290
	EE(4) = DD(2)	012300
42	PP(3) = EE(1) + EE(2) + EE(3) + EE(4)	012310
43	GG(1) = CC(4)	012320
44	GG(2) = CC(3)	012330
45	GG(3) = CC(5)	012340
	GG(4) = RATE(12,L)*CLO(K)*Y(3)	012350
	GG(5) = 2.0*RATE(13,L)*Y(3)*Y(3)	012360
48	GG(6) = DD(3)	012370
	GG(7) = RATE(15,L)*CL(K)*Y(3)	012380
50	GG(8) = BB(3)	012390
51	SS(3) = GG(1)+GG(2)+GG(3)+GG(4)+GG(5)+GG(6)+GG(7)+GG(8)	012400
52	A(3,1) = (EE(1) - GG(8))/Y(1)	012410
53	A(3,2) = (EE(2) + EE(4) - GG(6))/Y(2)	012420
54	A(3,3) = -(SS(3) + GG(5))/Y(3)	012430
56	PP(4) = 2.0*JO2(K)*O2(K)	012440
57	HH(1) = BB(2)	012450
58	HH(2) = DD(1)	012460
59	HH(3) = CC(4)	012470
60	HH(4) = CC(3)	012480
61	HH(5) = AA(2)	012490
	HH(6) = 2.0*RATE(42,L)*NO2(K)*Y(4)*ALP	012500
	HH(7) = 2.0*RATE(31,L)*CLO(K)*ALP*Y(4)	012510
	HH(8) = 2.0*ALP*RATE(35,L)*Y(4)*Y(4)	012520
65	SS(4) = HH(1)+HH(2)+HH(3)+HH(4)+HH(5)+HH(6)+HH(7)+HH(8)	012530
	N11 = (N1-1)/2	012540
	IF (K.LE.N11) GO TO 80	012550
	T1 = 2.0*RATE(42,L)*NO2(K)	012560
	T2 = RATE(13,L)*Y(2)	012570
	T3 = RATE(10,L)*Y(3)	012580
	T4 = 2.0*RATE(31,L)*CLO(K)	012590
	TT1 = (T1+T2+T3+T4)*ALP	012600


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T5 = RATE(6,L)*Y(1)                                012610
T6 = RATE(7,L)*Y(2)                                012620
T7 = RATE(9,L)*Y(3)                                012630
T8 = 2.0*RATE(41,L)*NO2(K)                          012640
TT2=T5+T6+T7+T8                                    012650
B1=TT1+TT2                                           012660
A1 = 2.0*RATE(35,L)*ALP                             012670
C1=PP(4)                                             012680
CALL QUAD(A1,B1,C1,XX)                             012690
Y(4)=XX                                              012700
O(K) = ALP * XX                                     012710
70 RETURN                                           012720
80 Y(4) = O3(K)                                     012730
RETURN                                              012740
END                                                  012750
SUBROUTINE CFLOW(N1,NITER)                          012760
C                                                    012770
C FLOW PROGRAM FOR VARIOUS SPECIES:                 012780
C SP1 = N2O, SP2 = NOX, SP3 = CH4                  012790
C SP4 = FC11, SP5 = FC12                           012800
C SP6 = CH3CL, SP7 = CLX, SP8 = J3, SP9 = CCL4, SP10 = CO 012810
C TIME-DEPENDENT TERM FOR EACH SPECIES IS DFP      012820
C (SHOULD ALL BE SET = 0. FOR STEADY-STATE CASE)   012830
C                                                    012840
COMMON /CHLOR/ XCL(81)                             012850
COMMON /COE2/ A(81),B(81),C(81),F(81),X(81)        012860
COMMON /INT81/ XOH(81),XDIO(81),XJN20(81),XJCF3(81),XJCF2(81),
1 XJCH3C(81),XJO2(81),XJO3(81),XJO2(81),XNO2(81),XO3(81) 012870
2,XJCCL4(81),XCLO(81),XNO(81)                      012880
COMMON /ITER/ KKK                                   012890
COMMON /JVAL/ CJO2(50),CJO3(50),CJCF2(50),CJCF3(50),CJCCL4(50),
1 CJCH3C(50),CJCLO3(50),CJN20(50),CJHNO3(50)       012900
2, CJH2O2(50),CJO31(50),CJN2O5(50)                 012910
COMMON /MODEL/ALT(41),TEMP(41),JH(41),DIO(41),DA23(41) 012920
COMMON /MOL4Y3/ XH(81),XH2O(81),PH2O,RH2,X11(81)   012930
COMMON /NDATA/ CEK(81),CDM(81),CTEMP(81),CDA(81)   012940
COMMON /PARA1/ STEP,QQU,PPL,PPU,N,M                012950
COMMON /RLOW/ RN2O,RNOX,RCH4,RF11,RF12,RCH33,RCLX,RJCL4,R03 012960
REAL NO,NO2,NOX,NO3,N2O5                          012970
COMMON /SPECIE/ H(41),OH(41),HO2(41),H2O2(41),O3(41),O(41),NO(41),
1 NO2(41),HNO3(41),NOX(41),CO(41),O2(41),CH4(41),H2O(41),H2(41),
2 CL(41),CLO(41),HCL(41),CLX(41),OCLX(41),NO3(41),N2O5(41),
3 CLNO3(41)                                          013000
COMMON /SPECION/ FJ,FJFC,TL                        013010
COMMON /XLS/ XL1(81),XL2(81),XL3(81),XL4(81),XL5(81),XL6(81),
1 XL7(81),XL8(81),XL9(81),XL10(81)                 013020
COMMON /XXES/ X1(81),X2(81),X3(81),X4(81),X5(81),X6(81),X7(81),
1 X8(81),X9(81),X10(81)                           013030
DIMENSION PR1(81),PR2(81),PR3(81),PR4(81),PR5(81),PR6(81),PR7(81),
1 PR8(81),PR9(81),PR10(81)                         013040
DIMENSION DFP1(81),DFP2(81),DFP3(81),DFP4(81),DFP5(81),DFP6(81),
1 DFP7(81),DFP8(81),DFP9(81),DFP10(81)            013050
DIMENSION PR11(81),XL11(81),DFP11(81)              013060
COMMON /TRAPH2/ XL11                                013070
LOGICAL CONV,OKP03                                  013080
EXTERNAL CXL1,CXL2,CXL3,CXL4,CX.5,CXL6,CXL7,CXL8,CX.9,CXL10,CXL11 013090
CALL RINTER (DIO,XDIO)                             013100
CALL RINTER (OH,XOH)                               013110
CALL RINTER (CJN20,XJN20)                          013120
CALL RINTER (CJCF3,XJCF3)                          013130
CALL RINTER (CJCF2,XJCF2)                          013140
CALL RINTER (CJCH3C,XJCH3C)                        013150
CALL RINTER (CJO2,XJO2)                            013160
CALL RINTER (CJO3,XJO3)                            013170
CALL RINTER (HO2,XHO2)                              013180
CALL RINTER (NO2,XNO2)                              013190

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CALL RINTER (NO,XNO)	013270
CALL RINTER (O3,XO3)	013280
CALL RINTER (CJCCL4,XJCCL4)	013290
CALL RINTER (CLO,XCLO)	013300
CALL RINTER (CL,XCL)	013310
CALL RINTER (H,XH)	013320
CALL RINTER (H2O,XH2O)	013330
IF (RN2O.GT.1.0) QL1 = 0.	013340
IF (RN2O.LE.1.0) QL1 = 1.	013350
CALL CSPEC(1.,0.,PPL,QL1,RN2O,PR1,DFP1,XL1,CXL1)	013360
DO 1 I = 1,N	013370
1 X1(I) = X(I)	013380
CONV = .FALSE.	013390
IF (RNOX.GT.1.0) QL2 = 0.	013400
IF (RNOX.LE.1.0) QL2 = 1.	013410
K1 = 1	013420
IF (NITER.GT.1) K1 = 2	013430
DO 206 KKK = <1,25	013440
CALL CSPEC(1.,0.,PPL,QL2,RNOX,PR2,DFP2,XL2,CXL2)	013450
EMAX = 0.	013460
DO 202 I = 40,81	013470
EI = ABS((X2(I)-X(I))/X(I))	013480
IF (EI.GT.EMAX) EMAX = EI	013490
202 CONTINUE	013500
IF (EMAX.LT.0.05) CONV = .TRUE.	013510
IF (CONV) GO TO 204	013520
IF (KKK.EQ.1) GO TO 204	013530
DO 203 I = 1,N	013540
203 X2(I) = (X2(I) + X(I))/2.	013550
GO TO 206	013560
204 DO 205 I = 1,N	013570
205 X2(I) = X(I)	013580
IF (CONV) GO TO 2	013590
206 CONTINUE	013600
GO TO 500	013610
2 CONTINUE	013620
IF (RCH4.GT.1.0) QL3 = 0.	013630
IF (RCH4.LE.1.0) QL3 = 1.	013640
CALL CSPEC(1.,0.,PPL,QL3,RCH4,PR3,DFP3,XL3,CXL3)	013650
DO 3 I = 1,N	013660
3 X3(I) = X(I)	013670
IF (RF11.GT.1.0) QL4 = 0.	013680
IF (RF11.LE.1.0) QL4 = 1.	013690
CALL CSPEC(1.,0.,PPL,QL4,RF11,PR4,DFP4,XL4,CXL4)	013700
DO 4 I = 1,N	013710
4 X4(I) = X(I)	013720
IF (RF12.GT.1.0) QL5 = 0.	013730
IF (RF12.LE.1.0) QL5 = 1.	013740
CALL CSPEC(1.,0.,PPL,QL5,RF12,PR5,DFP5,XL5,CXL5)	013750
DO 5 I = 1,N	013760
5 X5(I) = X(I)	013770
IF (RCH3C.GT.1.) QL6 = 0.	013780
IF (RCH3C.LE.1.) QL6 = 1.0	013790
CALL CSPEC(1.,0.,PPL,QL6,RCH3C,PR6,DFP6,XL6,CXL6)	013800
DO 6 I = 1,N	013810
6 X6(I) = X(I)	013820
IF (RCCL4.GT.1.) QL9 = 0.	013830
IF (RCCL4.LE.1.) QL9 = 1.0	013840
CALL CSPEC(1.,0.,PPL,QL9,RCCL4,PR9,DFP9,XL9,CXL9)	013850
DO 9 I = 1,N	013860
9 X9(I) = X(I)	013870
IF (RCLX.GT.1.0) QL7 = 0.	013880
IF (RCLX.LE.1.0) QL7 = 1.0	013890
CALL CSPEC(1.,0.,PPL,QL7,RCLX,PR7,DFP7,XL7,CXL7)	013900
DO 7 I = 1,N	013910
7 X7(I) = X(I)	013920

IF (RM2.GT.1.0) QL11 = 0.	013930
IF (RM2.LE.1.0) QL11 = 1.	013940
CALL CSPEC(1.,0.,PPL,QL11,RM2,PR11,DFP11,XL11,CXL11)	013950
DO 11 I = 1,N	013960
11 X11(I) = X(I)	013970
800 N = N1	013980
DO 801 I = 1,N	013990
801 X8(I) = X03(I)/CDM(I)	014000
CONV = .FALSE.	014010
RU03 = X03(N1)/CDM(N1)	014020
IF (R03.GT.1.0) QL8 = 0.	014030
IF (R03.LE.1.0) QL8 = 1.	014040
DO 806 KK = 1,25	014050
CALL CSPEC (0.,RU03,PPL,QL8,R03, PR8,JFP8,XL8,CXL8)	014060
EMAX = 0.	014070
DO 802 I = 1,N	014080
EI =ABS((X8(I)-X(I))/X(I))	014090
IF (EI.GT.EMAX) EMAX = EI	014100
802 CONTINUE	014110
IF (EMAX.LT.0.01) CONV = .TRUE.	014120
804 DO 805 I = 1,N	014130
805 X8(I) = X(I)	014140
IF (CONV) GO TO 8	014150
806 CONTINUE	014160
GO TO 501	014170
8 CONTINUE	014180
OKP03 = .FALSE.	014190
CALL REPCM (N1,OKP03)	014200
IF (OKP03) GO TO 50	014210
CALL RINTER (CLO,XCLO)	014220
CALL RINTER (NO2,XNO2)	014230
GO TO 800	014240
50 N = 81	014250
CALL SETUP2(STEP,N)	014260
C	014270
N12 = (N1 + 1)/2	014280
DO 100 J = 1,41	014290
I = 2*J - 1	014300
NOX(J) = X2(I) * CDM(I)	014310
CH4(J) = X3(I) * CDM(I)	014320
CLX(J) = X7(I) * CDM(I)	014330
H2(J) = X11(I) * CDM(I)	014340
IF (J.GT.N12) GO TO 100	014350
O3(J) = X8(I) * CDM(I)	014360
100 CONTINUE	014370
RETURN	014380
C	014390
500 WRITE (6,600)	014400
600 FORMAT (1H0,* X2 DOES NOT CONVERGE IN 25 ITERATIONS - CFLJW*)	014410
STOP	014420
501 WRITE (6,601)	014430
601 FORMAT (1H0,* X8 DOES NOT CONVERGE IN 25 ITERATIONS - CFLJW*)	014440
STOP	014450
END	014460
SUBROUTINE RINTER (XX,XXX)	014470
DIMENSION XX(50),XXX(81)	014480
DO 10 I = 1,41	014490
J = 2*I - 1	014500
10 XXX(J) = XX(I)	014510
C	014520
DO 20 I = 1,40	014530
J = 2*I	014540
IP1 = I + 1	014550
20 XXX(J) = SQRT(XX(I) * XX(IP1))	014560
RETURN	014570
END	014580

SUBROUTINE CSPEC (UP,UR,P,Q,R,PR,DFP,XL,CXL)	014590
3 FOR FIXED MIXING RATIO AT TOP - PU = 0, QU = 1., RU MUST BE SPECIFIED	014600
COMMON /BC/ PJ,QU,RU,PL,QL,RL(1000)	014610
COMMON /COEF2/ A(81),B(81),C(81),F(81),X(81)	014620
COMMON /PARA1/ STEP,QQU,PPL,PPU,N,M	014630
DIMENSION PR(81),DFP(81),XL(81)	014640
PU = UP	014650
RU = UR	014660
PL = P	014670
QL = Q	014680
IF (Q.EQ.1.) PL = 0.	014690
RL(1) = R	014700
CALL CXL (PR,DFP,XL,N)	014710
QU = 1.0	014720
IF (PU.EQ.0.) GO TO 10	014730
QU = XL(N) * QQU	014740
10 CALL COEF (PR,XL,DFP)	014750
CALL TRIDIA (N)	014760
DO 20 I = 1,N	014770
20 XL(I) = PR(I) - XL(I)*X(I)	014780
RETURN	014790
END	014800
SUBROUTINE CXL1 (PR1,DFP1,XL1,N)	014810
COMMON /INT81/ XOH(81),XDID(81),XJN20(81),XJCF3(81),XJCF2(81),	014820
1 XJCH3C(81),XJQ2(81),XJQ3(81),X4Q2(81),XNO2(81),XQ3(81)	014830
2,XJGCL4(81),XCLO(81),XNO(81)	014840
COMMON /NDATA/ CEK(81),CDM(81),CTEMP(81),CDA(81)	014850
REAL JNO3	014860
COMMON /RATES/ RATE(65,81),RA(65),RB(65),JNO3,PJQ3	014870
COMMON /SPEC2ON/ FJ,FJFC,TL	014880
COMMON /SPLOSS/ SPL1(81),SPL4(81),SPL5(81),SPL6(81),SPL9(81)	014890
DIMENSION PR1(81),DFP1(81),XL1(81)	014900
DO 10 I = 1,N	014910
PR1(I) = 0.	014920
DFP1(I) = 0.	014930
XL1(I) = ((RATE(43,I) + RATE(44,I))*XDID(I) + XJN20(I)) * CDM(I)	014940
SP1(I) = RATE(44,I) * XDID(I) * CDM(I)	014950
10 CONTINUE	014960
RETURN	014970
END	014980
SUBROUTINE CXL2 (PR2,DFP2,XL2,N)	014990
COMMON /ITER/ KKK	015000
COMMON /INT81/ XOH(81),XDID(81),XJN20(81),XJCF3(81),XJCF2(81),	015010
1 XJCH3C(81),XJQ2(81),XJQ3(81),X4Q2(81),XNO2(81),XQ3(81)	015020
2,XJGCL4(81),XCLO(81),XNO(81)	015030
COMMON /NDATA/ CEK(81),CDM(81),CTEMP(81),CDA(81)	015040
REAL JNO3	015050
COMMON /RATES/ RATE(65,81),RA(65),RB(65),JNO3,PJQ3	015060
COMMON /SPEC2ON/ FJ,FJFC,TL	015070
COMMON /SPLOSS/ SPL1(81),SPL4(81),SPL5(81),SPL6(81),SPL9(81)	015080
COMMON /XXES/ X1(81),X2(81),X3(81),X4(81),X5(81),X6(81),X7(81),	015090
1 X8(81),X9(81),X10(81)	015100
DIMENSION PR2(81),DFP2(81),XL2(81),XL2T(81)	015110
IF (KKK.GT.1) GO TO 8	015120
DO 5 I = 1,7	015130
XL2T(I) = CDM(I)/(7.*8.64E4)	015140
5 XL2(I) = XL2T(I)	015150
DO 6 I = 8,11	015160
XL2T(I) = CDM(I)/(10.*8.64E4)	015170
6 XL2(I) = XL2T(I)	015180
DO 7 I = 12,81	015190
XL2T(I) = 0.0	015200
7 XL2(I) = XL2T(I)	015210
8 DO 10 I = 1,N	015220
DFP2(I) = 0.	015230
PR2(I) = 2.0*SPL1(I)*X1(I)	015240

IF (KKK.EQ.1) GO TO 10	015250
XJN0 = 4.0E-6*EXP((I-81)/7.0)	015260
XL2(I)=(2.0*RATE(45,I)*XJN0/(RATE(46,I)*.21))*CDM(I)*X2(I)+XL2T(I)	015270
10 CONTINUE	015280
RETURN	015290
END	015300
SUBROUTINE CXL3 (PR3,DFP3,XL3,N)	015310
COMMON /CHLOR/ XCL(81)	015320
COMMON /INT81/ XOH(81),XDID(81),XJN20(81),XJCF3(81),XJCF2(81),	015330
1 XJCH3C(81),XJ02(81),XJ03(81),XN02(81),XN02(81),X03(81)	015340
2,XJCCCL4(81),XCLO(81),XNO(81)	015350
COMMON /NDATA/ CEK(81),CDM(81),CTEMP(81),CDA(81)	015360
REAL JN03	015370
COMMON /RATES/ RATE(65,81),RA(65),RB(65),JN03,PJ03	015380
COMMON /SPEC0N/ FJ,FJFC,TL	015390
DIMENSION PR3(81),DFP3(81),XL3(81)	015400
DO 10 I = 1,N	015410
PR3(I) = 0.	015420
DFP3(I) = 0.	015430
XL3(I) = (RATE(3,I)*XDID(I) + RATE(21,I)*XOH(I)) * CDM(I)	015440
XL3(I) = XL3(I) + RATE(30,I)*XCL(I)*CDM(I)	015450
10 CONTINUE	015460
RETURN	015470
END	015480
SUBROUTINE CXL4 (PR4,DFP4,XL4,N)	015490
COMMON /INT81/ XOH(81),XDID(81),XJN20(81),XJCF3(81),XJCF2(81),	015500
1 XJCH3C(81),XJ02(81),XJ03(81),XN02(81),XN02(81),X03(81)	015510
2,XJCCCL4(81),XCLO(81),XNO(81)	015520
COMMON /NDATA/ CEK(81),CDM(81),CTEMP(81),CDA(81)	015530
REAL JN03	015540
COMMON /RATES/ RATE(65,81),RA(65),RB(65),JN03,PJ03	015550
COMMON /SPEC0N/ FJ,FJFC,TL	015560
COMMON /SPLOSS/ SPL1(81),SPL4(81),SPL5(81),SPL6(81),SPL9(81)	015570
DIMENSION PR4(81),DFP4(81),XL4(81)	015580
DO 10 I = 1,N	015590
PR4(I) = 0.	015600
DFP4(I) = 0.	015610
XL4(I) = (FJ*XJCF3(I) + 1./TL + RATE(47,I)*XDID(I)) * CDM(I)	015620
SPL4(I) = XL4(I)	015630
10 CONTINUE	015640
RETURN	015650
END	015660
SUBROUTINE CXL5 (PR5,DFP5,XL5,N)	015670
COMMON /INT81/ XOH(81),XDID(81),XJN20(81),XJCF3(81),XJCF2(81),	015680
1 XJCH3C(81),XJ02(81),XJ03(81),XN02(81),XN02(81),X03(81)	015690
2,XJCCCL4(81),XCLO(81),XNO(81)	015700
COMMON /NDATA/ CEK(81),CDM(81),CTEMP(81),CDA(81)	015710
REAL JN03	015720
COMMON /RATES/ RATE(65,81),RA(65),RB(65),JN03,PJ03	015730
COMMON /SPEC0N/ FJ,FJFC,TL	015740
COMMON /SPLOSS/ SPL1(81),SPL4(81),SPL5(81),SPL6(81),SPL9(81)	015750
DIMENSION PR5(81),DFP5(81),XL5(81)	015760
DO 10 I = 1,N	015770
PR5(I) = 0.	015780
DFP5(I) = 0.	015790
XL5(I) = (FJ*XJCF2(I) + 1./TL + RATE(48,I)*XDID(I)) * CDM(I)	015800
SPL5(I) = XL5(I)	015810
10 CONTINUE	015820
RETURN	015830
END	015840
SUBROUTINE CXL6 (PR6,DFP6,XL6,N)	015850
COMMON /INT81/ XOH(81),XDID(81),XJN20(81),XJCF3(81),XJCF2(81),	015860
1 XJCH3C(81),XJ02(81),XJ03(81),XN02(81),XN02(81),X03(81)	015870
2,XJCCCL4(81),XCLO(81),XNO(81)	015880
COMMON /NDATA/ CEK(81),CDM(81),CTEMP(81),CDA(81)	015890
REAL JN03	015900

COMMON /RATES/ RATE(65,81),RA(65),RB(65),JN03,PJ03	015310
COMMON /SPEC04/ FJ,FJFC,TL	015320
COMMON /SPLOSS/ SPL1(81),SPL4(81),SPL5(81),SPL6(81),SPL9(81)	015330
DIMENSION PR6(81),DFP6(81),XL6(81)	015340
DO 10 I = 1,N	015350
PR6(I) = 0.	015360
DFP6(I) = 0.	015370
XL6(I) = (FJ*XJCH3C(I) + RATE(1,I)*XOH(I)) * COM(I)	015380
SPL6(I) = XL6(I)	015390
10 CONTINUE	016000
RETURN	016010
END	016020
SUBROUTINE 3XL7 (PR7,DFP7,XL7,N)	016030
COMMON /INT91/ XOH(81),XDID(81),XJN20(81),XJCF3(81),XJCF2(81),	016040
1 XJCH3C(81),XJ02(81),XJ03(81),X102(81),XN02(81),X03(81)	016050
2,XJCC4(81),XCLO(81),XNO(81)	016060
COMMON /NDATA/ CEK(81),COM(81),CTEMP(81),CDA(81)	016070
COMMON /SPEC04/ FJ,FJFC,TL	016080
COMMON /SPLOSS/ SPL1(81),SPL4(81),SPL5(81),SPL6(81),SPL9(81)	016090
COMMON /XXES/ X1(81),X2(81),X3(81),X4(81),X5(81),X6(81),X7(81),	016100
1 X8(81),X9(81),X10(81)	016110
DIMENSION PR7(81),DFP7(81),XL7(81)	016120
DO 10 I = 1,7	016130
10 XL7(I) = COM(I)/(7.*8.64E4)	016140
DO 20 I = 8,11	016150
20 XL7(I) = COM(I)/(10.*8.64E4)	016160
DO 30 I = 12,81	016170
30 XL7(I) = 0.0	016180
DO 40 I = 1,N	016190
DFP7(I) = 0.0	016200
PR7(I) = 3.0*SPL4(I)*X4(I) + 2.0*SPL5(I)*X5(I) + SPL6(I)*X6(I)	016210
1 + 2.0*SPL9(I)*X9(I)	016220
40 CONTINUE	016230
RETURN	016240
END	016250
SUBROUTINE 2XL8 (PR8,DFP8,XL8,N)	016260
COMMON /INT91/ XOH(81),XDID(81),XJN20(81),XJCF3(81),XJCF2(81),	016270
1 XJCH3C(81),XJ02(81),XJ03(81),X102(81),XN02(81),X03(81)	016280
2,XJCC4(81),XCLO(81),XNO(81)	016290
COMMON /NDATA/ CEK(81),COM(81),CTEMP(81),CDA(81)	016300
REAL JN03	016310
COMMON /RATES/ RATE(65,81),RA(65),RB(65),JN03,PJ03	016320
COMMON /SFACT/ FCL,FH20,FCLN03,FNO	016330
COMMON /XXES/ X1(81),X2(81),X3(81),X4(81),X5(81),X6(81),X7(81),	016340
1 X8(81),X9(81),X10(81)	016350
DIMENSION PR8(81),DFP8(81),XL8(81),XX(81)	016360
DO 10 I = 1,N	016370
ALP = (XJ03(I) + PJ03)/(RATE(34,I)*.21*COM(I)**2)	016380
XX(I) = XCLO(I)*ALP	016390
XLA = RATE(3,I)*XN02(I)	016400
XL3 = RATE(7,I)*XOH(I)	016410
XLC = 2.0*RATE(42,I)*XN02(I)*ALP	016420
XLD = RATE(10,I)*XN02(I)*ALP	016430
XLE = RATE(19,I)*XOH(I)*ALP	016440
XLF = 2.0*RATE(31,I)*XX(I)	016450
XLS = 2.0*RATE(35,I)*ALP*COM(I)*X8(I)	016460
XLT = 2.0*RATE(41,I)*XN02(I)	016470
XLN12 = (XLA+XLB+XLC+XLD+XLE+XLF+XLS)*COM(I)	016480
XLN11 = XLN12+XLT+XLN12*COM(I)	016490
DFP8(I) = XLN11 + XLN12 + XLN12*COM(I) * .21	016500
PR8(I) = PR8(I) + RATE(11,I)*XN02(I)*FNO	016510
DFP8(I) = 0.	016520
10 CONTINUE	016530
RETURN	016540
END	016550
	016560

COMMON /INT31/ XOH(81),XOID(81),XJN20(81),XJCF3(81),XJCF2(81),	016570
1 XJCH3C(81),XJO2(81),XJO3(81),X402(81),XNO2(81),XO3(81)	016580
2,XJCCL4(81),XCLO(81),XNO(81)	016590
COMMON /NDATA/ CEK(81),CDM(81),CTEMP(81),CDA(81)	016600
COMMON /SPEC04/ FJ,FJFC,TL	016610
COMMON /SPL05/ SPL1(81),SPL4(81),SPL5(81),SPL6(81),SPL9(81)	016620
DIMENSION PR9(81),DFP9(81),XL9(81)	016630
DO 10 I = 1,N	016640
PR9(I) = 0.	016650
DFP9(I) = 0.	016660
XL9(I) = FJ*XJCCL4(I)*CDM(I)	016670
SPL9(I) = XL9(I)	016680
10 CONTINUE	016690
RETURN	016700
END	016710
SUBROUTINE JXL11 (PR11,DFP11,XL11,N)	016720
COMMON /CHLOR/ XCL(81)	016730
COMMON /INT31/ XOH(81),XOID(81),XJN20(81),XJCF3(81),XJCF2(81),	016740
1 XJCH3C(81),XJO2(81),XJO3(81),X402(81),XNO2(81),XO3(81)	016750
2,XJCCL4(81),XCLO(81),XNO(81)	016760
COMMON /MOL4YD/ XH(81),XH20(81),PH20,RH2,X11(81)	016770
COMMON /NDATA/ CEK(81),CDM(81),CTEMP(81),CDA(81)	016780
REAL JN03	016790
COMMON /RATES/ RATE(65,81),RA(65),RB(65),JN03,PJ03	016800
COMMON /SPEC04/ FJ,FJFC,TL	016810
DIMENSION PR11(81),DFP11(81),XL11(81)	016820
DO 10 I = 1,N	016830
PR11(I) = RATE(16,I)*XH(I)*XNO2(I)+RATE(2,I)*XOID(I)*XH20(I)*PH20	016840
XL11(I) = (RATE(26,I)*XCL(I) + RATE(25,I)*XOH(I)	016850
1 + RATE(4,I)*XOID(I)) * CDM(I)	016860
10 CONTINUE	016870
RETURN	016880
END	016890
SUBROUTINE JOEF (PR,XL,DFP)	016900
3	016910
3 SUBROUTINE COEF TO COMPUTE ALL NEEDED VALUES FOR TRIDIA	016920
3 S.S. FT=0,FA=2,FB=0,FM=0; T.D. FT=1,FA=1,FB=1,FM=1	016930
3 EK=EDDY COEF,DM=AIR DENSITY,DF=INITIAL MIXING RATIO,N=NO.OF LAYERS	016940
3 THE VA.LUES OF B(1) AND C(N) ARE SPECIFIED BUT NOT USED	016950
C	016960
COMMON /BC/ PJ,QU,RU,PL,QL,RL(1000)	016970
COMMON /COE=1/AA(81),BB(81),CC(81),DL(81),DJ(81),U(81)	016980
COMMON /COE=2/ A(81),B(81),C(81),F(81),X(81)	016990
COMMON /NDATA/ CEK(81),CDM(81),CTEMP(81),CDA(81)	017000
COMMON /PARA1/ STEP,QUU,PPL,PPU,N,M	017010
COMMON /TFCTR/ FT,FA,FB,FM	017020
REAL PR(81),XL(81),DFP(81),T(81),DD(81),DDR(81),S(81)	017030
IF (FT.EQ.1.)GO TO 5	017040
DO 2 I = 1,N	017050
2 DFP(I) = 0.	017060
5 DZ=1.0E+05	017070
DT=3.15576E7*STEP	017080
AA(1) = 2.0*CEK(1)*CDM(1)	017090
TT = AA(1)*J(1)	017100
NM1=N-1	017110
DO 10 I=1,N	017120
10 T(I)=0.5*XL(I)*DT/CDM(I)	017130
DO 50 I=2,NM1	017140
S(I)=PR(I)*DT/CDM(I)	017150
DD(I)=(-FT+T(I)+U(I)*AA(I))*FA	017160
50 DDR(I)=(-FT+T(I)+U(I)*AA(I))*FB	017170
IF (ABS(PL).LE.1.E-60)GO TO 60	017180
3 FLUXES ARE SPECIFIED BOTH AT TOP AND BOTTOM	017190
S(1)=2.0*RL(N)*DZ/PL	017200
DD(1) =-(FT/TT + T(1)/TT + 1.0)*FA	017210
DU(1)=1.0*FA	017220

DDR(1) = (-FT/TT + T(1)/TT + 1.0)*FB	017230
F(1)=DDR(1)*DFP(1)-DU(1)*DFP(2)+S(1)	017240
GO TO 70	017250
C FLUX AT TOP, SPECIFIED MIXING RATIO AT BOTTOM	017260
60 S(1)=RL(1)	017270
DD(1)=.5*FA	017280
DU(1)=0.*FA	017290
DDR(1)=-.5*FB	017300
F(1)=DDR(1)*DFP(1)+S(1)	017310
70 IF (ABS(QU).LE.1.E-60)GO TO 71	017320
IF (ABS(PU).LE.1.E-60)GO TO 72	017330
S(1)=0.	017340
DD(N)=(1.+QU*DZ)*FA	017350
DL(N)=-1.*FA	017360
DDR(N)=-DD(N)*FB	017370
GO TO 73	017380
C FLUX SPECIFIED AT TOP	017390
71 S(N) = 2.0*QU*DZ/PU	017400
DD(N) = 1.0*FA	017410
DL(N) = -1.0*FA	017420
DDR(N) = -1.0*FB	017430
GO TO 73	017440
C MIXING RATIO SPECIFIED AT TOP	017450
72 S(1) = RU	017460
DD(N) = 0.5*FA	017470
DL(N) = 0.	017480
DDR(N) = -.5*FB	017490
73 DO 80 I=2,NM1	017500
IM1=I-1	017510
IP1=I+1	017520
80 F(I)=-DL(I)*DFP(IM1)+DDR(I)*DFP(I)-DU(I)*DFP(IP1)-S(I)	017530
F(N)=-DL(N)*DFP(N-1)+DDR(N)*DFP(N)+S(N)	017540
DO 90 I=1,N	017550
90 A(I)=DD(I)	017560
DO 91 I=2,N	017570
91 B(I)=DL(I)	017580
DO 92 I=1,NM1	017590
92 C(I)=DU(I)	017600
B(1)=1.0	017610
C(1)=1.0	017620
DL(1)=1.	017630
DU(N)=1.	017640
RETURN	017650
END	017660
SUBROUTINE TRIDIA (N)	017670
C SUBROUTINE TRIDIA TO COMPUTE MIXING RATIO	017680
COMMON /COEF2/ A(81),B(81),C(81),F(81),X(81)	017690
REAL ALPHA(81),GAMMA(81),G(81)	017700
IF (A(1).EQ.0.0) GO TO 100	017710
ALPHA(1)=A(1)	017720
GAMMA(1)=C(1)/ALPHA(1)	017730
NM1=N-1	017740
DO 10 I=1,NM1	017750
IF (ALPHA(I).EQ.0.0) GO TO 100	017760
GAMMA(I)=C(I)/ALPHA(I)	017770
IP1=I+1	017780
10 ALPHA(IP1)=A(IP1)-B(IP1)*GAMMA(I)	017790
G(1)=F(1)/ALPHA(1)	017800
DO 30 I=2,N	017810
30 G(I)=(F(I)-B(I)*G(I-1))/ALPHA(I)	017820
X(N)=G(N)	017830
DO 40 I=1,NM1	017840
J=I+1	017850
40 X(J)=G(J)-GAMMA(J)*X(J+1)	017860
GO TO 101	017870
100 WRITE (6,105) I	017880

105	FORMAT (/ ,2X,*SINGULAR MATRIX - I =*,I3/)	017890
101	RETURN	017900
	END	017910
	SUBROUTINE REPCN (N1,OKP03)	017920
	LOGICAL OKP03	017930
	COMMON /JVAL/ CJ02(50),CJ03(50),CJCF2(50),CJCF3(50),CJCCL4(50),	017940
1	CJCH3C(50),CJCLO3(50),CJN20(50),CJHNO3(50)	017950
2,	CJH202(50),CJ031(50),CJN205(50)	017960
	COMMON /MODEL/ALT(41),TEMP(41),DM(41),DID(41),DA23(41)	017970
	REAL JNO3	017980
	COMMON /RATES/ RATE(65,81),RA(65),RB(65),JN03,PJ03	017990
	REAL NO,N02,NOX,N03,N205	018000
	COMMON /SPECIE/ H(41),OH(41),H02(41),H202(41),O3(41),O(41),NO(41),	018010
1	N02(41),HNO3(41),NOX(41),CO(41),O2(41),CH4(41),H2O(41),H2(41),	018020
2	CL(41),CLO(41),HCL(41),CLX(41),DCLX(41),N03(41),N2O5(41),	018030
3	CLNO3(41)	018040
	COMMON /XXES/ X1(81),X2(81),X3(81),X4(81),X5(81),X6(81),X7(81),	018050
1	X8(81),X9(81),X10(81)	018060
	REAL CLO1(41),NO21(41)	018070
C		018080
	N11 = (N1 - 1)/2	018090
	E1MAX = 0.	018100
	E2MAX = 0.	018110
	DO 10 I = 1,N11	018120
	L = 2*I - 1	018130
	CLO1(I) = CLO(I)	018140
	NO21(I) = NO2(I)	018150
	ALP = (CJ03(I) + PJ03)/(RATE(34,L)*.21*DM(I)**2)	018160
	O3(I) = X8(2*I - 1) * DM(I)	018170
	O(I) = ALP * O3(I)	018180
	CLX(I) = X7(L)*DM(I)	018190
	NOX(I) = X2(L)*DM(I)	018200
	CALL PNOX (I)	018210
	CALL PCLOX(I)	018220
	E1 = ABS((CLO(I) - CLO1(I))/CLO1(I))	018230
	IF (E1.GT.E1MAX) E1MAX = E1	018240
	E2 = ABS((NO2(I) - NO21(I))/NO21(I))	018250
	IF (E2.GT.E2MAX) E2MAX = E2	018260
	CLO(I) = (CLO(I) + CLO1(I))/2.	018270
	NO2(I) = (NO2(I) + NO21(I))/2.	018280
10	CONTINUE	018290
	IF (E1MAX.LT..010.AND.E2MAX.LT..010) OKP03 = .TRUE.	018300
	RETURN	018310
	END	018320
	SUBROUTINE O3LINT (X,Y,IL,IU)	018330
	DIMENSION X(9,41),Y(9)	018340
C		018350
	IF (IU.LE.40) GO TO 5	018360
	WRITE (6,600) IU	018370
600	FORMAT (1H0,* IN SUBROUTINE O3LINT, IU =*,I3,* - TOO HIGH FOR INTE	018380
	1GRAND ARRAY*)	018390
	STOP	018400
C		018410
5	DO 10 I = 1,9	018420
	Y(I) = 0.	018430
	DO 10 J = IL,IU	018440
10	Y(I) = Y(I) + (X(I,J) + X(I,J+1))*1.E5	018450
C		018460
	RETURN	018470
	END	018480
	SUBROUTINE PRINTX (I,LLL,LLU)	018490
	COMMON /INTDEN/DO3INT(41),DMINT(41),DAINT(41)	018500
	COMMON /JVAL/ CJ02(50),CJ03(50),CJCF2(50),CJCF3(50),CJCCL4(50),	018510
1	CJCH3C(50),CJCLO3(50),CJN20(50),CJHNO3(50)	018520
2,	CJH202(50),CJ031(50),CJN205(50)	018530
	COMMON /MODEL/ALT(41),TEMP(41),DM(41),DID(41),DA23(41)	018540

COMMON /MOL4YD/ XH(81),XH20(81),PH20,RH2,X11(81)	018550
COMMON /MDATA/ CEK(81),CDM(81),CTEMP(81),CDA(81)	018560
COMMON /OLD/ OJ02(41),OJ03(41),OJCF2(41),OJCF3(41),OJCCL4(41),	018570
1 OJCH3C(41),OJCLO3(41),OJN20(41),OJHNO3(41),OJH202(41),OJ031(41),	018580
2 OJN205(41),OLD0H(41),O03INT(41),O03(41)	018590
COMMON /PRODS/ P0DDH(7,41),S0DDH(9,41),O3INT(41),CLCH4(41),	018600
1 YY(9),HHH(9,41)	018610
REAL NO,N02,NOX,N03,N205	018620
COMMON /SPECIE/ H(41),OH(41),MO2(41),H2O2(41),O3(41),O(41),NO(41),	018630
1 NO2(41),H4J3(41),NOX(41),CO(41),O2(41),CH4(41),H2O(41),H2(41),	018640
2 CL(41),CLO(41),HCL(41),CLX(41),DCLX(41),N03(41),N2J5(41),	018650
3 CLN03(41)	018660
DIMENSION XL11(81)	018670
COMMON /TRAPH2/ XL11	018680
COMMON /XLS/ XL1(81),XL2(81),XL3(81),XL4(81),XL5(81),XL6(81),	018690
1 XL7(81),XL8(81),XL9(81),XL10(81)	018700
COMMON /XXES/ X1(81),X2(81),X3(81),X4(81),X5(81),X6(81),X7(81),	018710
1 X8(81),X9(81),X10(81)	018720
DIMENSION C1(41),C4(41),C5(41),C6(41),C9(41)	018730
REAL MCL(41),MCLO(41),MHCL(41),MCLN03(41),M5(41)	018740
	018750
CALL PAGE	018760
WRITE (6,601) I	018770
WRITE (6,602) (ALT(J),OJ02(J),OJ03(J),OJCF2(J),OJCF3(J),OJ031(J),	018780
1 O03(J),O03INT(J),DMINT(J),OLD0H(J),J=LLL,LLU)	018790
CALL PAGE	018800
WRITE (6,603) I	018810
WRITE (6,604) (ALT(J),OJCLO3(J),OJN20(J),OJHNO3(J),OJH202(J),	018820
1 OJN205(J),OJCCL4(J),OJCH3C(J),J=LLL,LLU)	018830
	018840
CALL PAGE	018850
WRITE (6,1601)	018860
WRITE (6,602) (ALT(J),CJ02(J),CJ03(J),CJCF2(J),CJCF3(J),CJ031(J),	018870
1 O3(J),O03INT(J),DMINT(J), OH(J),J=LLL,LLU)	018880
CALL PAGE	018890
WRITE (6,1603)	018900
WRITE (6,604) (ALT(J),CJCLO3(J),CJN20(J),CJHNO3(J),CJH202(J),	018910
1 CJN205(J),CJCCL4(J),CJCH3C(J),J=LLL,LLU)	018920
	018930
DO 10 J = LLL,LLU	018940
MCL(J) = CL(J)/OH(J)	018950
MCLO(J) = CLO(J)/OH(J)	018960
MHCL(J) = HCL(J)/OH(J)	018970
MCLN03(J) = CLN03(J)/OH(J)	018980
10 CONTINUE	018990
NLINE = LLU - LLL + 1	019000
CALL PAGE	019010
CALL LINES (3+NLINE),RETURNS(315)	019020
315 WRITE (6,605)	019030
WRITE (6,606) (K,ALT(K),H(K),OH(K),MO2(K),H2O2(K),O(K),O3(K),	019040
1 O3INT(K),DID(K),K=LLL,LLU)	019050
CALL LINES (3+NLINE),RETURNS(320)	019060
320 WRITE (6,607)	019070
WRITE (6,608) (K,ALT(K),NO(K),MO2(K),HNO3(K),NO3(K),N205(K),NOX(K),	019080
1 K=LLL,LLU)	019090
CALL LINES (3+NLINE),RETURNS(325)	019100
325 WRITE (6,609)	019110
WRITE (6,615) (K,ALT(K),CL(K),HCL(K),CLO(K),MCLO(K),MCL(K),	019120
1 MHCL(K),CLN03(K),MCLN03(K),DCLX(K),K=LLL,LLU)	019130
	019140
CALL LINES (7+NLINE),RETURNS(330)	019150
330 WRITE (6,614)	019160
WRITE (6,615) (K,ALT(K), (HHH(J,C), J=1,9), K=LLL,LLU)	019170
WRITE (6,714)	019180
WRITE (6,715) (YY(J), J=1,9)	019190
CALL LINES (3+NLINE),RETURNS(335)	019200

335	WRITE (6,615)	019210
	WRITE (6,605) (K,ALT(K), (PODDH(J,K),J=1,7),CLCH4(K),K=LLL,LLU)	019220
	CALL LINES (3+NLIN),RETURNS(340)	019230
340	WRITE (6,618)	019240
	WRITE (6,615) (K,ALT(K), (SOODH(J,K),J=1,9),K=LLL,LLJ)	019250
C		019260
	CALL PRINT9 (X1,X2,X3,X4,X5,X6,X7,X9,X11,4HN20,4HN2X,4HC44,14HFC11,4HFC12,4HCH3C,4HCLX,4HCCL4,4H H2)	019270
		019280
C	COMPUTE FLUX AT BOTTOM	019290
	CALL TRAP (XL1,FN20,1,81)	019300
	CALL TRAP (XL2,FNOX,1,81)	019310
	CALL TRAP (XL3,FCH4,1,81)	019320
	CALL TRAP (XL4,FF11,1,81)	019330
	CALL TRAP (XL5,FF12,1,81)	019340
	CALL TRAP (XL6,FCH3C,1,81)	019350
	CALL TRAP (XL7,FCLX,1,81)	019360
	CALL TRAP (XL9,FCCL4,1,81)	019370
	CALL TRAP (XL11,FH2,1,81)	019380
	WRITE (6,70) FN20,FNOX,FCH4,FF11,FF12,FCH3C,FCLX,FCCL4,FH2	019390
C		019400
	DO 100 J = LLL,LLU	019410
	K = 2*J - 1	019420
	C4(J) = X4(K) * CDM(K)	019430
	C5(J) = X5(K) * CDM(K)	019440
	C6(J) = X6(K) * CDM(K)	019450
	C9(J) = X9(K) * CDM(K)	019460
	C1(J) = X1(K) * CDM(K)	019470
	M8(J) = O3(J)/DM(J)	019480
100	CONTINUE	019490
	CALL PAGE	019500
	WRITE (6,611)	019510
	WRITE (6,609) (K,ALT(K),M8(K),C4(K),C5(K),C5(K),C9(K),	019520
	1 CLX(K),K=LLL,LLU)	019530
	CALL PAGE	019540
	WRITE (6,612)	019550
	WRITE (6,613) (K,ALT(K), C1(K),NOX(K),CH4(K),K=LLL,...U)	019560
	RETURN	019570
C		019580
	70 FORMAT (1H0,3X,*FN20 =*,1PE13.5,4X,*FNOX =*,E13.5,4X,	019590
	1 *FCH4 =*,E13.5,4X,*FF11 =*,E13.5,4X,*FF12 =*,E13.5//	019600
	2 4X,*FCH3C =*,E13.5,4X,*FCLX =*,E13.5,4X,*FCCL4 =*,E13.5,	019610
	3 4X,*FH2 =*,E13.5)	019620
	601 FORMAT (1H0,5X,*LAST ITERATION =*,I3 // 5X,*ALT*,6X,*CJ02*, 7X,*	019630
	1 *CJ03*, 6X,*CJCF2*, 6X,*CJCF3*, 6X,*CJ031*,5X,*PREVJ3*,5X,	019640
	2 *DOJINT*,5X,*DMINT*,6X,*PREVOH*//)	019650
	602 FORMAT (1H , 0PF9.0, 1P09E11.3)	019660
	603 FORMAT (1H0,5X,*LAST ITERATION =*,I3 //	019670
	A 6X,*ALT*,5X,*CJCLO3*,5X,*CJN20*,	019680
	1 6X,*CJHNO3*,5X,*CJH202*,5X,*CJN205*,5X,*CJCCL4*,4X,*CJCH3CL*//)	019690
	604 FORMAT (1H , 0PF9.0, 1P07E11.3)	019700
	605 FORMAT (1H0,2X,*K*,7X,*ALT*, 9X,*H*,12X,*OH*,12X,*HJ2*,11X,*H202*,	019710
	1 11X,*O*,13X,*O3*,10X,*O3INT*,9X,*O(*O*)//)	019720
	606 FORMAT (1H , I3,0PF11.0,1P0E14.4)	019730
	607 FORMAT (1H0,2X,*K*,7X,*ALT*, 9X,*NO*,13X,*NO2*,12X,*HNO3*,11X,	019740
	1 *H03*,12X,*H205*,10X,* NOX*//)	019750
	608 FORMAT (1H , I3,0PF11.0,1P6E15.4)	019760
	609 FORMAT (1H0,1X,*K*,7X,*ALT*,15X,*CL*,23X,*CLO*,23X,*HCL*,22X,	019770
	1 *CLNO3*,15X,*OCLX*//)	019780
	610 FORMAT (1H , I3,0PF11.0,1P5E15.4)	019790
	611 FORMAT (1H0,2X,*K*,7X,*ALT*,8X,*MR O3*,11X,*FC11*,11X,*FC12*,10X,	019800
	1 *CH3CL*,11X,*CCL4*,11X,*CLX*//)	019810
	612 FORMAT (1H0,2X,*K*,7X,*ALT*, 9X,*N20*,12X,*NOX*,12X,*CH4*//)	019820
	613 FORMAT (1H , I3,0PF11.0,1P3E15.4)	019830
	614 FORMAT (1H0,1X,*K*,7X,*ALT*,6X,*H + O3*,7X,*OH + O3*,5X,	019840
	1 *H02 + O3*,6X,*H02 + O*,6X,*OH + O*,7X,*NO2 + O*,6X,*CLO + O*,	019850
	2 6X,*O + O3*, 7X,*O2 + HV*//)	019860


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615 FORMAT (1H ,I2,0PF11.0,1P9E13.4) 019870
616 FORMAT (1H0,2X,*K*,7X,*ALT*,6X,*H2O + HV*,6X,*H2O + O1D*,5X, 019880
1 *CH4 + O1D*,5X,*HNO3 + HV*,5X,*CO + OH*,7X,*NO + H02*,5X, 019890
2 *JH2O2+H2O2*,5X,*CL + CH4*//) 019900
617 FORMAT (1H , I3,0PF11.0,1P7E15.4) 019910
618 FORMAT (1H0,2X,*K*,7X,*ALT*,5X,*H2O2 + OH*,4X,*H02 + OH*,5X, 019920
1 *HCL + OH*,5X,*CH4 + OH*,5X,*OH + H02*,5X,*OH + HNO3*,5X, 019930
2 *OH + OH*,5X,*H + H02*,5X,*CL + H02*//) 019940
714 FORMAT (1H0,* INTEGRATED LOSS FOR OZONE*//) 019950
715 FORMAT (1H ,I3X,1P9E13.4) 019960
1601 FORMAT (1H0,5X,*LAST ITERATION + 1* // 5X,*ALT*,6X,*CJ02*, 7X, 019970
1 *CJ03*, 6X,*CJCF2*, 6X,*CJCF3*,6X,*CJ031*,5X,*PREV03*,5X, 019980
2 *DO3INT*,5X,*DMINT*,6X,*PREV0H*//) 019990
1603 FORMAT (1H0,5X,*LAST ITERATION + 1*// 020000
A 6X,*ALT*,5X,*CJCL03*,5X,*CJN20*, 020010
1 6X,*CJHNO3*,5X,*CJH2O2*,5X,*CJN205*,5X,*CJCL4*,4X,*CJCH3CL*//) 020020
C 020030
END 020040
SUBROUTINE TRAP (XX,XXX,N1,N2) 020050
DIMENSION XX(81) 020060
XXX = (XX(N1) + XX(N2))* .5 020070
N1+1 = N1 + 1 020080
N2M1 = N2 - 1 020090
DO 10 I = N1P1,N2M1 020100
10 XXX = XXX + XX(I) 020110
XXX = XXX*1.0E5 020120
RETURN 020130
END 020140
SUBROUTINE PRINT9 (X1,X2,X3,X4,X5,X6,X7,X8,X9,HD1,HD2,HD3,HD4,HD5, 020150
1 HD6,HD7,HD8,HD9) 020160
DIMENSION X1(81),X2(81),X3(81),X4(81),X5(81),X6(81),X7(81),X8(81), 020170
1 X9(81) 020180
COMMON /MODEL/ALT(41),TEMP(41),JH(41),O1D(41),DA23(41) 020190
600 FORMAT (1H0,6X,*ALT*,2X,9(6X,A4,3X)//) 020200
601 FORMAT (1X,0P=11.0,1P9E13.4) 020210
603 FORMAT (1H0,5X,*MIXING RATIOS*//) 020220
C 020230
CALL PAGE 020240
WRITE (6,603) 020250
WRITE (6,600) HD1,HD2,HD3,HD4,HD5,HD6,HD7,HD8,HD9 020260
DO 60 I = 1,41 020270
60 WRITE (6,601) ALT(I),X1(2*I-1),X2(2*I-1),X3(2*I-1),X4(2*I-1), 020280
1 X5(2*I-1),X6(2*I-1),X7(2*I-1),X8(2*I-1),X9(2*I-1) 020290
RETURN 020300
END 020310
SUBROUTINE INPUT(KEYS,N,IC,IFORM,TITLE,K),RETURNS(A) 020320
C 020330
REAL NAME 020340
INTEGER KEYS(N),TITLE(13),KEYW(5),KEY(3),BLANK 020350
DATA KEYW/4H PARA,4H COMM,4H COMP,4H ENDJ,4H 9999/,BLANK/1H /, 020360
X NAME/5H INPJT/ 020370
C 020380
10 READ(5,5010)KEY,IC,IFORM,TITLE,JF 020390
5010 FORMAT(3A4,I3,I3,2X,12A4,2A2) 020400
IF(E0F(5))800,15 020410
15 IF(IC)20,49,22 020420
20 IC=-IC 020430
REWIND IC 020440
22 CALL PAGE 020450
CALL LINES(4),RETURNS(25) 020460
25 WRITE(6,6025)IC,TITLE 020470
6025 FORMAT(/T21,*TAPE*,I2,T31,*LABEL=*,12A4,A2//) 020480
IF(JF.NE.BLANK)CALL INE(IC,.TRUE.) 020490
READ(IC,5010)KEY,K,IFORM,TITLE,JF 020500
IF(E0F(IC))800,50 020510
49 IC=5 020520

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50	DO 60 K=1,5	020530
	IF(KEY(1).EQ.KEYM(K))GO TO (100,200,10,400,10),K	020540
60	CONTINUE	020550
	DO 80 K=1,N	020560
	IF(KEY(1).EQ.KEYS(K))GO TO 90	020570
80	CONTINUE	020580
	CALL ERRX(80,NAME)	020590
90	IF(IC.EQ.5)CALL PAGE	020600
	WRITE(6,6090)KEY,TITLE,IC	020610
6090	FORMAT(/T2,3A4,T21,12A4,A2,T81,*(UNIT *,I2,*)*/)	020620
	CALL LINES(3),RETURNS(95)	020630
95	RETURN	020640
100	CALL INPARM	020650
	GO TO 10	020660
200	CALL INE(IC,.TRUE.)	020670
	GO TO 10	020680
800	CALL ERRM(800,NAME),RETURNS(400)	020690
400	RETURN A	020700
	END	020710
	SUBROUTINE PAGE	020720
C	*****	020730
C	PRINTS PAGE HEADER AND KEEPS TRACK OF LINE COUNT	020740
C	VERSION 1.0 LEVEL 711122	020750
C	*****	020760
	INTEGER ICODE,IRUN,NPAGE	020770
	REAL TITLE(6)	020780
	COMMON /HEAD/ TITLE,ICODE,VERS,LEVEL,DAT, IRUN,NPAGE,NLOG	020790
	COMMON/LINUM/LINE	020800
C	-----	020810
	LINE=4	020820
	NPAGE=NPAGE+1	020830
	WRITE (6,2030) ICODE,IRUN,TITLE,VERS,LEVEL,DAT, NPAGE	020840
2030	FORMAT(*1*,I3,I6,5X,6A8,* VERSION *,F5.1,* (*,I6,*)*,11X,	020850
X	A10,10X,*PAGE *,I3/1X,127(*--))	020860
	RETURN	020870
	END	020880
	SUBROUTINE LINES(N),RETURNS(A)	020890
C	*****	020900
C	VERSION 1.0 LEVEL 760921	020910
C	*****	020920
	REAL TITLE(6)	020930
	INTEGER ICODE,IRUN,NPAGE,LCT	020940
	COMMON /HEAD/ TITLE,ICODE,VERS,LEVEL,DATE,IRUN,NPAGE,NLOG	020950
	COMMON/LINUM/LINE	020960
	DATA LCT/61/	020970
C	-----	020980
	LINE=LINE+N	020990
	IF(LINE.LT.LCT) RETURN	021000
	LINE=N+4	021010
30	NPAGE=NPAGE+1	021020
	WRITE(6,2030) ICODE,IRUN,TITLE,VERS,LEVEL,DATE,NPAGE	021030
2030	FORMAT(*1*,I3,I6,5X,6A8,* VERSION *,F5.1,* (*,I6,*)*,11X,	021040
X	A10,10X,*PAGE *,I3/1X,127(*--))	021050
	RETURN A	021060
	END	021070
	SUBROUTINE INE(IC,PRINT)	021080
C	*****	021090
C	VERSION 1 LEVEL 720602	021100
C	READS AND PRINTS COMMENTS CARDS	021110
C	*****	021120
	REAL NAME	021130
	LOGICAL PRINT	021140
	INTEGER IFORM,IF(3),COM(13),BLANK	021150
	DATA IF/1H,1H0,1H1/,NAME/3HINE/,BLANK/1H /	021160
C	-----	021170
10	READ(IC,5010) IFORM,COM,JF	021180

5010	FORMAT(14X,A1,5X,12A4,A2,A2)	021130
	IF(.NOT.PRINT) GO TO 50	021200
	DO 20 I=1,3	021210
	IF(I.FORM.EQ.IF(I)) GO TO (30,30,40),I	021220
20	CONTINUE	021230
	CALL ERRX(20,NAME)	021240
30	CALL LINES(I),RETURNS(32)	021250
32	WRITE(6,6032) IF(I),COM	021260
6032	FORMAT(A1,F21,12A4,A2)	021270
	GO TO 50	021280
40	CALL PAGE	021290
	I=2	021300
	GO TO 30	021310
50	IF(.JF.NE.BLANK) GO TO 10	021320
	RETURN	021330
	END	021340
	SUBROUTINE JAY	021350
	*****	021360
	VERSION 1.0 LEVEL 760921	021370
	*****	021380
	REAL TITLE(5)	021390
	COMMON /HEAD/ TITLE,ICODE,VERS,LEVEL,DAT,IRJN,NPAGE,NLOG	021400
	-----	021410
	DAT = DATE(J)	021420
	RETURN	021430
	END	021440
	SUBROUTINE ERRX(N,NAME)	021450
	*****	021460
	VERSION 2 LEVEL 720421	021470
	*****	021480
	INTEGER N	021490
	REAL NAME	021500
	-----	021510
	WRITE(6,6000) N,NAME	021520
6000	FORMAT(*OEXECUTION TERMINATED DUE TO ERROR NO. *,I4,* IN *,A8)	021530
	STOP	021540
	END	021550
	SUBROUTINE ERRN(N,NAME)	021560
	*****	021570
	VERSION 1.0 LEVEL 760921	021580
	*****	021590
	INTEGER N	021600
	REAL NAME	021610
	-----	021620
	WRITE(6,6100) N,NAME	021630
6100	FORMAT(*OERROR NO. *,I4,* IN *,A8/)	021640
	RETURN	021650
	END	021660
	SUBROUTINE JSCATT	021670
	*****	021680
	CHLORINE MODEL STUDY PROGRAM	021690
	-----	021700
	SUBROUTINE JSCATT COMPUTES AEROSOL AND MOLECULAR EXTINCTION	021710
	COEFFICIENTS	021720
	RAY(J)= RAYLEIGH SCATTERING COEFFICIENT	021730
	QAE(J)= AEROSOL EXTINCTION COEFFICIENT	021740
	QAA(J)= AEROSOL ABSORPTION COEFFICIENT	021750
	-----	021760
	SIZE DISTRIBUTION PARAMETER ISIZE= 1 (RURAL) FROM SELBY ET AL	021770
	2 (MARITIME) (1976)	021780
	3 (URBAN)	021790
	4 (TROPOSPHERE)	021800
	5 (SPECIAL)	021810
	-----	021820
	TO INPUT SPECIAL MODEL DIMENSION ALAM(8) AND DE(5).QA(5)	021830
	-----	021840

C	N= # OF WAVELENGTH INTERVALS AEROSOL DATA DIGITIZED	021850
C	ALAM= ARRAY OF WAVELENGTH VALUES CORRESPONDING TO DIGITIZATION	021860
C	021870
	COMMON /SCAPAR/GRAY(100),QAE(100),QAA(100)	021880
	COMMON /SOLCON/ML(100),FL(100),Q02(100),Q03(100)	021890
	COMMON /PARM/ ISWIT,TSTEP,TSTOP,TLOOP,ITPRNT,ISIZE,ISCAIT	021900
	DIMENSION ALAM(8),QE(5,8),QA(5,8)	021910
	DATA ALAM/.200,.250,.300,.400,.488,.550,.694,.860/	021920
	DATA IL,IU,N/1,99,7/	021930
C		021940
C	SPECIFY AEROSOL MODEL	021950
	GO TO (1,2,3,4,5) ISIZE	021960
C	RURAL	021970
1	QE(1,1)=.38223	021980
	QE(1,2)=.32979	021990
	QE(1,3)=.28540	022000
	QE(1,4)=.22026	022010
	QE(1,5)=.17989	022020
	QE(1,6)=.15800	022030
	QE(1,7)=.12864	022040
	QE(1,8)=.09151	022050
	QA(1,1)=.07945	022060
	QA(1,2)=.03661	022070
	QA(1,3)=.02110	022080
	QA(1,4)=.01317	022090
	QA(1,5)=.01114	022100
	QA(1,6)=.01095	022110
	QA(1,7)=.00968	022120
	QA(1,8)=.01058	022130
	GO TO 20	022140
C	MARITIME	022150
2	QE(2,1)=.20932	022160
	QE(2,2)=.19518	022170
	QE(2,3)=.18479	022180
	QE(2,4)=.17032	022190
	QE(2,5)=.16213	022200
	QE(2,6)=.15900	022210
	QE(2,7)=.15001	022220
	QE(2,8)=.14412	022230
	QA(2,1)=.02054	022240
	QA(2,2)=.00864	022250
	QA(2,3)=.00442	022260
	QA(2,4)=.00243	022270
	QA(2,5)=.00193	022280
	QA(2,6)=.00186	022290
	QA(2,7)=.00155	022300
	QA(2,8)=.00171	022310
	GO TO 20	022320
C	URBAN	022330
3	QE(3,1)=.31030	022340
	QE(3,2)=.28416	022350
	QE(3,3)=.25805	022360
	QE(3,4)=.20867	022370
	QE(3,5)=.17631	022380
	QE(3,6)=.15900	022390
	QE(3,7)=.12601	022400
	QE(3,8)=.10071	022410
	QA(3,1)=.10692	022420
	QA(3,2)=.08649	022430
	QA(3,3)=.07571	022440
	QA(3,4)=.06376	022450
	QA(3,5)=.05674	022460
	QA(3,6)=.05282	022470
	QA(3,7)=.04528	022480
	QA(3,8)=.04022	022490
	GO TO 20	022500

3	TROPOSPHERE	022510
4	QE(4,1)=.40212	022520
	QE(4,2)=.34505	022530
	QE(4,3)=.29674	022540
	QE(4,4)=.22585	022550
	QE(4,5)=.18187	022560
	QE(4,6)=.15800	022570
	QE(4,7)=.11722	022580
	QE(4,8)=.08537	022590
	QA(4,1)=.08042	022600
	QA(4,2)=.03451	022610
	QA(4,3)=.01767	022620
	QA(4,4)=.00371	022630
	QA(4,5)=.00772	022640
	QA(4,6)=.00745	022650
	QA(4,7)=.00619	022660
	QA(4,8)=.00683	022670
	GO TO 20	022680
5	CONTINUE	022690
3	INPUT SPECIAL MODEL	022700
20	DO 40 J=IL,IU	022710
	WLM1C=WLM(J)/1.0E4	022720
	QRAY(J)=(9.307E-20)*(1.0E4/WLM1C)**4.0117	022730
	QRAY(J)=QRAY(J)*1.E-5	022740
	IF(WLM1C.LT.0.2)GO TO 35	022750
	DO 30 K=1,N	022760
	KP1=K+1	022770
	IF(WLM1C.GE.ALAM(K).AND.WLM1C.LE.ALAM(KP1))GO TO 31	022780
30	CONTINUE	022790
31	XD=WLM1C-ALAM(K)	022800
	QAE(J)=(QE(ISIZE,KP1)-QE(ISIZE,K))*XD/(ALAM(KP1)-ALAM(K))+	022810
1	QE(ISIZE,K)	022820
	QAE(J)=QAE(J)*1.E-5	022830
	QAA(J)=(QA(ISIZE,KP1)-QA(ISIZE,K))*XD/(ALAM(KP1)-ALAM(K))+	022840
1	QA(ISIZE,K)	022850
	QAA(J)=QAA(J)*1.E-5	022860
	GO TO 40	022870
35	QAE(J)=0.0	022880
	QAA(J)=0.0	022890
40	CONTINUE	022900
	WRITE(6,101) ISIZE	022910
101	FORMAT(* AEROSOL MODEL =*,I4)	022920
	WRITE(6,105)	022930
105	FORMAT(3X,*J*,11X,*WLM(J)*,8X,*QRAY(J)*,9X,*QAE(J)*,9X,*QAA(J)*)	022940
	DO 50 J=IL,IU	022950
	WRITE(6,102) J,WLM(J),QRAY(J),QAE(J),QAA(J)	022960
102	FORMAT(I4,4E15.4)	022970
50	CONTINUE	022980
	RETURN	022990
	END	023000
	SUBROUTINE OMEGA(NT,IL,IU,GMU)	023010
C.....		023020
C	SUBROUTINE OMEGA COMPUTES SINGLE SCATTERING ALBEDO PROFILE AND	023030
C	OPTICAL DEPTH AS A FUNCTION OF ALTITUDE	023040
C	SINGLE SCATTERING ALBEDO PROFILE AS A FUNCTION OF TAU COMPUTED	023050
C	FOR INPUT TO VIN	023060
C		023070
C	MEAN INTENSITY RETURNED AS A FUNCTION OF TAU REINTERPOLATED	023080
C	FOR ALTITUDE LEVELS	023090
C		023100
C	RETURN TO COMPI	023110
C.....		023120
	COMMON /SCAPAR/QRAY(100),QAE(100),QAA(100)	023130
	COMMON /SOLCON/WLM(100),FL(100),J02(100),Q03(100)	023140
	COMMON /INTDEN/DO3INT(41),DMINT(41),DAINT(41)	023150
	COMMON /MODEL/ALT(41),TEMP(41),DN(41),DID(41),DA23(41)	023160

	COMMON /SPECIE/H(41),OH(41),HO2(41),H2O2(41),O3(41),J(41),NO(41),	023170
	1 NO2(41),HNO3(41),NOX(41),CO(41),O2(41),CH4(41),H2O(41),H2(41),	023180
	2 CL(41),CLO(41),HCL(41),CLX(41),DCLX(41),NO3(41),N2O5(41),	023190
	3 CLNO3(41)	023200
	COMMON /VRP/TAUZ(41,100),OMEGAZ(41,100),TAU(41),OMEGAT(41)	023210
	COMMON/SCA/TAUINT(100),F(41,100),FAV(41,100),FLUX(41)	023220
	COMMON /PARA/ U0,N,N1,N2,NN,NNP1,REF	023230
	DIMENSION IN(100),INN(100),II(41)	023240
C		023250
C	COMPUTE OPTICAL DEPTH AND ALBEDO AS A FUNCTION OF	023260
C	WAVELENGTH FOR EACH LEVEL	023270
	P02=0.21	023280
	J0=GMU	023290
	DO 20 I=1,NT	023300
	DO 10 J=IL,IU	023310
	TAUZ(I,J)=Q03(J)*D03INT(I)+Q02(J)*P02*DMINT(I)+QRAY(J)*DMINT(I)	023320
	1 /DM(I)+QAE(J)*DAINT(I)/DA23(1)	023330
	GAMSCA=QRAY(J)*DM(I)/DM(1)+(QAE(J)-QAA(J))*DA23(I)/DA23(1)	023340
	GAMEXT=QAE(J)*DA23(I)/DA23(1)+QRAY(J)*DM(I)/DM(1)+Q03(J)*	023350
	1 O3(I)+Q02(J)*P02*DM(I)	023360
	OMEGAZ(I,J)=GAMSCA/GAMEXT	023370
	IF(I.NE.NT)GO TO 10	023380
	TZ=TAUZ(1,J)	023390
	N=TZ/.5+1.6	023400
	IF(N.LT.3)N=3	023410
	IF(N.GT.21)N=21	023420
	IN(J)=N	023430
	NN=(N-1)*2	023440
	IF(TZ.LE.1.)NN=10	023450
	IF(TZ.GT.1..AND.TZ.LE.3.)NN=(N-1)*5	023460
	IF(TZ.GT.3..AND.TZ.LE.5.)NN=(N-1)*3	023470
	INN(J)=NN	023480
	TAUINT(J)=TZ/NN	023490
10	CONTINUE	023500
20	CONTINUE	023510
C	COMPUTE SINGLE SCATTERING ALBEDO VS TAU AT EQUAL TAU INTERVALS	023520
	DO 50 J=IL,IU	023530
	NN=INN(J)	023540
	NNP1=NN+1	023550
	II(1)=1	023560
	II(NNP1)=NT	023570
	TAU(1)=TAUZ(1,J)	023580
	TAU(NNP1)=0.0	023590
	OMEGAT(1)=OMEGAZ(1,J)	023600
	OMEGAT(NNP1)=OMEGAZ(NT,J)	023610
	DO 40 K=2,NN	023620
	KK=NNP1-K	023630
	TAU(K)=TAUINT(J)*KK	023640
	DO 30 I=1,NT	023650
	IM1=I-1	023660
	DELTAU=TAU(K)-TAUZ(I,J)	023670
	IF(DELTAU)30,35,35	023680
30	CONTINUE	023690
	GO TO 40	023700
35	OMEGAT(K)=(OMEGAZ(IM1,J)-OMEGAZ(I,J))*DELTAU/(TAUZ(IM1,J)	023710
	1 -TAUZ(I,J))+OMEGAZ(I,J)	023720
	II(K)=I	023730
40	CONTINUE	023740
	NN=INN(J)	023750
	NNP1=NN+1	023760
	N=INN(J)	023770
	N1=N-1	023780
	N2=N-2	023790
	DO 85 I=1,NT	023800
	IF(OMEGAZ(I,J).GT..05)GO TO 88	023810
85	CONTINUE	023820

	DO 86 I=1,NF	023830
	FR=0.	023840
	IF(-TAUZ(1,J)/GMU.LF.-70.)GO TO 87	023950
	FR=GMU*2.*REF*E2(TAUZ(1,J)-TAUZ(I,J))*EXP(-TAUZ(1,J)/GMU)	023960
87	F(I,J)=FR	023970
	IF(-TAUZ(I,J)/GMU.LF.-70.)GO TO 86	023980
	F(I,J)=EXP(-TAUZ(I,J)/GMU)*FR	023990
86	CONTINUE	023900
	GO TO 50	023910
88	CALL VIM	023920
C	CONVERT FLUX FROM TAU TO Z LEVELS FOR COMPI	023930
	F(1,J)=FLUX(1)	023940
	F(NF,J)=FLUX(NNP1)	023950
	DO 70 K=2,NN	023960
	IKL=II(K)	023970
	IKU=II(K+1)	023980
	IF(IKL.EQ.IKU)GO TO 70	023990
	IKU=IKU-1	024000
	DO 60 I=IKL,IKU	024010
	KP1=K+1	024020
	TAUEXP=TAU(K)-TAUZ(I,J)	024030
	TAUEXP=TAUEXP/TAUINT(J)	024040
	F(I,J)=(FLUX(KP1)**TAUEXP)*(FLUX(K)**(1.-TAUEXP))	024050
50	CONTINUE	024060
70	CONTINUE	024070
50	CONTINUE	024080
	RETURN	024090
	END	024100
	SUBROUTINE VIM	024110
2	024120
C	VARIATIONAL ITERATIVE METHOD CALCULATES ATMOSPHERIC MULTIPLE	024130
C	SCATTERING AND SURFACE REFLECTION EFFECTS WHICH AFFECT PHOTO-	024140
C	DISSOCIATION RATES	024150
C		024160
C	INPUT INFORMATION INCLUDES SURFACE REFLECTION COEFFICIENT,	024170
C	SINGLE SCATTERING ALBEDO AND OPTICAL DEPTH PROFILES	024180
C	RESULTANT FLUX ADJUSTMENT PROFILE RETURNS TO OMEGA	024190
C		024200
C	ADAPTED FROM 4. K. BURKE, E.R.T., INC. 1977	024210
C	024220
	LOGICAL LINEQV	024230
	REAL M,MIN,INT	024240
	COMMON /PARA/ U0,N,N1,N2,NN,NNP1,REF	024250
	COMMON/SCA/TAUINT(100),Q(41,100),FAV(41,100),FLUX(41)	024260
	COMMON /VRP/TAUZ(41,100),OMEGAZ(41,100),TAU(41),OMEGAT(41)	024270
	COMMON /MATRIX/M(20,21)	024280
	COMMON /MES4/ T(21),G(101),W(21)	024290
	COMMON /EFUN/ E3T(21),E2T(101),E3TT(101),E3F1(101),E2TT(101)	024300
	COMMON /COEFF/ A(20),AA(20)	024310
	DIMENSION S1(101),T1(101),S0(101)	024320
	DIMENSION SS2(101),F(101),F0(101),F1(101),F2(101)	024330
	DIMENSION GG(101),FF(21),WW(101)	024340
	DIMENSION U(50),INT(50),GA(101)	024350
	DIMENSION F3(101),EK(101)	024360
	4 FORMAT(/'1',6X,'MATRIX ELEMENTS, WL=',I4)	024370
	5 FORMAT(4X,1P11E11.3)	024380
	6 FORMAT(/,9X,'TA',8X,'A(J)',10X,'AA(J)')	024390
	7 FORMAT(6X,E9.3,2E16.6)	024400
	9 FORMAT(* SINGULAR MATRIX*)	024410
	11 FORMAT('1',9X,'T1',9X,'1ST ITERATION',5X,'OMEGA')	024420
	12 FORMAT(6X,E9.3,5X,E14.6,5X,E14.6)	024430
	13 FORMAT(/,9X,'ITERATION= ',I5,/,9X,'T1',9X,'NEW ITERA',9X,'LAST	024440
	ITERA',9X,'JEL')	024450
	14 FORMAT(6X,E9.3,3(5X,E14.6))	024460
	16 FORMAT(/,9X,'NOT CONVERGE')	024470
	17 FORMAT(4X,F7.3,5(5X,E14.6))	024480

	18 FORMAT(///,7X,*T*,10X,*F*,19X,*=0*,18X,*F1*,18X,*F2*,18X,*F3*)	024490
C		024500
C	DEFINE T1 AND W SUCH THAT K=1 CORRESPONDS TO TOP OF ATMOSPHERE,	024510
C	K=NNP1 IS BOTTOM OF ATMOSPHERE	024520
C		024530
	DO 111 K=1,NNP1	024540
	NK=NNP1-K+1	024550
	T1(K)=TAU(NK)	024560
111	WW(K)=OMEGA(T(K))	024570
	DO 45 K=1,NNP1	024580
	E2T(K)=E2(T1(K))	024590
	E3T1(K)=E3(T1(K))	024600
	E2TT(K)=E2(T1(NNP1)-T1(K))	024610
	E3TT(K)=E3(T1(NNP1)-T1(K))	024620
	EX(K)=EXP(-T1(K)/U0)	024630
45	CONTINUE	024640
	OT=T1(NNP1)/N1	024650
	K=0	024660
	L=NN/N1+.1	024670
C		024680
C	COMPUTE T AND W PROFILES	024690
C		024700
	T(V)=OT*N1	024710
	E3T(N)=E3(T(N))	024720
	DO 10 J=1,N1	024730
	T(J)=OT*(J-1)	024740
	E3T(J)=E3(T(J))	024750
	SUM=0.	024760
	DO 15 KK=1,L	024770
	K=K+1	024780
	SUM=SUM+WW(K)	024790
15	W(J)=SUM/L	024800
10	CONTINUE	024810
	DO 46 K=1,NNP1	024820
	S0(K)=.5*WW(K)*(E2T(K)*U0*REF+.5)*EX(K)	024830
46	CONTINUE	024840
	CALL RMATRI	024850
	DO 20 J=1,N1	024860
	FF(J)=M(J,N)	024870
20	CONTINUE	024880
	IF (LINEQN(N-1)) GO TO 100	024890
	DO 25 J=1,N1	024900
	TA=(T(J)+T(J+1))*0.5	024910
C		024920
C	THIS IS T AVERAGE FOR EACH LAYER	024930
C		024940
	A(J)=M(J,N)	024950
C		024960
C	THIS IS SOLUTION TO MATRIX EQN	024970
C		024980
	AA(J)=SQRT(W(J))*A(J)	024990
C		025000
C	THIS IS AVERAGE SOURCE IN THE INTERVAL	025010
C		025020
	25 CONTINUE	025030
	GO TO 200	025040
100	WRITE(6,9)	025050
	GO TO 400	025060
200	S2=0.	025070
	DO 40 J=1,N1	025080
	JP1=J+1	025090
	SS2(J)=AA(J)*(E3(T(N))-T(JP1))-E3(T(N))-T(J))	025100
	S2=S2+SS2(J)	025110
40	CONTINUE	025120
	DO 30 K=1,NNP1	025130
	X=T1(K)	025140

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ENVIRONMENTAL RESEARCH AND TECHNOLOGY INC CONCORD MASS F/6 4/1
DEVELOPMENT OF THE RADIATIVE TRANSFER PORTION OF A 1-D PHOTOCHE--ETC.(U)
MAR 78 R G ISAACS, H K BURKE, N TRIPP F19628-77-C-0078

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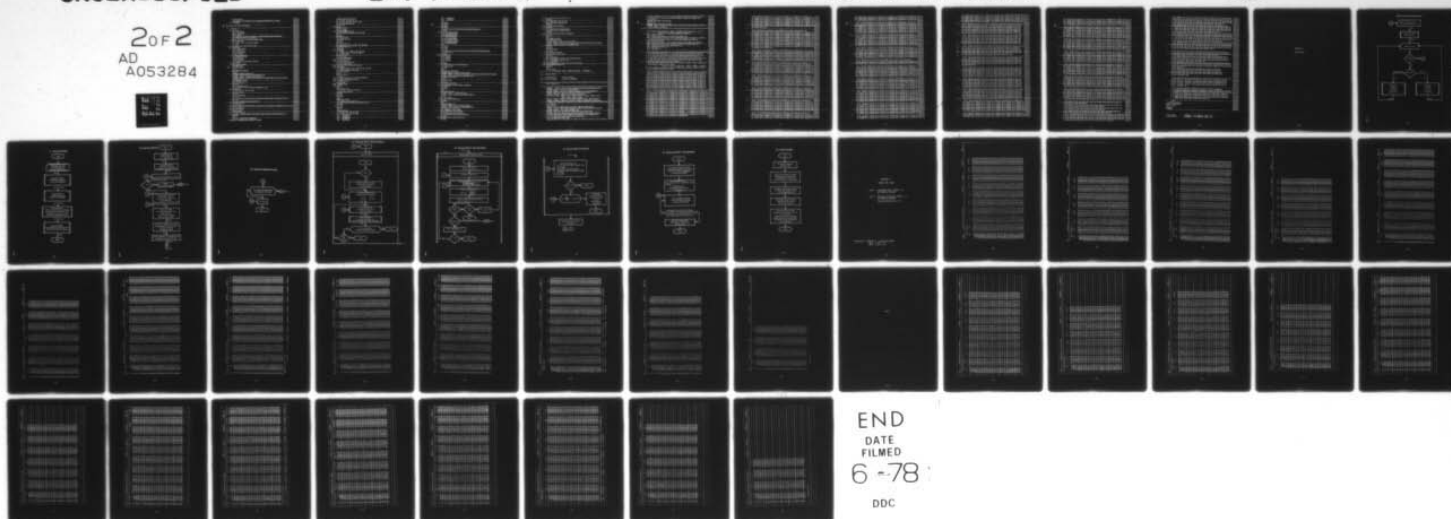
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DDC

S1(K)=S11(X)	025150
G(K)=S0(K)+.5*WH(K)*S1(K)+.5*WH(K)*REF*E2TT(K)*S2*2.	025160
30 CONTINUE	025170
C	025180
C RESULT OF 1ST ITERATION	025190
C	025200
II=2	025210
300 DIFF=0.	025220
CALL COMP(SG)	025230
DO 35 K=1,NNP1	025240
GG(K)=G(K)	025250
G(K)=S0(K)+.5*WH(K)*S1(K)+.5*WH(K)*REF*E2TT(K)*S2*2.	025260
DEL=ABS((GG(K)-G(K))/G(K))	025270
WRITE (6,14) T1(K),G(K),GG(K),DEL	025280
35 DIFF=DIFF+DEL	025290
IF (DIFF .LE. .1) GO TO 400	025300
II=II+1.	025310
IF (II .LT. 10.) GO TO 300	025320
400 CONTINUE	025330
Y=EXP(-T(N)/U0)	025340
CALL COMP(SG)	025350
DO 50 K=1,NNP1	025360
F0(K)=EX(K)	025370
F1(K)=2.*S1NT(K)	025380
X=2.*REF*E2TT(K)	025390
F2(K)=X*SG*2.	025400
F3(K)=X*U0*Y	025410
F(K)=F0(K)+F1(K)+F2(K)+F3(K)	025420
50 CONTINUE	025430
DO 333 K=1,NNP1	025440
NK=NNP1-K+1	025450
333 FLJX(K)=F(NK)	025460
END	025470
SUBROUTINE RMATRI	025480
REAL M	025490
COMMON /MATRIX/ M(20,21)	025500
COMMON /PARAM/ U0,N,N1,N2,NN,NNP1,REF	025510
COMMON /MESH/ T(21),G(101),W(21)	025520
COMMON /EFUN/ E3T(21),E2T(101),E3TT(101),E3T1(101),E2TT(101)	025530
DIMENSION DH(21)	025540
DIMENSION TJ(21)	025550
DO 10 J=1,N1	025560
JP1=J+1	025570
DH(J)=T(JP1)-T(J)	025580
M(J,J)=DH(J)-W(J)*(DH(J)+E3(DH(J))-.5)	025590
10 CONTINUE	025600
IF (N .EQ. 3) GO TO 100	025610
DO 20 I=1,N2	025620
IP1=I+1	025630
DO 20 J=IP1,N1	025640
JP1=J+1	025650
EE= E3(T(J)-T(I))-E3(T(J)-T(IP1))-E3(T(JP1)-T(I))+E3(T(JP1)-	025660
T(IP1))	025670
M(I,J)=.5*SQR(M(I)*M(J))*EE	025680
20 M(J,I)=M(I,J)	025690
GO TO 200	025700
100 M(1,2)=.5*SQR(M(1)*M(2))*(E3(DH(1))+E3(DH(2))-E3(DH(1)+DH(2))-.5)	025710
M(2,1)=M(1,2)	025720
200 DO 30 J=1,N1	025730
TU(J)=T(J)	025740
TU(J+1)=T(J+1)	025750
30 M(J,N)=.25*U0*(EXP(-TU(J)/U0)-EXP(-TU(J+1)/U0))*(M(J))**.5	025760
RETURN	025770
END	025780
LOGICAL FUNCTION LINEQN(N)	025790
C GAUSSIAN ELIMINATION METHOD IS USED	025800

COMMON/MATRIX/A(20,21)	025810
IF (N .GT. 1) GO TO 10	025820
IF (A(1,1).EQ.0.) GO TO 500	025830
A(1,2)=A(1,2)/A(1,1)	025840
GO TO 420	025850
10 SUM=0.	025860
DO 20 I=1,N	025870
DO 20 J=1,N	025880
20 SUM=SUM+ABS(A(I,J))	025890
TOLER=(SUM/FLOAT(N)**2)*1.E-10	025900
N1=N-1	025910
NP1=N+1	025920
DO 300 K=1,N1	025930
TEMP=ABS(A(K,K))	025940
ITEMP=K	025950
KP1=K+1	025960
DO 100 I=KP1,N	025970
IF(ABS(A(I,K)).LE.TEMP) GO TO 100	025980
TEMP=ABS(A(I,K))	025990
ITEMP=I	026000
100 CONTINUE	026010
IF (TEMP .LE. TOLER) GO TO 500	026020
IF (ITEMP .EQ. K) GO TO 200	026030
DO 110 I=K,NP1	026040
TEMP=A(K,I)	026050
A(K,I)=A(ITEMP,I)	026060
110 A(ITEMP,I)=TEMP	026070
200 DO 210 I=KP1,N	026080
A(I,K)=A(I,K)/A(K,K)	026090
DO 210 J=KP1,NP1	026100
210 A(I,J)=A(I,J)-A(I,K)*A(K,J)	026110
300 CONTINUE	026120
IF (ABS(A(N,N)) .LE. TOLER) GO TO 500	026130
A(N,NP1)=A(N,NP1)/A(N,N)	026140
DO 410 I=1,N1	026150
K=N-I	026160
DO 400 J=1,I	026170
L=NP1-J	026180
400 A(K,NP1)=A(K,NP1)-A(K,L)*A(L,NP1)	026190
410 A(K,NP1)=A(K,NP1)/A(K,K)	026200
420 LINEQN=.FALSE.	026210
GO TO 600	026220
500 LINEQN=.TRUE.	026230
600 RETURN	026240
END	026250
FUNCTION E2(X)	026260
IF (X .LE. 1.0E-6) GO TO 1	026270
E2=EXP(-X)-X*E(X)	026280
RETURN	026290
1 E2=1.0	026300
RETURN	026310
END	026320
FUNCTION E3(X)	026330
IF (X.LE.1.0E-6) GO TO 1	026340
E3=(EXP(-X)-X*(EXP(-X)-X*E(X)))*0.5	026350
RETURN	026360
1 E3= .5	026370
RETURN	026380
END	026390
FUNCTION E(X)	026400
IF (X.GE.10.) GO TO 200	026410
IF (X.GE.1.0) GO TO 100	026420
A0=-.57721566	026430
A1=.99999193	026440
A2=-.24991055	026450
A3=.05519968	026460

A4=-.00976004	026470
A5=.00107857	026480
X1=X	026490
X2=X*X1	026500
X3=X*X2	026510
X4=X*X3	026520
X5=X*X4	026530
E=A0+A1*X1+A2*X2+A3*X3+A4*X4+A5*X5-ALOG(X)	026540
RETURN	026550
100 A1=8.573328740100	026560
A2=18.059016973000	026570
A3=8.634760892500	026580
A4=.267773734300	026590
B1=9.573322345400	026600
B2=25.632956148600	026610
B3=21.899650382700	026620
B4=3.958496922800	026630
X1=X	026640
X2=X*X1	026650
X3=X*X2	026660
X4=X*X3	026670
F=(X4+A1*X3+A2*X2+A3*X1+A4)/(X4+B1*X3+B2*X2+B3*X1+B4)	026680
E=F*EXP(-X)/X	026690
RETURN	026700
200 A1=4.03640	026710
A2=1.15198	026720
B1=5.03637	026730
B2=4.19160	026740
X1=X	026750
X2=X*X1	026760
F=(X2+A1*X1+A2)/(X2+B1*X1+B2)	026770
E=F*EXP(-X)/X	026780
RETURN	026790
END	026800
SUBROUTINE COMP(SG)	026810
COMMON /MESH/ T(21),G(101),W(21)	026820
COMMON /EFUN/ E3T(21),E2T(101),E3TT(101),E3T1(101),E2TT(101)	026830
COMMON /PARA/ J0,N,N1,N2,NN,NNP1,REF	026840
DIMENSION G4(101)	026850
SUM=0.	026860
DO 10 K=1,NN	026870
KP1=K+1	026880
GM(K)=G(K)+G(KP1)	026890
10 SUM=SUM+GM(K)*(E3TT(KP1)-E3TT(K))	026900
SG=SUM*.5	026910
RETURN	026920
END	026930
FUNCTION S11(X)	026940
COMMON /COEFF/ A(20),AA(20)	026950
COMMON /PARA/ J0,N,N1,N2,NN,NNP1,REF	026960
S11=0.	026970
DO 10 J=1,N1	026980
10 S11=S11+AA(J)*SE(J,X)	026990
RETURN	027000
END	027010
FUNCTION SE(J,X)	027020
COMMON /MESH/ T(21),G(101),W(21)	027030
COMMON /PARA/ J0,N,N1,N2,NN,NNP1,REF	027040
IF(J.EQ.1) GO TO 100	027050
IF(J.EQ.N-1) GO TO 200	027060
IF(X.LE.T(J)) GO TO 300	027070
IF(X.GE.T(J+1)) GO TO 400	027080
SE=2.0-E2(X-T(J))-E2(T(J+1)-X)	027090
RETURN	027100
300 SE=E2(T(J)-X)-E2(T(J+1)-X)	027110
RETURN	027120

400	SE=E2(X-T(J+1))-E2(X-T(J))	027130
	RETURN	027140
100	IF(X.GE.T(2)) GO TO 500	027150
	SE=2.-E2(X)-E2(T(2)-X)	027160
	RETURN	027170
500	SE=E2(X-T(2))-E2(X)	027180
	RETURN	027190
200	IF(X.GE.T(N-1)) GO TO 600	027200
	SE=E2(T(N-1)-X)-E2(T(N)-X)	027210
	RETURN	027220
600	SE=2.0-E2(X-T(N-1))-E2(T(N)-X)	027230
	RETURN	027240
	END	027250
	FUNCTION SINT(I)	027260
	DIMENSION GM(101)	027270
	COMMON /MESH/ T(21),G(101),W(21)	027280
	COMMON /EFUN/ E3T(21),E2T(101),E3TT(101),E3T1(101),E2TT(101)	027290
	COMMON /PARA/ JO,N,N1,N2,NN,MNP1,REF	027300
	SUM1=0.	027310
	SUM2=0.	027320
	DO 10 K=1,NN	027330
	KP1=K+1	027340
10	GM(K)=G(K)+G(KP1)	027350
	IF(I.EQ.1) GO TO 100	027360
	I1=I-1	027370
	DO 20 K=1,I1	027380
20	SUM1=SUM1+GM(K)*(E2T(I-K)-E2T(I-K+1))	027390
	IF (I.EQ.MNP1) GO TO 200	027400
100	DO 30 K=I,NN	027410
30	SUM2=SUM2+GM(K)*(E2T(K-I+2)-E2T(K-I+1))	027420
200	SINT=(SUM1-SUM2)*.5	027430
	RETURN	027440
	END	027450
	BLOCK DATA	027460
C.....	CHLORINE MODEL STUDY PROGRAM - VERSION 4	027470
C.....	BLOCK DATA	027480
C.....	VERSION 4.0	027490
C.....	LEVEL 770214	027500
C.....	E.R.T., INC.	027510
C.....	L.PERRY, N.TRIPP	027520
C.....		027530
C.....		027540
	REAL TITLE(6)	027550
C.....		027560
C.....		027570
	COMMON /HEAD/ TITLE,ICODE,VERS,LEVEL,DATE,IRUN,NPAGE,NLOG	027580
	COMMON /EDDY/ FKK,I1,P11,P22,NEJOY	027590
	COMMON /MODEL/ ALT(41),TEMP(41),DH(41),DID(41),DA23(41)	027600
	COMMON /MOL4YD/ XH(81),XH20(81),PH20,R42,X11(81)	027610
	COMMON /MSCAT/ SCNO2,SCCL03,SCN202,SCN205	027620
	REAL JO2, JO3, JH20, JNO2, JN20, JN205, JHN03, JCH4, JCF2,	027630
X	JCF3, JHCL, JH202, JH0CL	027640
	COMMON /PARM/ ISWIT,TSTEP,TSTOP,TLOOP,ITPRNT,ISIZE,ISCAT	027650
	COMMON /PHRATE/ JO2(41),JO3(41),JH20(41),JN22(41),JN20(41),	027660
X	JN205(41),JHN03(41),JCH4(41),JCF2(41),JCF3(41),JHCL(41),JH202(41)	027670
Y	,JH0CL(41)	027680
	REAL JNO3	027690
	COMMON /RATES/ RATE(65,81),RA(65),RB(65),JNO3,PJO3	027700
	COMMON /RLOW/ RN20,RNOX,RCH4,RF11,RF12,RCH3,RCLX,RJCL4,R03	027710
	COMMON /SFACT/ FCL,FH20,FCLN03,*NO	027720
	COMMON /SOLJOY/ WL(100),FL(100),QO2(100),QO3(100)	027730
	COMMON /SOLCN1/ QCF2(100),QCF3(100),QCCL4(100),QCH3C(100),	027740
X	QCLN03(100),QN20(100),QHNO3(100),QH202(100),QN205(100),	027750
Y	QHCL(100),QH0CL(100),QH02(100),QH20(100)	027760
	REAL NO,NO2,NOX,NO3,N205	027770
	COMMON /SPECIE/ H(41),OH(41),HO2(41),H2O2(41),O3(41),O(41),NO(41),N27780	


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1 NO2(41),HNO3(41),NOX(41),CO(41),O2(41),CH4(41),H2O(41),H2(41), 027790
2 CL(41),CLO(41),HCL(41),CLX(41),DCLX(41),NO3(41),N2O5(41), 027800
3 CLNO3(41) 027810
COMMON /SPECOM/ FJ,FJFC,TL 027820
REAL LAT 027830
COMMON /WT/ A(6),DL,LAT,DEL 027840
COMMON /XRES/ X1(81),X2(81),X3(81),X4(81),X5(81),X6(81),X7(81), 027850
1 X8(81),X9(81),X10(81) 027860
C+++++ 027870
C 027880
DATA TITLE/3HCHLORINE,8M MODEL 5,8HTUDY PRO,4HGRAM,14 ,1M /, 027890
X DATE/1M /,NLOG/9/,IRUN/0/,NPAGE/0/ 027900
DATA JMO3/1.3E-2/ 027910
DATA FCL,FCLNO3,FH2O/1.0,1.00,1.0/,FNO/1.0/ 027920
DATA RN2O,RNOX,RCH4,RF11,RF12,RCH3C,RCLX,RCCL4/2.50E-7,2.00E10, 027930
1 1.50E-06,9.30E+06,1.30E+07,1.50E-09,1.00E+10,1.30E-10/ 027940
DATA RO3/3.00E-08/ 027950
DATA FJ,FJFC,TL/1.0,1.0,3.15E13/,FKK/1.0/,ISMIT/1/,NEDDY/0/ 027960
DATA I1,P11,P22/59,1.0,1.0/,PJ03/1.8E-4/,LAT,DEL/30.,0./ 027970
DATA SCNO2,SCCLO3,SCN2O2,SCN2O5/4*1.0/ 027980
DATA RH2,PH2O/5.E-7,0./ 027990
DATA X2/81*0./ 028000
C 028010
DATA RA/1.66E-12,2.35E-10,1.4E-10,1.0E-10,1.8E-32,2.6E-11,2.3E-12, 028020
A 1.0E-11,1.0E-13,1.0E-10,1.1E-11,0.,5.0E-12,2.0E-11,3.0E-11, 028030
B 1.0E-11,4.2E-10,2.1E-13,1.0E-10,2.0E-12,2.36E-12,0.,1.0E-12, 028040
C 1.7E-12,6.7E-12,5.7E-11,6.0E-13,3.8E-33,2.7E-11,7.29E-12, 028050
D 1.07E-10,2.0E-11,0.,1.05E-34,1.3E-11,1.0E-12,0.,3.7E-11,9.0E-6, 028060
E 2.30E-12,1.2E-13,9.12E-12,5.0E-11,7.0E-11,2.8E-11,5.5E-12, 028070
F 3.0E-10,3.0E-10,2*0.,2.0E-11,14*0./ 028080
DATA RB/-1070.,3*0.,340.,0.,-1125.,-750.,-1525.,-250.,-1000.,0., 028090
X -500.,3*0.,-350.,-115.,-250., 028100
A -313.,-1710.,0.,-600.,0.,-2010.,-2400.,0.,1055., 028110
B -257.,-1260.,-224.,2*0.,520.,-2140.,3*0.,-3700.,-1450.,-2450., 028120
C 4*0.,-3200.,4*0.,107.,14*0./ 028130
C 028140
DATA WL/937.8,949.7,970.0,972.5,977.0,1008.0,991.5,1026.8,1035.0, 028150
21050.0,1110.0,1155.0,1190.0,1210.0,1215.7,1250.0,1300.0,1350.0, 028160
31400.0,1450.0,1500.0,1550.0,1600.0,1650.0,1700.0,1750.0,1800.0, 028170
41850.0,1900.0,1950.0,2000.0,2050.0,2100.0,2150.0,2200.0,2250.0, 028180
52300.0,2350.0,2400.0,2450.0,2500.0,2550.0,2575.0,2625.0,2675.0, 028190
62725.0,2775.0,2825.0,2875.0,2925.0,2975.0,3025.0,3075.0,3125.0, 028200
73175.0,3225.0,3275.0,3325.0,3375.0,3425.0,3475.0,3525.0,3575.0, 028210
83625.0,3675.0,3725.0,3775.0,3825.0,3875.0,3925.0,3975.0,4025.0, 028220
94100.0,4200.0,4300.0,4400.0,4500.0,4600.0,4700.0,4800.0,4900.0, 028230
A5000.0,5100.0,5200.0,5300.0,5400.0,5500.0,5600.0,5700.0,5800.0, 028240
85900.0,6000.0,6200.0,6400.0,6600.0,6800.0,7000.0,7200.0,7300.0/ 028250
C 028260
DATA FL/2.2000E+08,3.9000E+08,6.1000E+08,9.0000E+08,4.4000E+09, 028270
25.5000E+08,4.0000E+07,3.5000E+03,3.9100E+09,4.6800E+09,4.4000E+09, 028280
39.3000E+09,5.5000E+09,1.1700E+10,2.7000E+11,2.6000E+10,1.1900E+10, 028290
41.7700E+10,1.9300E+10,3.7000E+10,7.3000E+10,1.3300E+11,2.1600E+11, 028300
52.0600E+11,2.5800E+11,4.3000E+11,9.1000E+11,1.3100E+12,2.2500E+12, 028310
63.9000E+12,5.9000E+12,8.7000E+12,1.4400E+13,2.3800E+13,3.1600E+13, 028320
73.8300E+13,3.8300E+13,3.5400E+13,3.6800E+13,4.6300E+13,4.5000E+13, 028330
87.1600E+13,4.0800E+13,1.1200E+14,1.5100E+14,1.6200E+14,1.16100E+14, 028340
92.0600E+14,3.1100E+14,4.2400E+14,4.6400E+14,4.8700E+14,5.5400E+14, 028350
A6.2200E+14,6.5200E+14,6.9500E+14,9.3300E+14,9.5900E+14,9.3300E+14, 028360
89.9000E+14,9.3100E+14,1.1000E+15,1.0200E+15,1.1100E+15,1.13100E+15, 028370
C1.1700E+15,1.3300E+15,1.1400E+15,1.1600E+15,1.1600E+15,1.12700E+15, 028380
D1.3800E+15,2.9900E+15,4.0100E+15,3.9500E+15,4.2300E+15,4.18700E+15, 028390
E4.9700E+15,5.0500E+15,5.2000E+15,4.9000E+15,5.0100E+15,4.9900E+15, 028400
F4.8600E+15,5.1000E+15,5.3100E+15,5.3800E+15,5.3200E+15,5.3400E+15, 028410
G5.4000E+15,5.4200E+15,5.4400E+15,1.0800E+16,1.0700E+16,1.11900E+16, 028420
H1.0300E+16,1.0100E+16,9.9300E+15,4.9000E+15/ 028430
C 028440

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DATA Q02/5.2000E-18,5.9000E-18,5.5000E-18,4.0000E-17,2.0000E-18, 028450
21.9000E-18,1.9000E-18,1.6000E-18,1.2000E-18,1.0000E-18,1.0000E-19,028460
34.0000E-19,3.6000E-19,4.6000E-18,1.0000E-20,1.0000E-18,5.5000E-19,028470
44.0000E-18,1.0000E-17,1.0000E-17,1.0000E-17,8.4000E-18,4.3000E-18,028480
54.3000E-18,8.8000E-19,2.7000E-19,6.0000E-21,5.5000E-22,1.0000E-21,028490
62.0000E-23,1.3000E-23,1.0000E-23,8.5000E-24,6.5000E-24,5.0000E-24,028500
74.0000E-24,3.0000E-24,1.6000E-24,1.0000E-24,7.0000E-25,3.0000E-25,028510
81.2000E-25,30*8./ 028520
C - - - - - 028530
DATA Q03/24*8.,8.3500E-19,8.3500E-19,7.4190E-19,6.6670E-19, 028540
24.7000E-19,4.0740E-19,2.9630E-19,3.3330E-19,5.9260E-19,1.0500E-18,028550
31.8600E-18,2.9000E-18,4.4000E-18,6.2000E-18,8.1000E-18,9.9000E-18,028560
41.1000E-17,1.1300E-17,1.1000E-17,1.0000E-17,8.6000E-18,6.4000E-18,028570
54.3000E-18,2.7000E-18,1.6000E-18,1.0000E-18,4.7000E-19,2.6000E-19,028580
61.4000E-19,6.9000E-20,3.6000E-20,1.8000E-20,7.7000E-21,4.1000E-21,028590
72.0000E-21,6.9000E-22,4.0000E-22,2.5000E-22,10*0.00000,2.9000E-23,028600
84.0000E-23,6.8000E-23,1.2500E-22,1.7100E-22,3.5700E-22,4.0600E-22,028610
97.1000E-22,3.3000E-22,1.2000E-21,1.6000E-21,1.8000E-21,2.5000E-21,028620
A2.3000E-21,3.2000E-21,3.9000E-21,4.7000E-21,4.6000E-21,4.6000E-21,028630
84.9000E-21,3.9000E-21,2.7000E-21,2.1000E-21,1.4000E-21,9.1000E-22,028640
C6.4000E-22,5.1000E-22/ 028650
C - - - - - 028660
DATA TEMP/3.0458E+02,2.8956E+02,2.7787E+02,2.6652E+02,2.5241E+02, 028670
22.3839E+02,2.2442E+02,2.1050E+02,2.0315E+02,2.0738E+02,2.1175E+02,028680
32.1594E+02,2.1920E+02,2.2384E+02,2.2783E+02,2.3179E+02,2.3574E+02,028690
42.4040E+02,2.4514E+02,2.4988E+02,2.5462E+02,2.5935E+02,2.6408E+02,028700
52.6880E+02,2.7215E+02,2.7215E+02,2.7114E+02,2.6721E+02,2.6328E+02,028710
62.5936E+02,2.5479E+02,2.4735E+02,2.3991E+02,2.3247E+02,2.2504E+02,028720
72.1761E+02,2.1019E+02,2.0277E+02,1.9536E+02,1.8795E+02,1.8054E+02,028730
C - - - - - 028740
DATA DM/2.4110E+19,2.1050E+19,1.6510E+19,1.3400E+19,1.0880E+19, 028750
28.7330E+18,6.9130E+18,5.9310E+18,4.1030E+18,2.8240E+18,2.0000E+18,028760
31.4290E+18,1.0320E+18,7.4450E+17,5.4230E+17,3.9700E+17,2.9240E+17,028770
42.1590E+17,1.6040E+17,1.1980E+17,8.9990E+16,6.7980E+16,5.1610E+16,028780
53.9390E+16,3.0350E+16,2.3720E+16,1.8600E+16,1.4710E+16,1.1590E+16,028790
69.1050E+15,7.1440E+15,5.6360E+15,4.4160E+15,3.4350E+15,2.6620E+15,028800
72.0260E+15,1.5350E+15,1.1520E+15,8.5540E+14,6.2810E+14,4.5560E+14,028810
C - - - - - 028820
DATA O3/6.2500E+11,6.1300E+11,5.3100E+11,4.7800E+11,4.4900E+11, 028830
24.1800E+11,5.2500E+11,6.5200E+11,2.6700E+12,3.7400E+12,4.4700E+12,028840
34.8000E+12,4.8700E+12,4.4700E+12,3.9100E+12,3.2500E+12,2.5700E+12,028850
41.3200E+12,1.3800E+12,9.6600E+11,6.6200E+11,4.4300E+11,2.8900E+11,028860
51.9100E+11,1.1400E+11,7.4600E+10,4.9300E+10,3.4000E+10,2.3200E+10,028870
61.5700E+10,1.0600E+10,7.5400E+09,5.2900E+09,3.5200E+09,2.2600E+09,028880
71.3700E+09,3.5600E+08,5.0700E+08,3.1700E+08,2.0300E+08,1.3200E+08,028890
C - - - - - 028900
DATA OH/1.6100E+06,1.2400E+06,1.0600E+06,1.0100E+06,7.3200E+05, 028910
24.3600E+05,3.4100E+05,1.9400E+05,2.0000E+05,2.7000E+05,3.4400E+05,028920
34.3300E+05,5.5400E+05,7.1200E+05,9.3200E+05,1.2600E+06,1.7300E+06,028930
42.4300E+06,3.3800E+06,4.5900E+06,5.9800E+06,7.2600E+06,8.0000E+06,028940
57.3600E+06,7.4000E+06,6.7300E+06,6.0100E+06,5.3800E+06,4.7600E+06,028950
64.1800E+06,3.6700E+06,3.1600E+06,2.6700E+06,2.3400E+06,2.1000E+06,028960
71.3200E+06,1.7000E+06,1.5500E+05,1.2800E+06,9.8900E+05,7.10500E+05,028970
C - - - - - 028980
DATA O/2.8300E+03,2.8900E+03,3.4800E+03,3.6300E+03,4.6100E+03, 028990
25.9800E+03,1.0400E+04,1.5000E+04,1.1500E+05,3.6400E+05,9.2900E+05,029000
32.1100E+06,4.4200E+06,8.6700E+06,1.6000E+07,2.8400E+07,4.18600E+07,029010
43.1700E+07,1.3500E+08,2.2100E+08,3.6500E+08,6.0800E+08,9.0300E+08,029020
51.4700E+09,2.0000E+09,2.5500E+09,3.1200E+09,3.6900E+09,4.2500E+09,029030
64.8100E+09,5.3300E+09,5.9200E+09,6.5100E+09,6.8300E+09,6.9100E+09,029040
76.8300E+09,6.9400E+09,6.8400E+09,7.2800E+09,8.0900E+09,9.4000E+09,029050
C - - - - - 029060
DATA H/1.2100E-01,8.8000E-02,8.1500E-02,8.0000E-02,5.9100E-02, 029070
24.1500E-02,2.8700E-02,1.5400E-02,1.4000E-02,2.1000E-02,3.2700E-02,029080
35.7700E-02,1.1500E-01,2.5800E-01,6.2700E-01,1.6800E+00,5.10300E+00,029090
41.7000E+01,5.1100E+01,2.2700E+02,8.3300E+02,2.9000E+03,8.19000E+03,029100

52.2700E+04,4.8500E+04,9.0900E+04,1.5800E+05,2.5800E+05,4.0900E+05,029110
66.3200E+05,9.5800E+05,1.3800E+06,1.9500E+06,2.7800E+06,3.9900E+06,029120
75.9900E+06,8.6900E+06,1.3100E+07,1.9200E+07,2.7500E+07,3.8100E+07/029130
- - - - - 029140
DATA H02/2.4200E+08,1.7600E+08,1.3100E+08,1.2500E+08,8.1500E+07,029150
25.0400E+07,3.1500E+07,1.8100E+07,1.5800E+07,1.7900E+07,2.0400E+07,029160
32.2900E+07,2.5400E+07,2.6700E+07,2.7000E+07,2.5800E+07,2.1300E+07,029170
41.9200E+07,1.5100E+07,1.1700E+07,9.2300E+06,7.6900E+06,6.1720E+06,029180
55.3200E+06,5.1800E+06,4.5500E+06,3.9600E+06,3.4600E+06,3.0800E+06,029190
62.5900E+06,2.2300E+06,1.8700E+06,1.5400E+06,1.3300E+06,1.1900E+06,029200
71.0800E+06,3.5200E+05,8.6700E+05,7.0500E+05,5.2500E+05,3.15500E+05/029210
- - - - - 029220
DATA H202/2.1000E+10,2.5000E+10,1.8000E+10,1.2000E+10,1.13000E+10,029230
25.3000E+09,4.5000E+09,1.4000E+09,9.9400E+07,2.4100E+07,3.9400E+07,029240
34.4200E+07,4.1500E+07,3.5500E+07,3.0100E+07,2.4800E+07,2.12700E+07,029250
42.0800E+07,1.8600E+07,1.6100E+07,1.3300E+07,1.0700E+07,8.4500E+06,029260
56.3800E+06,4.5800E+06,3.2000E+06,2.2400E+06,1.6000E+06,1.1300E+06,029270
67.9800E+05,5.7400E+05,3.8600E+05,2.4600E+05,1.7100E+05,1.2300E+05,029280
79.5900E+04,7.2300E+04,5.9300E+04,3.8300E+04,2.0500E+04,9.10200E+03/029290
- - - - - 029300
DATA JHCL/1.3476E-29,1.7155E-26,1.0596E-23,3.5073E-21,6.9259E-19,029310
26.7111E-17,3.1183E-15,8.7227E-14,1.5159E-12,1.4303E-11,8.4891E-11,029320
33.6315E-10,1.2327E-09,3.4042E-09,7.9316E-09,1.5998E-08,2.18437E-08,029330
44.5049E-08,6.4398E-08,8.4481E-08,1.0523E-07,1.2410E-07,1.4043E-07,029340
51.5440E-07,1.6726E-07,1.7994E-07,1.9339E-07,2.0849E-07,2.2585E-07,029350
62.4560E-07,2.6740E-07,2.9069E-07,3.1487E-07,3.4177E-07,3.6896E-07,029360
74.0039E-07,4.3648E-07,4.7911E-07,5.2843E-07,5.8180E-07,6.3504E-07/029370
- - - - - 029380
DATA JCH4/25*0.,1.0289E-27,3.2369E-23,1.1507E-19,7.5248E-17,029390
21.2647E-14,7.2754E-13,1.8015E-11,2.3133E-10,1.7445E-09,8.5503E-09,029400
33.0106E-08,7.3105E-08,1.6859E-07,3.0472E-07,4.8102E-07,6.17959E-07/029410
- - - - - 029420
DATA DID/2.9228E-03,3.3919E-03,3.8611E-03,4.3988E-03,5.1697E-03,029430
26.1919E-03,1.0078E-02,1.5063E-02,9.7719E-02,2.3901E-01,5.1692E-01,029440
31.0496E+00,2.0826E+00,3.8613E+00,6.8855E+00,1.1820E+01,1.19289E+01,029450
42.9819E+01,4.3466E+01,6.1222E+01,8.4508E+01,1.1458E+02,1.4672E+02,029460
51.6955E+02,1.7919E+02,1.8142E+02,1.7690E+02,1.7115E+02,1.16057E+02,029470
61.4725E+02,1.3288E+02,1.2417E+02,1.1422E+02,9.9626E+01,8.3651E+01,029480
76.7259E+01,5.5916E+01,4.4580E+01,3.8082E+01,3.3875E+01,3.11108E+01/029490
- - - - - 029500
DATA JN20/3.3115E-10,3.3776E-10,3.4402E-10,3.4968E-10,3.5496E-10,029510
23.5999E-10,3.6561E-10,3.7298E-10,3.9724E-10,4.6762E-10,6.6381E-10,029520
31.2383E-09,2.9256E-09,6.5720E-09,1.4198E-08,2.7762E-08,4.18867E-08,029530
47.7590E-08,1.1187E-07,1.4846E-07,1.8706E-07,2.2282E-07,2.5396E-07,029540
52.8033E-07,3.0302E-07,3.2303E-07,3.4130E-07,3.5868E-07,3.17595E-07,029550
63.9349E-07,4.1144E-07,4.2975E-07,4.4813E-07,4.6727E-07,4.8608E-07,029560
75.0774E-07,5.3259E-07,5.6308E-07,6.0045E-07,6.4319E-07,6.8785E-07/029570
- - - - - 029580
DATA JN205/1.2807E-05,1.2864E-05,1.2918E-05,1.2965E-05,1.3010E-05,029590
21.3052E-05,1.3098E-05,1.3157E-05,1.3330E-05,1.3694E-05,1.4245E-05,029600
31.5057E-05,1.6326E-05,1.8306E-05,2.1404E-05,2.6320E-05,3.13719E-05,029610
44.4228E-05,5.7854E-05,7.4327E-05,9.3804E-05,1.1526E-04,1.13777E-04,029620
51.5999E-04,1.8017E-04,1.9764E-04,2.1265E-04,2.2476E-04,2.3475E-04,029630
62.4284E-04,2.4919E-04,2.5410E-04,2.5789E-04,2.6070E-04,2.6267E-04,029640
72.6400E-04,2.6488E-04,2.6546E-04,2.6584E-04,2.6610E-04,2.6627E-04/029650
- - - - - 029660
DATA JMN03/1.7653E-07,1.7967E-07,1.8265E-07,1.8533E-07,1.8783E-07,029670
21.9022E-07,1.9287E-07,1.9629E-07,2.0680E-07,2.3252E-07,2.8660E-07,029680
34.1257E-07,7.1813E-07,1.3894E-06,2.7000E-06,4.9742E-06,8.4498E-06,029690
41.3130E-05,1.8690E-05,2.4671E-05,3.1130E-05,3.7342E-05,4.3095E-05,029700
54.9260E-05,5.2789E-05,5.6697E-05,6.0084E-05,6.2996E-05,6.5600E-05,029710
66.7984E-05,7.0208E-05,7.2324E-05,7.4349E-05,7.6237E-05,7.7946E-05,029720
77.9638E-05,8.1042E-05,8.2214E-05,8.3244E-05,8.4143E-05,8.4903E-05/029730
- - - - - 029740
DATA JN202/1.3571E-06,1.3663E-06,1.3750E-06,1.3828E-06,1.3900E-06,029750
21.3968E-06,1.4044E-06,1.4140E-06,1.4241E-06,1.4317E-06,1.4316E-06,029760

31.7219E-06,1.3206E-06,2.2204E-06,2.6755E-06,3.3861E-06,4.4527E-06,029770
 46.0019E-06,1.1055E-06,1.0840E-05,1.4314E-05,1.8545E-05,2.3397E-05,029780
 52.3488E-05,3.3262E-05,3.7486E-05,4.1182E-05,4.4205E-05,4.6749E-05,029790
 64.3867E-05,5.0575E-05,5.1938E-05,5.3028E-05,5.3880E-05,5.4513E-05,029800
 75.4992E-05,5.5353E-05,5.5639E-05,5.5874E-05,5.6073E-05,5.6238E-05,029810
 - - - - - 029820
 DATA HNO3/4.74E+10,2.13E+10,1.09E+10,1.58E+10,1.22E+10,8.84E+09,029830
 26.56E+09,4.63E+09,8.86E+09,1.03E+10,9.90E+09,8.16E+09,5.73E+09,029840
 33.31E+09,1.75E+09,9.13E+08,4.84E+08,2.55E+08,1.33E+08,6.72E+07,029850
 43.07E+07,1.18E+07,3.67E+06,9.55E+05,2.35E+05,6.09E+04,1.60E+04,029860
 54.52E+03,1.26E+03,3.30E+02,8.95E+01,2.48E+01,6.86E+00,2.06E+00,029870
 66.94E-01,7.66E-01,3.00E-01,1.37E-01,6.29E-02,2.99E-02,1.39E-02,029880
 - - - - - 029890
 DATA NOX/2.99E-09,1.76E-09,1.33E-09,1.35E-09,1.36E-09,1.33E-09,029900
 21.48E-09,1.60E-09,3.41E-09,5.45E-09,7.69E-09,1.00E-08,1.23E-08,029910
 31.44E-08,1.62E-08,1.77E-08,1.87E-08,1.92E-08,1.93E-08,1.90E-08,029920
 41.35E-08,1.77E-08,1.67E-08,1.55E-08,1.42E-08,1.29E-08,1.15E-08,029930
 53.98E-09,8.50E-09,7.10E-09,5.83E-09,4.75E-09,3.39E-09,3.26E-09,029940
 62.85E-09,7.91E-09,7.64E-09,7.84E-09,8.58E-09,1.02E-08,1.28E-08,029950
 - - - - - 029960
 DATA N2O/2.6E-07,2.6E-07,2.6E-07,2.6E-07,2.6E-07,2.6E-07,2.6E-07,029970
 22.6E-07,2.57E-07,2.27E-07,1.87E-07,1.52E-07,1.29E-07,1.09E-07,029980
 39.20E-08,7.63E-08,6.23E-08,5.03E-08,4.03E-08,3.21E-08,2.56E-08,029990
 42.06E-08,1.66E-08,1.36E-08,1.12E-08,9.35E-09,7.89E-09,6.73E-09,030000
 55.80E-09,5.06E-09,4.46E-09,3.98E-09,3.58E-09,3.26E-09,3.01E-09,030010
 62.80E-09,2.64E-09,2.51E-09,2.42E-09,2.33E-09,2.3E-09,030020
 - - - - - 030030
 DATA CH4/1.50E-06,1.49E-06,1.43E-06,1.48E-06,1.48E-06,1.47E-06,030040
 21.47E-06,1.47E-06,1.40E-06,1.33E-06,1.25E-06,1.16E-06,1.06E-06,030050
 39.68E-07,8.68E-07,7.69E-07,6.71E-07,5.79E-07,4.93E-07,4.17E-07,030060
 43.52E-07,2.98E-07,2.55E-07,2.23E-07,2.00E-07,1.83E-07,1.71E-07,030070
 51.62E-07,1.56E-07,1.51E-07,1.47E-07,1.45E-07,1.43E-07,1.41E-07,030080
 61.40E-07,6*0./ 030090
 - - - - - 030100
 DATA CO/9.37E-08,9.53E-08,9.05E-08,8.60E-08,8.24E-08,7.98E-08,030110
 27.42E-08,7.08E-08,4.60E-08,3.15E-08,2.39E-08,2.07E-08,2.02E-08,030120
 32.14E-08,2.34E-08,2.56E-08,2.72E-08,2.80E-08,2.77E-08,2.68E-08,030130
 42.37E-08,2.51E-08,2.54E-08,2.66E-08,2.90E-08,3.25E-08,3.75E-08,030140
 54.41E-08,5.21E-08,6.14E-08,7.13E-08,8.11E-08,8.98E-08,9.63E-08,030150
 69.33E-08,5.74E-07,1.10E-06,1.99E-06,3.59E-06,6.45E-06,1.17E-05,030160
 - - - - - 030170
 DATA NO/6.61E+09,5.03E+09,4.40E+09,1.07E+09,1.48E+09,2.13E+09,030180
 22.50E+09,3.46E+09,2.20E+09,1.60E+09,1.34E+09,1.26E+09,1.29E+09,030190
 31.34E+09,1.35E+09,1.33E+09,1.28E+09,1.22E+09,1.15E+09,1.07E+09,030200
 49.76E+08,8.58E+08,7.10E+08,5.51E+08,4.09E+08,2.97E+08,2.10E+08,030210
 51.45E+08,9.30E+07,6.44E+07,4.16E+07,2.68E+07,1.72E+07,1.12E+07,030220
 67.59E+06,1.60E+07,1.17E+07,9.03E+06,7.34E+06,6.41E+06,5.83E+06,030230
 - - - - - 030240
 DATA NO2/1.81E+10,1.07E+10,6.70E+09,1.20E+09,1.16E+09,1.15E+09,030250
 21.19E+09,1.39E+09,2.86E+09,3.32E+09,3.78E+09,4.29E+09,4.85E+09,030260
 35.16E+09,4.97E+09,4.34E+09,3.49E+09,2.59E+09,1.79E+09,1.14E+09,030270
 46.53E+08,3.30E+08,1.46E+08,5.83E+07,2.30E+07,9.03E+06,3.52E+06,030280
 51.37E+06,5.22E+05,1.96E+05,7.29E+04,2.71E+04,1.02E+04,3.98E+03,030290
 61.59E+03,2.36E+03,1.22E+03,7.09E+02,4.66E+02,3.46E+02,2.79E+02,030300
 - - - - - 030310
 DATA H2/5.0000E-07,5.0000E-07,5.0000E-07,5.0000E-07,5.0000E-07,5.0000E-07,030320
 25.0000E-07,5.0000E-07,5.0000E-07,5.0000E-07,5.0000E-07,5.0000E-07,030330
 35.0000E-07,5.0000E-07,5.0000E-07,5.0000E-07,5.0000E-07,5.0000E-07,030340
 45.0000E-07,5.0000E-07,5.0000E-07,5.0000E-07,5.0000E-07,5.0000E-07,030350
 55.0000E-07,5.0000E-07,5.0000E-07,5.0000E-07,5.0000E-07,5.0000E-07,030360
 65.0000E-07,5.0000E-07,1.0000E-06,1.6000E-06,2.2000E-06,2.9000E-06,030370
 73.3000E-06,4.4000E-06,4.5000E-06,4.3000E-06,4.2000E-06,4.1000E-06,030380
 - - - - - 030390
 DATA JNO2/4.3974E-03,4.3992E-03,4.4009E-03,4.4024E-03,4.4038E-03,030400
 24.4051E-03,4.4065E-03,4.4083E-03,4.4134E-03,4.4238E-03,4.4381E-03,030410
 34.4558E-03,4.4775E-03,4.5019E-03,4.5277E-03,4.5553E-03,4.5829E-03,030420

44.5104E-03,4.6360E-03,4.6598E-03,4.6810E-03,4.6999E-03,4.7159E-03,030430
 54.7291E-03,4.7394E-03,4.7474E-03,4.7536E-03,4.7583E-03,4.7619E-03,030440
 64.7646E-03,4.7667E-03,4.7687E-03,4.7702E-03,4.7710E-03,4.7720E-03,030450
 74.7723E-03,4.7728E-03,4.7733E-03,4.7733E-03,4.7737E-03,4.7737E-03/030460

DATA JCF2/4.0383E-29,6.7920E-26,4.6511E-23,1.6649E-20,3.4437E-18,030470
 23.3930E-16,1.5605E-14,4.1950E-13,6.8864E-12,6.2006E-11,3.5744E-10,030490

31.5095E-09,5.1218E-09,1.4246E-08,3.3557E-08,6.0392E-08,1.1226E-07,030500
 41.9576E-07,2.8127E-07,3.7010E-07,4.6109E-07,5.4441E-07,6.1635E-07,030510
 56.7728E-07,7.3306E-07,7.6765E-07,8.4524E-07,9.0972E-07,9.8409E-07,030520
 61.0693E-06,1.1642E-06,1.2662E-06,1.3715E-06,1.4831E-06,1.5852E-06,030530
 71.6855E-06,1.7735E-06,1.8506E-06,1.9193E-06,1.9193E-06,2.0290E-06/030540

DATA JCF3/2.4654E-27,3.0229E-24,1.5298E-21,3.4449E-19,5.0888E-17,030560

24.3030E-15,1.8292E-13,4.6028E-12,7.0755E-11,6.0305E-10,3.3214E-09,030570
 31.3478E-08,4.4144E-08,1.1916E-07,2.7409E-07,5.5114E-07,9.8385E-07,030580
 41.5742E-06,2.2816E-06,3.0398E-06,3.8463E-06,4.5932E-06,5.2451E-06,030590
 55.7977E-06,6.2725E-06,6.6895E-06,7.0691E-06,7.4289E-06,7.7937E-06,030600
 68.1405E-06,8.5016E-06,8.8656E-06,9.2254E-06,9.5906E-06,9.9197E-06,030610
 71.0238E-05,1.0514E-05,1.0752E-05,1.0962E-05,1.1145E-05,1.1297E-05/030620

DATA H20/2.2717E-02,1.1092E-02,6.7620E-03,3.5403E-03,1.2747E-03,030640

24.0172E-04,1.0814E-04,2.1832E-05,4.2000E-06,4.2000E-06,4.2000E-06,030650
 34.2000E-06,4.2000E-06,4.2000E-06,4.2000E-06,4.2000E-06,4.2000E-06,030660
 44.2000E-06,4.2000E-06,4.2000E-06,4.2000E-06,4.2000E-06,4.2000E-06,030670
 54.2000E-06,4.2000E-06,4.2000E-06,4.2000E-06,4.2000E-06,4.2000E-06,030680
 64.2000E-06,4.2000E-06,3.6000E-05,2.9000E-06,2.6000E-06,2.3000E-06,030690
 71.3000E-06,1.3000E-06,1.0000E-06,6.7000E-07,4.4000E-07,2.9000E-07/030700

DATA JH20/8.1806E-67,6.1806E-67,2.2712E-31,3.1934E-27,7.6346E-24,030720

24.2150E-21,6.6966E-19,4.4976E-17,1.3713E-15,1.8280E-14,1.4238E-13,030730
 37.8392E-13,3.3426E-12,1.1276E-11,3.0938E-11,7.0234E-11,1.13649E-10,030740
 42.3139E-10,3.4800E-10,4.7399E-10,5.9999E-10,7.3020E-10,8.7195E-10,030750
 51.0725E-09,1.4382E-09,2.0754E-09,3.0979E-09,4.5909E-09,6.5824E-09,030760
 69.0177E-09,1.1798E-08,1.4922E-08,1.8869E-08,2.6066E-08,4.1000E-08,030770
 77.4037E-08,1.3761E-07,2.4305E-07,3.8386E-07,5.8130E-07,7.8685E-07/030780

DATA JO3/2.3315E-05,2.9694E-05,3.0051E-05,3.0373E-05,3.0674E-05,030800

23.0960E-05,3.1279E-05,3.1686E-05,3.2891E-05,3.5506E-05,3.9544E-05,030810
 34.5423E-05,5.4081E-05,6.6396E-05,8.3774E-05,1.0940E-04,1.4673E-04,030820
 42.0226E-04,2.8193E-04,3.9934E-04,5.7774E-04,8.5549E-04,1.2515E-03,030830
 51.7333E-03,2.2239E-03,2.6768E-03,3.0877E-03,3.4194E-03,3.6993E-03,030840
 63.3344E-03,4.1230E-03,4.2709E-03,4.3859E-03,4.4786E-03,4.5289E-03,030850
 74.5668E-03,4.5906E-03,4.6055E-03,4.6146E-03,4.6204E-03,4.6242E-03/030860

DATA JO2/2.8970E-31,3.1074E-28,1.4126E-25,2.5237E-23,2.6991E-21,030880

21.7903E-19,6.5744E-18,1.4959E-15,2.1357E-15,1.7354E-14,9.2769E-14,030890
 33.7073E-13,1.2105E-12,3.3061E-12,7.7843E-12,1.6251E-11,3.0572E-11,030900
 45.2363E-11,8.2376E-11,1.2038E-10,1.6697E-10,2.1867E-10,2.7155E-10,030910
 53.2242E-10,3.6953E-10,4.1477E-10,4.6269E-10,5.1803E-10,5.46584E-10,030920
 66.6887E-10,7.6743E-10,8.8054E-10,1.0076E-09,1.1568E-09,1.3310E-09,030930
 71.5628E-09,1.8491E-09,2.1997E-09,2.6087E-09,3.0475E-09,3.4791E-09/030940

DATA QCF2/ 27°0.,9.12E-19,5.70E-19,2.46E-19,9.02E-20,3.11E-20,030960

1 9.76E-21,2.00E-21,38°0./ 030970

DATA QCF3/ 27°0.,2.41E-18,1.80E-18,1.13E-18,6.56E-19,3.49E-19,030980

1 1.52E-19,6.40E-20,2.47E-20,1.00E-20,36°0./ 030990

DATA QCCL4 /27°0.,3.36E-18,1.36E-18,7.33E-19,6.92E-19,6.25E-19,031000

1 4.54E-19,3.01E-19,1.75E-19,7.00E-20,36°0./ 031010

DATA QCM3C/25°0.,5.5E-19,3.55E-19,1.80E-19,7.68E-20,3.02E-20,031020

2 9.83E-21,3.42E-21,9.10E-22,2.30E-22,5.00E-23,37°0./ 031030

DATA QCLN3/28°0.,8.0E-18,5.3E-18,3.5E-18,3.4E-18,3.3E-18,031040

2,3.2E-18,3.2E-18,2.3E-18,1.6E-18,1.2E-18,8.4E-19,6.3E-19,4.7E-19,031050

3 4.2E-19,3.8E-19,2.6E-19,2.2E-19,1.6E-19,1.3E-19,8.5E-20,6.3E-20,031060

4 3.8E-20,3.0E-20,2.3E-20,1.6E-20,1.2E-20,8.3E-21,6.4E-21,4.6E-21,031070

5 3.1E-21,2.6E-21,2.2E-21,1.7E-21,1.1E-21,7.1E-22,8°0./ 031080

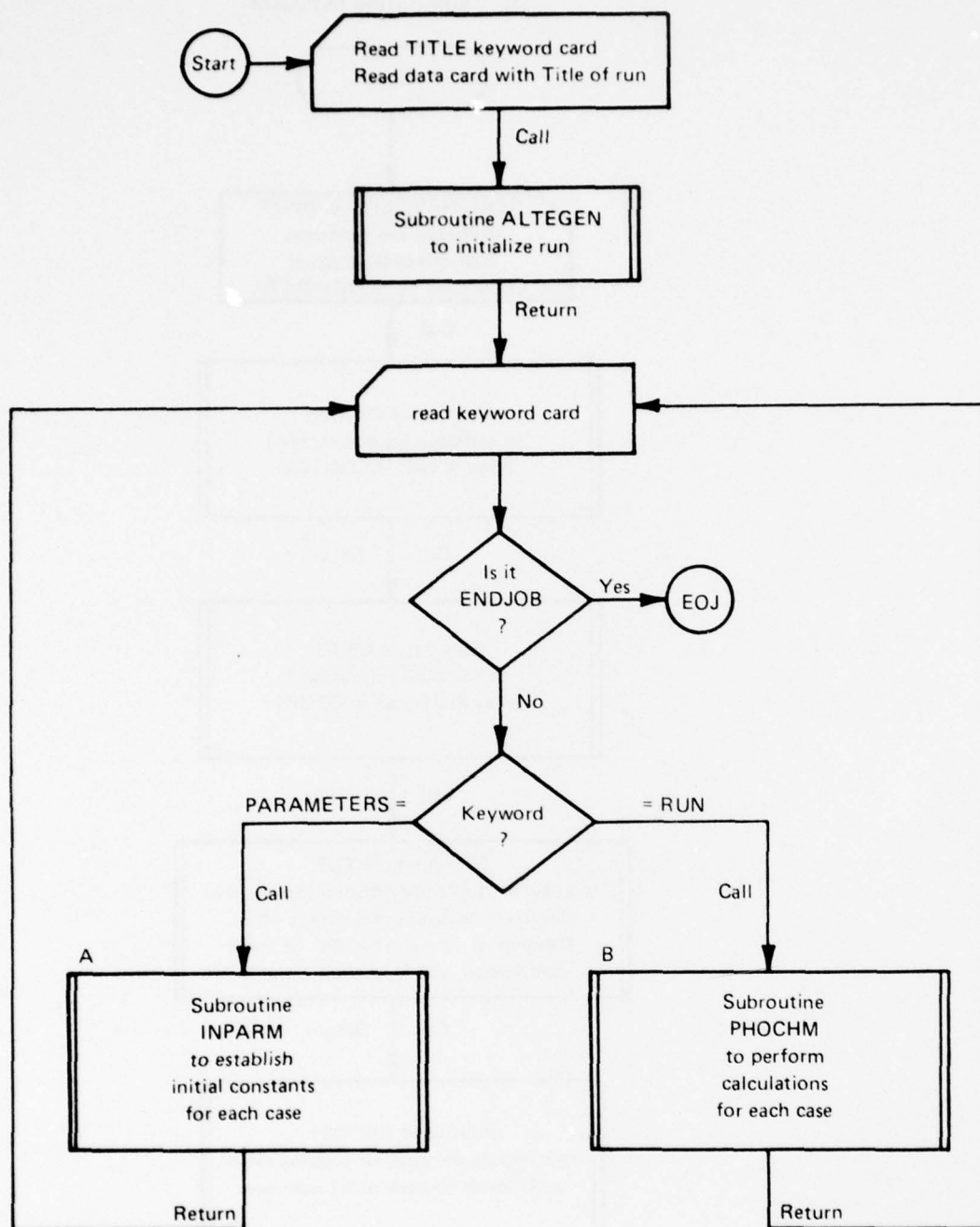
DATA QM20/ 8*0., 3.7E-17, 3.7E-17, 3.7E-17, 1.5E-17, 3.7E-18, 2.6E-18,	031090
2 2.6E-18, 1.7E-17, 8.9E-17, 3.7E-17, 5.0E-19, 4.0E-18, 1.0E-18, 1.0E-19,	031100
3 3.0E-20, 4.0E-20, 7.0E-20, 9.0E-20, 1.1E-19, 1.1E-19, 1.0E-19, 6.0E-20,	031110
4 3.3E-20, 1.5E-20, 6.0E-21, 2.5E-21, 1.1E-21, 3.0E-22, 1.0E-22, 3.2E-23,	031120
5 1.5E-23, 7.6E-24, 5.0E-24, 2.0E-24, 6.8E-25, 4.0E-25, 28*0./	031130
DATA QMNO3/28*0., 1.32E-17, 9.10E-18, 5.5E-18, 2.55E-18, 9.7E-19,	031140
2 3.28E-19, 1.44E-19, 8.51E-20, 5.63E-20, 3.74E-20, 2.60E-20, 2.10E-20,	031150
3 1.95E-20, 1.94E-20, 1.90E-20, 1.80E-20, 1.63E-20, 1.40E-20, 1.14E-20,	031160
4 8.77E-21, 6.34E-21, 4.26E-21, 2.75E-21, 1.68E-21, 9.50E-22, 4.70E-22,	031170
5 1.80E-22, 1.00E-22, 1.00E-23, 1.00E-24, 1.00E-24, 13*0./	031180
DATA QM202/26*0., 1.5E-18, 1.2E-18, 7.5E-19, 6.2E-19, 4.9E-19, 4.3E-19,	031190
2 3.8E-19, 3.4E-19, 3.0E-19, 2.4E-19, 1.9E-19, 1.5E-19, 1.3E-19, 1.1E-19,	031200
3 8.4E-20, 6.5E-20, 5.3E-20, 3.8E-20, 3.0E-20, 2.3E-20, 1.9E-20, 1.4E-20,	031210
4 1.1E-20, 8.1E-21, 5.8E-21, 3.4E-21, 2.7E-21, 1.9E-21, 1.3E-21, 6.5E-22,	031220
5 5.1E-22, 3.5E-22, 2.5E-22, 1.3E-22, 1.0E-22, 7.3E-23, 5.4E-23, 3.4E-23,	031230
6 2.5E-23, 1.6E-23, 1.1E-23, 6.9E-24, 1.1E-24, 8.0E-25, 0., 0./	031240
DATA QM205/ 32*0., 4.7E-18, 3.2E-18, 2.0E-18, 1.3E-18, 9.6E-19, 7.8E-19,	031250
26.0E-19, 4.8E-19, 3.7E-19, 3.1E-19, 2.5E-19, 2.1E-19, 1.7E-19, 1.3E-19,	031260
38.9E-20, 5.1E-20, 4.2E-20, 3.3E-20, 2.5E-20, 1.9E-20, 1.3E-20, 1.03E-20,	031270
47.5E-21, 5.8E-21, 4.0E-21, 3.4E-21, 2.7E-21, 2.3E-21, 1.8E-21, 1.4E-21,	031280
51.0E-21, 7.4E-22, 4.7E-22, 3.0E-22, 1.3E-22, 5*0./	031290
DATA QMCL/19*0., 2.11E-18, 2.81E-18, 3.45E-18, 3.82E-18, 3.32E-18,	031300
12.48E-18, 1.63E-18, 1.09E-18, 5.88E-19, 3.13E-18, 1.45E-18, 6.18E-20,	031310
27.56E-20, 9.83E-21, 3.95E-21, 1.37E-21, 4.80E-22, 37*0./	031320
DATA QMOCL/49*0., 6.3E-20, 7.9E-20, 9.5E-20, 1.05E-19, 1.15E-19,	031330
11.25E-19, 1.35E-19, 1.27E-19, 1.19E-19, 1.07E-19, 9.5E-20, 8.8E-20,	031340
27.90E-20, 6.35E-20, 4.80E-20, 3.80E-20, 2.90E-20, 2.6E-20, 2.4E-20,	031350
32.00E-20, 1.60E-20, 1.20E-20, 4.80E-20/	031360
DATA QM208/8*0., 5.0E-18, 4.0E-18, 3.0E-18, 4.0E-18, 5.0E-18, 4.0E-18,	031370
11.4E-17, 6.0E-18, 7.0E-18, 3.2E-18, 7.0E-19, 5.0E-19, 1.0E-18, 2.2E-18,	031380
23.5E-18, 4.8E-18, 4.3E-18, 2.8E-18, 7.5E-19, 5.0E-20, 5.2E-21, 6.3E-22,	031390
36.3E-23, 41*0./	031400
DATA QM02/49*0., 6.77E-20, 8.52E-20, 1.09E-19, 1.67E-19,	031410
11.83E-19, 2.19E-19, 2.35E-19, 2.54E-19, 2.91E-19, 3.14E-19,	031420
23.23E-19, 3.43E-19, 3.11E-19, 4.37E-19, 3.90E-19, 5.37E-19,	031430
34.97E-19, 5.00E-19, 5.93E-19, 5.79E-19, 5.49E-19, 5.62E-19,	031440
46.56E-19, 8.66E-19/	031450
DATA CLX/1.1E-9, 5.7E-10, 3.1E-10, 1.7E-10, 1.2E-10, 8.4E-11, 1.1E-10,	031460
11.3E-10, 2.4E-10, 6.0E-10, 9.5E-10, 1.3E-9, 1.6E-9, 1.8E-9, 2.0E-9,	031470
22.2E-9, 2.3E-9, 2.3E-9, 2.4E-9, 2.4E-9, 2.4E-9, 2.4E-9, 2.4E-9,	031480
32.4E-9, 2.4E-9, 2.4E-9, 2.4E-9, 2.4E-9, 2.4E-9, 2.4E-9, 2.4E-9,	031490
42.4E-9, 2.4E-9, 2.4E-9, 2.4E-9, 2.4E-9, 2.4E-9, 2.4E-9, 2.4E-9,	031500
52.4E-9, 2.4E-9/	031510
DATA DA23/2.828E03, 5.371E02, 1.192E02, 6.337E01, 6.069E01,	031520
1 5.675E01, 5.585E01, 5.048E01, 4.511E01, 4.314E01, 2.667E01, 1.4555E01,	031530
2 8.826E00, 5.706E00, 3.574E00, 2.238E00, 1.148E00, 8.223E-01, 4.219E-01,	031540
3 3.022E-01, 1.550E-01, 7.960E-02, 5.704E-02, 2.329E-02, 2.099E-02,	031550
4 1.078E-02, 5.580E-03, 4.014E-03, 2.078E-03, 1.495E-03, 7.735E-04,	031560
5 4.003E-04, 2.880E-04, 1.490E-04, 1.072E-04, 5.550E-05, 2.144E-05,	031570
6 1.332E-05, 5.144E-06, 3.196E-06, 1.234E-06/	031580
END	031590
LIBRARY(LIB,NEW)	031600
ADD(*,MAIN,AL=1)	031610
ADD(*,LG3)	031620
FINISH.	031630
ENDRUN.	031640

***** OXOXIDX //// END OF LIST ////
 ***** OXOXIDX //// END OF LIST ////

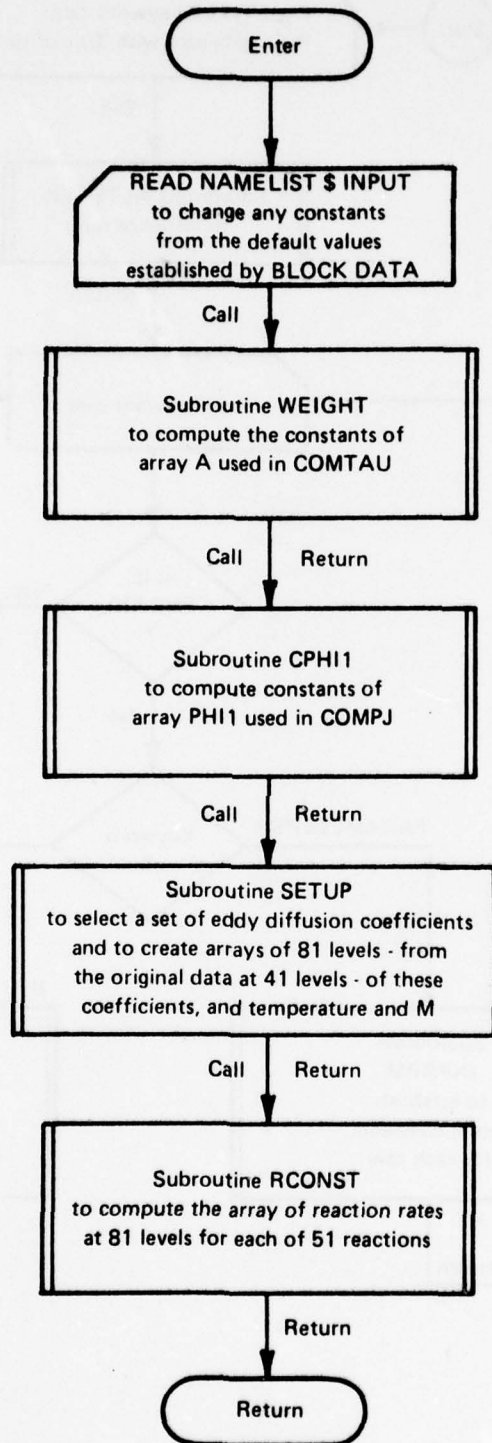
APPENDIX B

FLOW CHARTS

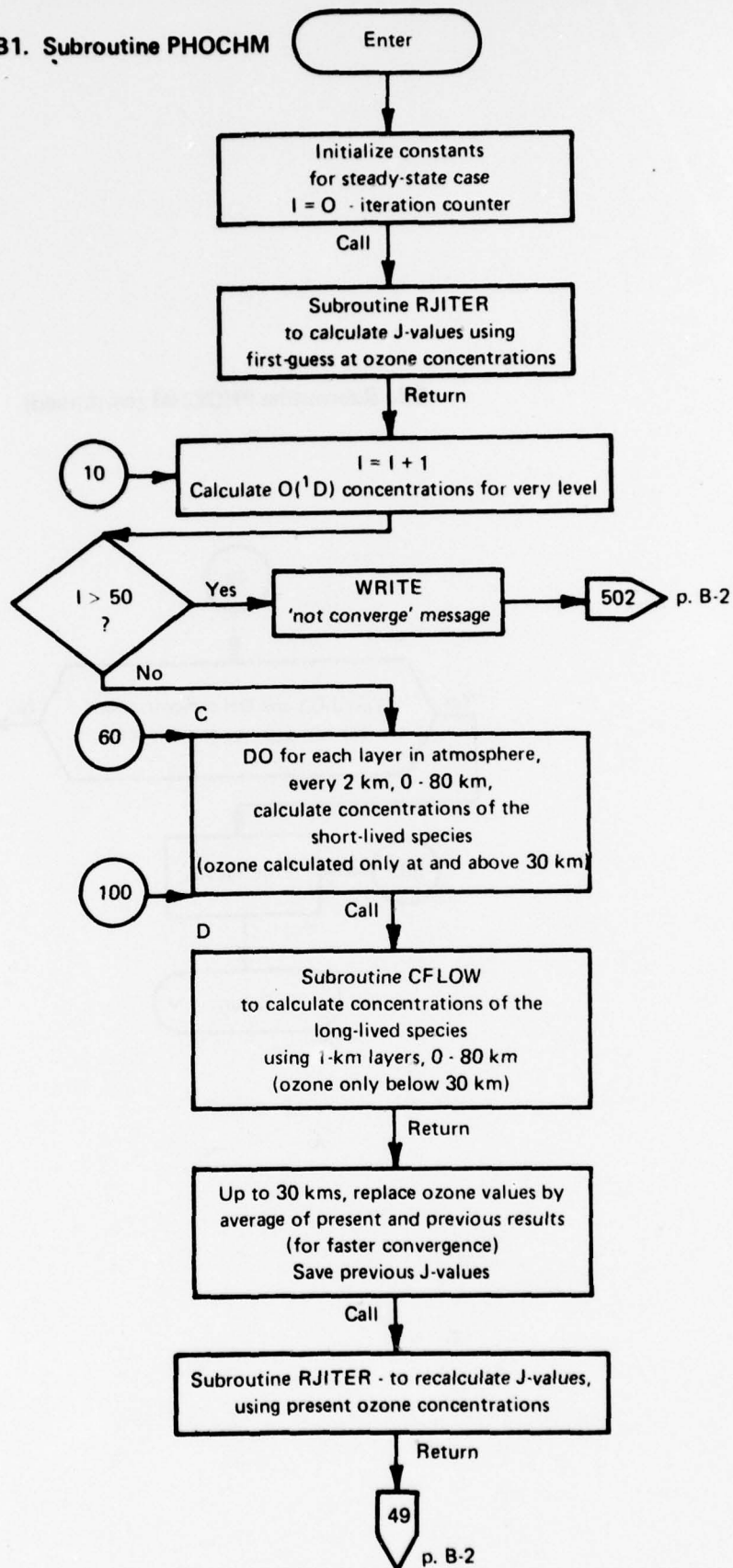
CMSP Chlorine Model Study Program



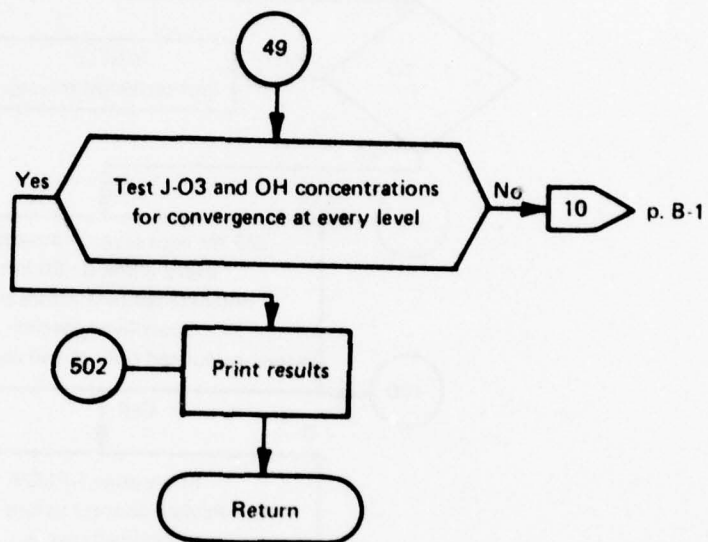
A. Subroutine INPARM



B1. Subroutine PHOCHM



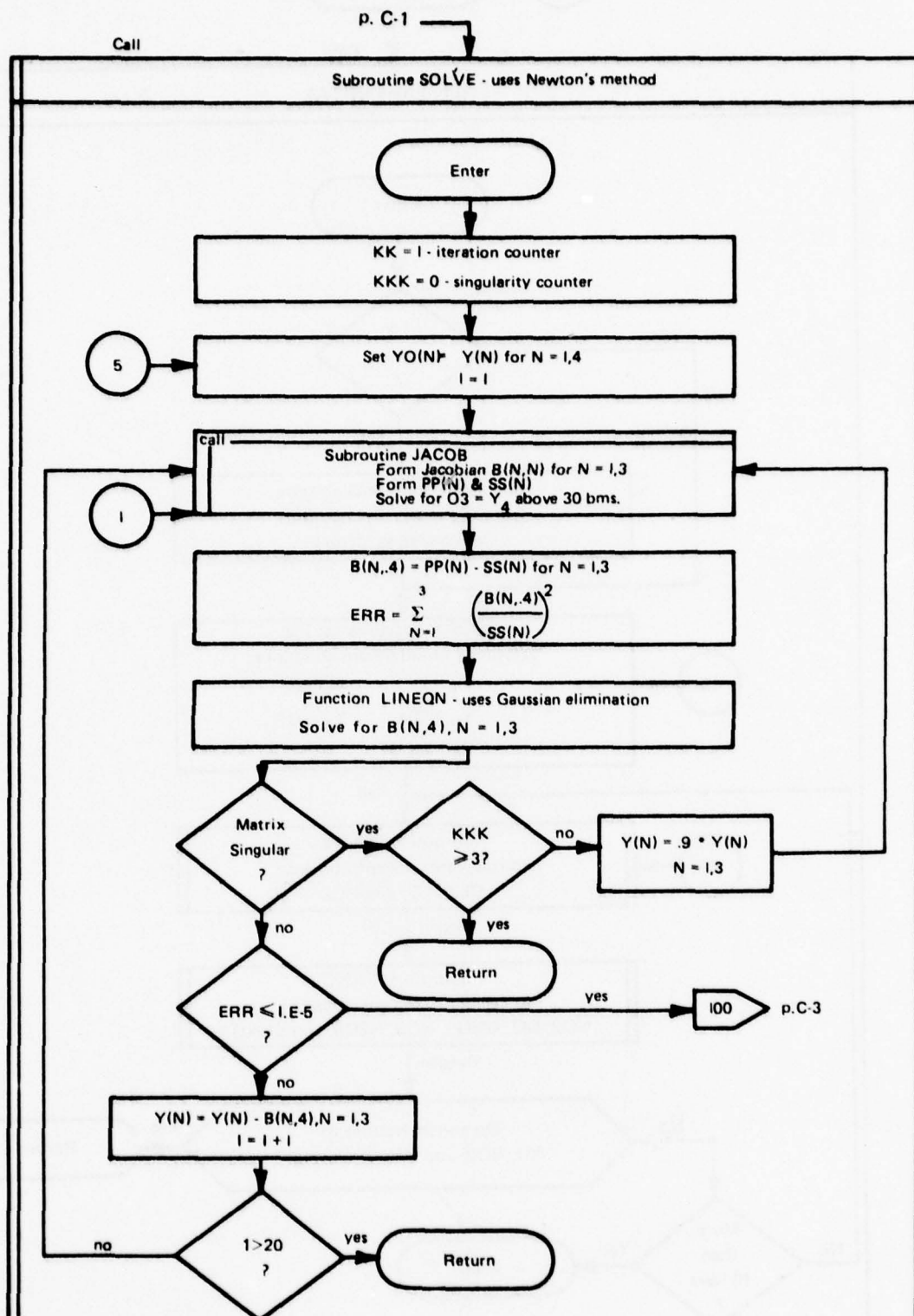
B2. Subroutine PHOCHM (continued)



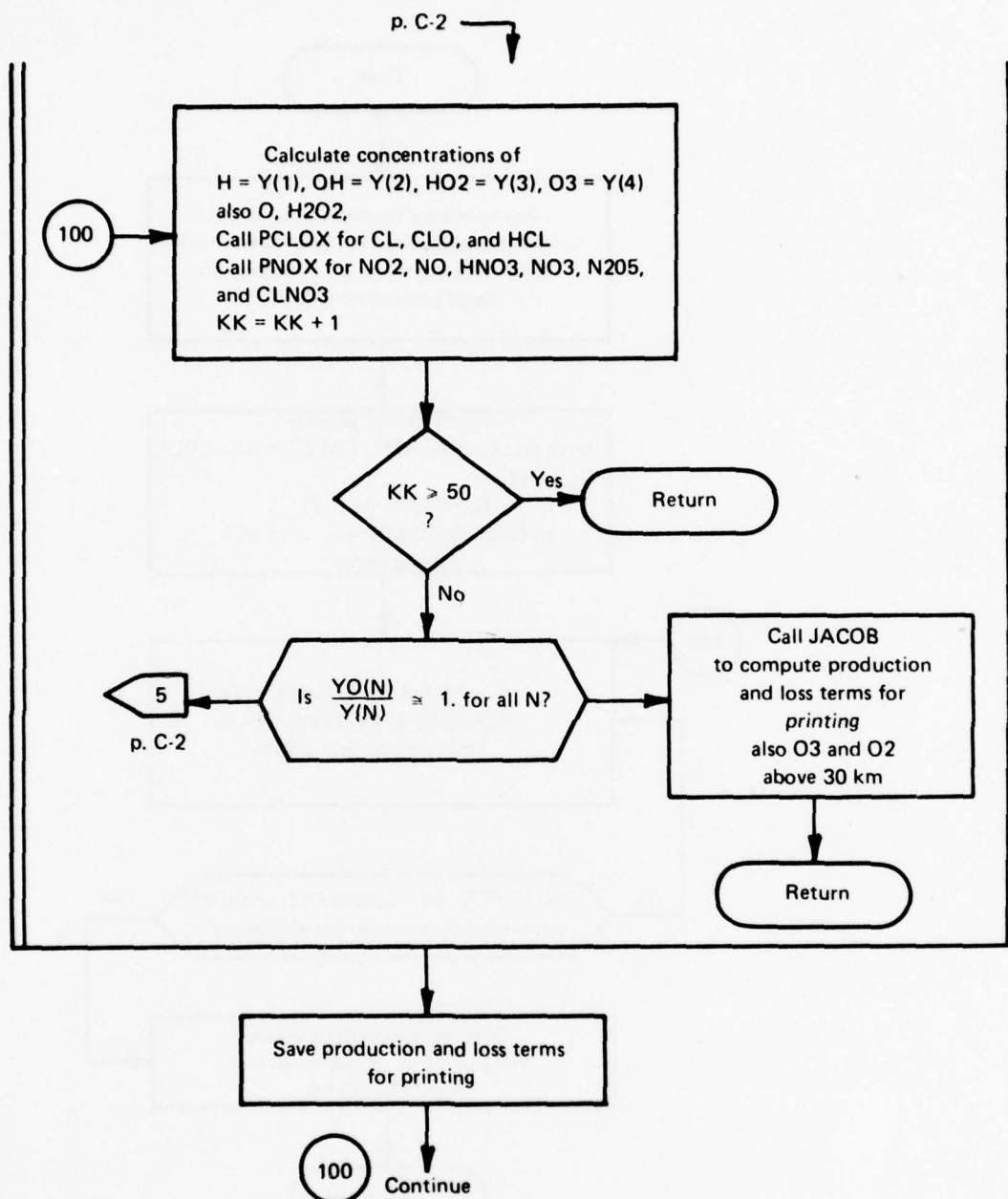
60



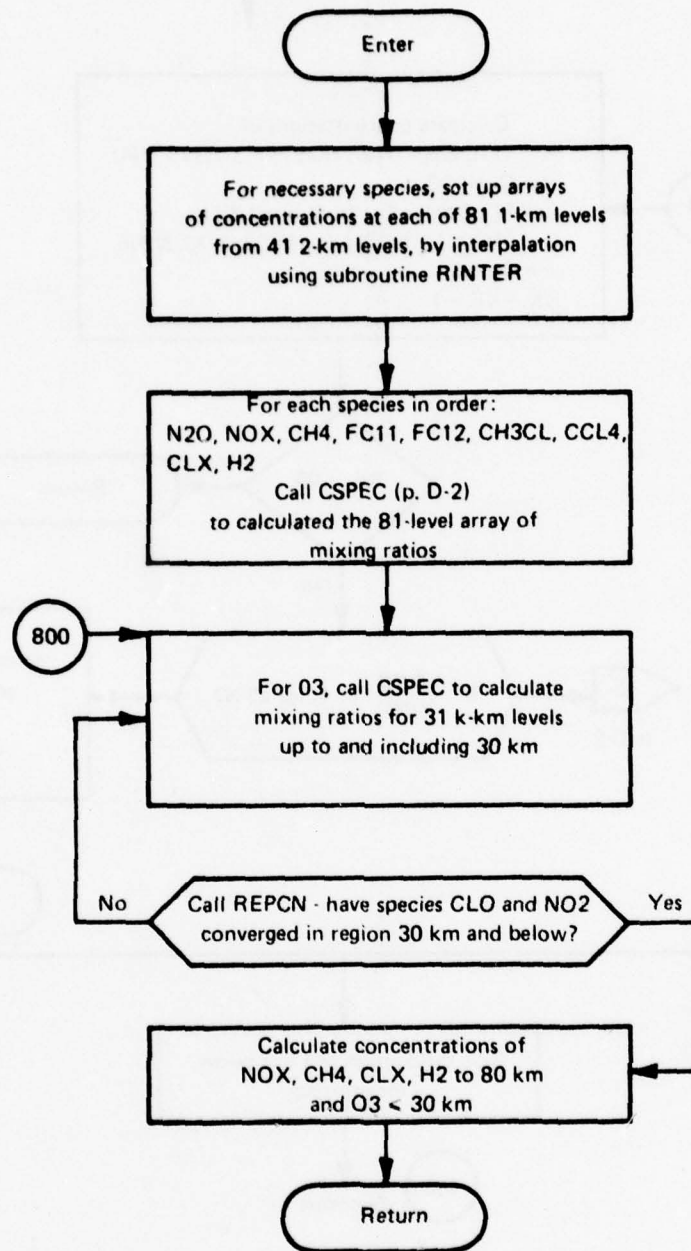
C2. Subroutine SOLVE - Short-lived Species



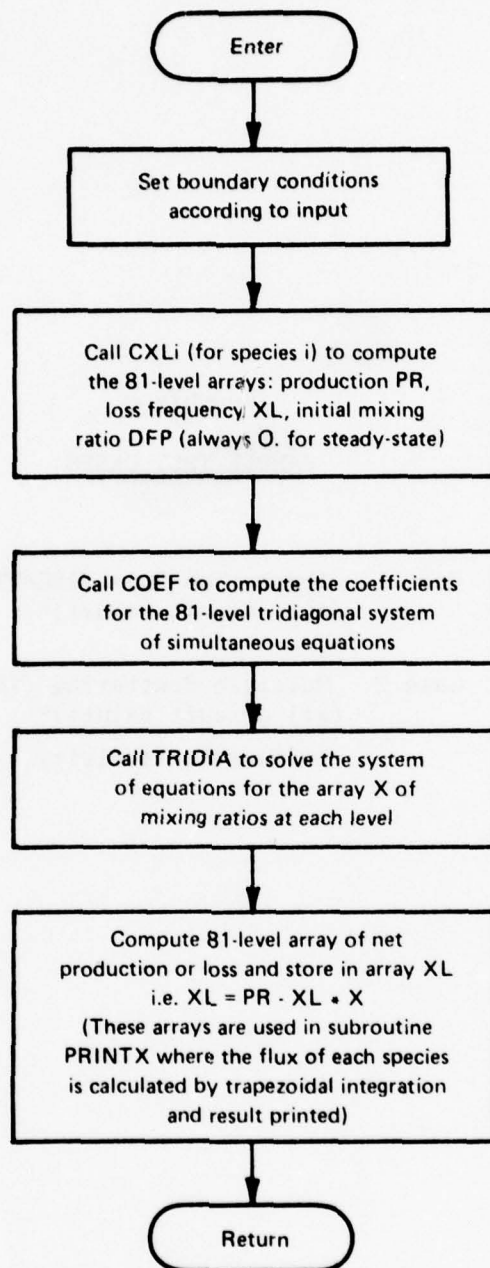
C3. Subroutine SOLVE (continued)



D1. Subroutine CFLOW - Long-lived Species



D2. Subroutine CSPEC



APPENDIX C
SAMPLE TEST CASES

Case 1 Absorption Only (ISCATT = 0)
(all default values)*

Case 2 Multiple Scattering (ISCATT = 1)
(all default values)*
Surface Reflectivity = 0.2

*Exceptions: ISWITCH = 0 (fixed sun angle)
RF11 = 8.30 E + 05
RF12 = 1.13 E + 06

LAST ITERATION =	ALT	QJ02	QJ03	QJ04	QJ05	QJ06	QJ07	QJ08	QJ09	QJ10	QJ11	QJ12	QJ13	QJ14	QJ15	QJ16	QJ17	QJ18	QJ19	QJ20	QJ21	QJ22	QJ23	QJ24	QJ25	QJ26	QJ27	QJ28	QJ29	QJ30	QJ31	QJ32	QJ33	QJ34	QJ35	QJ36	QJ37	QJ38	QJ39	QJ40	QJ41	QJ42	QJ43	QJ44	QJ45	QJ46	QJ47	QJ48	QJ49	QJ50	QJ51	QJ52	QJ53	QJ54	QJ55	QJ56	QJ57	QJ58	QJ59	QJ60	QJ61	QJ62	QJ63	QJ64	QJ65	QJ66	QJ67	QJ68	QJ69	QJ70	QJ71	QJ72	QJ73	QJ74	QJ75	QJ76	QJ77	QJ78	QJ79	QJ80	QJ81	QJ82	QJ83	QJ84	QJ85	QJ86	QJ87	QJ88	QJ89	QJ90	QJ91	QJ92	QJ93	QJ94	QJ95	QJ96	QJ97	QJ98	QJ99	QJ100	QJ101	QJ102	QJ103	QJ104	QJ105	QJ106	QJ107	QJ108	QJ109	QJ110	QJ111	QJ112	QJ113	QJ114	QJ115	QJ116	QJ117	QJ118	QJ119	QJ120	QJ121	QJ122	QJ123	QJ124	QJ125	QJ126	QJ127	QJ128	QJ129	QJ130	QJ131	QJ132	QJ133	QJ134	QJ135	QJ136	QJ137	QJ138	QJ139	QJ140	QJ141	QJ142	QJ143	QJ144	QJ145	QJ146	QJ147	QJ148	QJ149	QJ150	QJ151	QJ152	QJ153	QJ154	QJ155	QJ156	QJ157	QJ158	QJ159	QJ160	QJ161	QJ162	QJ163	QJ164	QJ165	QJ166	QJ167	QJ168	QJ169	QJ170	QJ171	QJ172	QJ173	QJ174	QJ175	QJ176	QJ177	QJ178	QJ179	QJ180	QJ181	QJ182	QJ183	QJ184	QJ185	QJ186	QJ187	QJ188	QJ189	QJ190	QJ191	QJ192	QJ193	QJ194	QJ195	QJ196	QJ197	QJ198	QJ199	QJ200	QJ201	QJ202	QJ203	QJ204	QJ205	QJ206	QJ207	QJ208	QJ209	QJ210	QJ211	QJ212	QJ213	QJ214	QJ215	QJ216	QJ217	QJ218	QJ219	QJ220	QJ221	QJ222	QJ223	QJ224	QJ225	QJ226	QJ227	QJ228	QJ229	QJ230	QJ231	QJ232	QJ233	QJ234	QJ235	QJ236	QJ237	QJ238	QJ239	QJ240	QJ241	QJ242	QJ243	QJ244	QJ245	QJ246	QJ247	QJ248	QJ249	QJ250	QJ251	QJ252	QJ253	QJ254	QJ255	QJ256	QJ257	QJ258	QJ259	QJ260	QJ261	QJ262	QJ263	QJ264	QJ265	QJ266	QJ267	QJ268	QJ269	QJ270	QJ271	QJ272	QJ273	QJ274	QJ275	QJ276	QJ277	QJ278	QJ279	QJ280	QJ281	QJ282	QJ283	QJ284	QJ285	QJ286	QJ287	QJ288	QJ289	QJ290	QJ291	QJ292	QJ293	QJ294	QJ295	QJ296	QJ297	QJ298	QJ299	QJ300	QJ301	QJ302	QJ303	QJ304	QJ305	QJ306	QJ307	QJ308	QJ309	QJ310	QJ311	QJ312	QJ313	QJ314	QJ315	QJ316	QJ317	QJ318	QJ319	QJ320	QJ321	QJ322	QJ323	QJ324	QJ325	QJ326	QJ327	QJ328	QJ329	QJ330	QJ331	QJ332	QJ333	QJ334	QJ335	QJ336	QJ337	QJ338	QJ339	QJ340	QJ341	QJ342	QJ343	QJ344	QJ345	QJ346	QJ347	QJ348	QJ349	QJ350	QJ351	QJ352	QJ353	QJ354	QJ355	QJ356	QJ357	QJ358	QJ359	QJ360	QJ361	QJ362	QJ363	QJ364	QJ365	QJ366	QJ367	QJ368	QJ369	QJ370	QJ371	QJ372	QJ373	QJ374	QJ375	QJ376	QJ377	QJ378	QJ379	QJ380
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LAST ITERATION = 9

ALT	CJCL03	CJN20	CJ4N03	CJ4N02	CJN205	CJCL04	CJCM30L
0.	3.069E-15	2.477E-26	1.941E-17	1.504E-06	1.476E-05	3.255E-20	1.970E-33
240000.	3.682E-05	1.458E-06	1.374E-07	1.614E-06	1.413E-05	1.775E-24	1.320E-29
340000.	3.693E-05	2.477E-25	2.301E-07	1.523E-06	1.414E-05	7.000E-23	2.497E-26
500000.	3.718E-15	1.500E-24	2.032E-17	1.031E-16	1.423E-05	1.544E-22	2.022E-23
600000.	3.711E-12	7.344E-20	2.008E-17	1.639E-16	4.427E-05	4.380E-19	9.739E-21
1000000.	3.728E-15	1.157E-17	2.374E-07	1.632E-16	1.432E-05	5.852E-14	2.203E-18
1200000.	3.732E-15	9.468E-15	2.141E-17	1.657E-16	1.437E-05	5.091E-14	2.040E-16
1400000.	3.746E-15	4.427E-11	2.179E-07	1.674E-16	1.444E-05	2.054E-12	9.702E-15
1600000.	3.771E-05	1.013E-12	2.177E-07	1.692E-16	1.457E-05	4.292E-11	7.557E-17
1800000.	3.629E-15	1.111E-14	2.352E-07	1.744E-16	1.453E-05	4.485E-10	2.734E-12
2000000.	3.935E-15	1.073E-11	2.788E-07	1.539E-16	1.437E-05	2.002E-10	1.964E-11
2200000.	4.058E-05	3.314E-10	2.712E-07	1.995E-16	1.544E-05	1.395E-08	1.006E-10
2400000.	4.338E-05	1.513E-09	3.347E-07	2.215E-16	1.728E-05	5.179E-18	4.021E-10
2600000.	4.718E-05	4.447E-09	1.230E-06	2.570E-16	1.911E-15	1.714E-07	1.349E-09
2800000.	5.215E-05	1.296E-09	2.777E-06	3.100E-16	2.236E-15	4.719E-07	7.602E-09
3000000.	6.259E-05	2.913E-09	5.355E-06	3.100E-16	2.344E-15	1.118E-05	5.184E-09
3200000.	9.137E-05	7.507E-08	1.114E-05	3.124E-16	3.943E-15	2.688E-05	1.544E-08
3400000.	1.097E-04	8.553E-08	1.532E-05	3.924E-16	5.503E-15	3.944E-05	2.465E-08
3600000.	1.501E-04	1.241E-07	2.233E-05	1.271E-15	7.949E-15	7.890E-05	3.412E-08
3800000.	2.024E-04	1.561E-07	3.477E-05	1.707E-15	1.074E-14	7.745E-16	4.259E-08
4000000.	2.615E-14	1.823E-07	5.333E-05	2.514E-15	1.395E-14	9.747E-16	4.951E-08
4200000.	3.204E-04	2.027E-07	7.852E-05	2.979E-15	1.693E-14	1.047E-15	5.490E-08
4400000.	3.373E-04	2.183E-07	9.240E-05	3.408E-15	1.943E-14	1.134E-15	5.937E-08
4600000.	4.109E-04	2.705E-07	1.349E-15	7.835E-15	2.192E-14	1.159E-15	6.718E-08
4800000.	4.528E-04	2.444E-07	1.768E-05	4.164E-15	2.763E-14	1.248E-15	7.714E-08
5000000.	4.784E-04	2.492E-07	1.977E-05	4.444E-15	2.952E-14	1.288E-15	8.213E-08
5200000.	4.970E-04	2.580E-07	2.142E-05	4.657E-15	3.150E-14	1.324E-15	8.897E-08
5400000.	5.105E-04	2.675E-07	2.220E-05	4.794E-15	3.267E-14	1.354E-15	9.413E-08
5600000.	5.208E-04	2.749E-07	2.322E-05	4.888E-15	3.374E-14	1.392E-15	9.987E-08
5800000.	5.282E-04	2.802E-07	2.430E-05	4.944E-15	3.460E-14	1.427E-15	1.034E-07
6000000.	5.334E-04	3.071E-07	2.527E-05	5.028E-15	3.546E-14	1.462E-15	1.070E-07
6200000.	5.378E-04	3.165E-07	2.623E-05	5.075E-15	3.630E-14	1.496E-15	1.104E-07
6400000.	5.405E-04	3.249E-07	2.713E-05	5.114E-15	3.714E-14	1.528E-15	1.136E-07
6600000.	5.429E-04	3.295E-07	2.805E-05	5.145E-15	3.798E-14	1.557E-15	1.167E-07
6800000.	5.447E-04	3.356E-07	2.901E-05	5.171E-15	3.883E-14	1.583E-15	1.193E-07
7000000.	5.460E-04	3.477E-07	3.004E-05	5.192E-15	3.974E-14	1.605E-15	1.218E-07
7200000.	5.471E-04	3.575E-07	3.115E-05	5.211E-15	4.069E-14	1.623E-15	1.237E-07
7400000.	5.477E-04	3.676E-07	3.235E-05	5.229E-15	4.167E-14	1.637E-15	1.251E-07
7600000.	5.482E-04	3.783E-07	3.361E-05	5.245E-15	4.268E-14	1.648E-15	1.262E-07
7800000.	5.487E-04	3.897E-07	3.493E-05	5.259E-15	4.371E-14	1.657E-15	1.271E-07
8000000.	5.494E-04	4.017E-07	3.632E-05	5.273E-15	4.476E-14	1.663E-15	1.278E-07

LAST ITERATION + 1

ALT	CJ2	CJ3	CJ4	CJ5	CJ6	CJ7	CJ8	CJ9	PCVOT	JOINT	QINI	PREVOM
7.78E-15	3.77E-15	1.83E-15	7.77E-15	7.77E-15	7.77E-15	7.77E-15	7.77E-15	7.77E-15	7.77E-15	7.77E-15	7.77E-15	7.77E-15
3.05E-31	3.05E-31	1.13E-31	3.05E-31	3.05E-31	3.05E-31	3.05E-31	3.05E-31	3.05E-31	3.05E-31	3.05E-31	3.05E-31	3.05E-31
6.50E-28	3.87E-05	2.13E-28	6.50E-28	6.50E-28	6.50E-28	6.50E-28	6.50E-28	6.50E-28	6.50E-28	6.50E-28	6.50E-28	6.50E-28
3.19E-25	3.87E-12	1.37E-25	3.19E-25	3.19E-25	3.19E-25	3.19E-25	3.19E-25	3.19E-25	3.19E-25	3.19E-25	3.19E-25	3.19E-25
3.38E-23	3.31E-13	3.33E-23	3.38E-23	3.38E-23	3.38E-23	3.38E-23	3.38E-23	3.38E-23	3.38E-23	3.38E-23	3.38E-23	3.38E-23
1.23E-20	3.04E-06	2.13E-20	1.23E-20	1.23E-20	1.23E-20	1.23E-20	1.23E-20	1.23E-20	1.23E-20	1.23E-20	1.23E-20	1.23E-20
3.87E-12	3.04E-06	1.31E-12	3.87E-12	3.87E-12	3.87E-12	3.87E-12	3.87E-12	3.87E-12	3.87E-12	3.87E-12	3.87E-12	3.87E-12
3.49E-17	3.53E-05	3.37E-14	3.49E-17	3.49E-17	3.49E-17	3.49E-17	3.49E-17	3.49E-17	3.49E-17	3.49E-17	3.49E-17	3.49E-17
7.25E-16	3.10E-05	2.13E-16	7.25E-16	7.25E-16	7.25E-16	7.25E-16	7.25E-16	7.25E-16	7.25E-16	7.25E-16	7.25E-16	7.25E-16
7.48E-15	3.79E-05	7.22E-11	7.48E-15	7.48E-15	7.48E-15	7.48E-15	7.48E-15	7.48E-15	7.48E-15	7.48E-15	7.48E-15	7.48E-15
4.58E-14	3.45E-05	3.13E-10	4.58E-14	4.58E-14	4.58E-14	4.58E-14	4.58E-14	4.58E-14	4.58E-14	4.58E-14	4.58E-14	4.58E-14
2.62E-13	3.56E-15	7.22E-10	2.62E-13	2.62E-13	2.62E-13	2.62E-13	2.62E-13	2.62E-13	2.62E-13	2.62E-13	2.62E-13	2.62E-13
7.42E-13	3.44E-05	1.43E-10	7.42E-13	7.42E-13	7.42E-13	7.42E-13	7.42E-13	7.42E-13	7.42E-13	7.42E-13	7.42E-13	7.42E-13
3.08E-12	3.44E-05	1.43E-10	3.08E-12	3.08E-12	3.08E-12	3.08E-12	3.08E-12	3.08E-12	3.08E-12	3.08E-12	3.08E-12	3.08E-12
3.07E-12	1.11E-04	1.35E-10	3.07E-12	3.07E-12	3.07E-12	3.07E-12	3.07E-12	3.07E-12	3.07E-12	3.07E-12	3.07E-12	3.07E-12
4.10E-11	1.03E-14	7.18E-06	4.10E-11	4.10E-11	4.10E-11	4.10E-11	4.10E-11	4.10E-11	4.10E-11	4.10E-11	4.10E-11	4.10E-11
4.74E-11	2.32E-05	1.21E-17	4.74E-11	4.74E-11	4.74E-11	4.74E-11	4.74E-11	4.74E-11	4.74E-11	4.74E-11	4.74E-11	4.74E-11
9.12E-11	7.55E-07	2.13E-17	9.12E-11	9.12E-11	9.12E-11	9.12E-11	9.12E-11	9.12E-11	9.12E-11	9.12E-11	9.12E-11	9.12E-11
1.31E-10	5.40E-07	3.11E-17	1.31E-10	1.31E-10	1.31E-10	1.31E-10	1.31E-10	1.31E-10	1.31E-10	1.31E-10	1.31E-10	1.31E-10
1.89E-10	3.45E-07	3.74E-17	1.89E-10	1.89E-10	1.89E-10	1.89E-10	1.89E-10	1.89E-10	1.89E-10	1.89E-10	1.89E-10	1.89E-10
2.46E-10	1.74E-07	4.34E-17	2.46E-10	2.46E-10	2.46E-10	2.46E-10	2.46E-10	2.46E-10	2.46E-10	2.46E-10	2.46E-10	2.46E-10
2.07E-10	1.03E-07	4.31E-17	2.07E-10	2.07E-10	2.07E-10	2.07E-10	2.07E-10	2.07E-10	2.07E-10	2.07E-10	2.07E-10	2.07E-10
3.46E-10	2.02E-07	5.13E-17	3.46E-10	3.46E-10	3.46E-10	3.46E-10	3.46E-10	3.46E-10	3.46E-10	3.46E-10	3.46E-10	3.46E-10
3.75E-10	3.04E-07	5.23E-17	3.75E-10	3.75E-10	3.75E-10	3.75E-10	3.75E-10	3.75E-10	3.75E-10	3.75E-10	3.75E-10	3.75E-10
4.80E-10	3.47E-07	5.73E-17	4.80E-10	4.80E-10	4.80E-10	4.80E-10	4.80E-10	4.80E-10	4.80E-10	4.80E-10	4.80E-10	4.80E-10
5.00E-10	3.70E-07	5.11E-17	5.00E-10	5.00E-10	5.00E-10	5.00E-10	5.00E-10	5.00E-10	5.00E-10	5.00E-10	5.00E-10	5.00E-10
4.66E-10	3.73E-07	5.13E-17	4.66E-10	4.66E-10	4.66E-10	4.66E-10	4.66E-10	4.66E-10	4.66E-10	4.66E-10	4.66E-10	4.66E-10
3.08E-10	3.04E-07	5.23E-17	3.08E-10	3.08E-10	3.08E-10	3.08E-10	3.08E-10	3.08E-10	3.08E-10	3.08E-10	3.08E-10	3.08E-10
5.63E-10	3.77E-07	5.73E-17	5.63E-10	5.63E-10	5.63E-10	5.63E-10	5.63E-10	5.63E-10	5.63E-10	5.63E-10	5.63E-10	5.63E-10
5.32E-10	3.47E-07	5.11E-17	5.32E-10	5.32E-10	5.32E-10	5.32E-10	5.32E-10	5.32E-10	5.32E-10	5.32E-10	5.32E-10	5.32E-10
7.11E-10	3.70E-07	5.11E-17	7.11E-10	7.11E-10	7.11E-10	7.11E-10	7.11E-10	7.11E-10	7.11E-10	7.11E-10	7.11E-10	7.11E-10
9.00E-10	3.70E-07	5.11E-17	9.00E-10	9.00E-10	9.00E-10	9.00E-10	9.00E-10	9.00E-10	9.00E-10	9.00E-10	9.00E-10	9.00E-10
3.07E-10	3.70E-07	5.11E-17	3.07E-10	3.07E-10	3.07E-10	3.07E-10	3.07E-10	3.07E-10	3.07E-10	3.07E-10	3.07E-10	3.07E-10
1.15E-09	3.70E-07	5.11E-17	1.15E-09	1.15E-09	1.15E-09	1.15E-09	1.15E-09	1.15E-09	1.15E-09	1.15E-09	1.15E-09	1.15E-09
1.17E-09	3.70E-07	5.11E-17	1.17E-09	1.17E-09	1.17E-09	1.17E-09	1.17E-09	1.17E-09	1.17E-09	1.17E-09	1.17E-09	1.17E-09
1.41E-09	3.70E-07	5.11E-17	1.41E-09	1.41E-09	1.41E-09	1.41E-09	1.41E-09	1.41E-09	1.41E-09	1.41E-09	1.41E-09	1.41E-09
1.70E-09	3.70E-07	5.11E-17	1.70E-09	1.70E-09	1.70E-09	1.70E-09	1.70E-09	1.70E-09	1.70E-09	1.70E-09	1.70E-09	1.70E-09
2.21E-09	3.70E-07	5.11E-17	2.21E-09	2.21E-09	2.21E-09	2.21E-09	2.21E-09	2.21E-09	2.21E-09	2.21E-09	2.21E-09	2.21E-09
2.74E-09	3.70E-07	5.11E-17	2.74E-09	2.74E-09	2.74E-09	2.74E-09	2.74E-09	2.74E-09	2.74E-09	2.74E-09	2.74E-09	2.74E-09
3.29E-09	3.70E-07	5.11E-17	3.29E-09	3.29E-09	3.29E-09	3.29E-09	3.29E-09	3.29E-09	3.29E-09	3.29E-09	3.29E-09	3.29E-09
3.65E-09	3.70E-07	5.11E-17	3.65E-09	3.65E-09	3.65E-09	3.65E-09	3.65E-09	3.65E-09	3.65E-09	3.65E-09	3.65E-09	3.65E-09

LAST ITERATION *

ALT	CJCL07	CJN20	CJ4N03	CJ4N02	CJN205	CJCL14	CJCL01
200000	3.27E-05	2.00E-03	1.94E-03	1.64E-06	1.47E-05	3.46E-03	2.00E-33
200000	3.53E-03	1.40E-02	1.30E-07	1.64E-06	1.47E-05	1.79E-24	1.33E-29
500000	3.60E-05	2.00E-03	2.00E-07	1.64E-06	1.47E-05	3.03E-27	2.00E-26
500000	3.70E-03	1.40E-02	2.00E-07	1.64E-06	1.47E-05	4.56E-27	2.00E-27
800000	3.72E-03	5.97E-02	2.00E-07	1.64E-06	1.47E-05	4.39E-19	0.79E-24
1000000	3.72E-03	1.10E-07	2.00E-07	1.64E-06	1.47E-05	4.48E-16	2.21E-16
1200000	3.72E-03	3.30E-14	2.00E-07	1.64E-06	1.47E-05	5.11E-14	2.04E-16
1400000	3.72E-03	4.44E-14	2.00E-07	1.64E-06	1.47E-05	2.05E-12	0.73E-15
1500000	3.72E-03	1.00E-14	2.00E-07	1.64E-06	1.47E-05	4.37E-11	2.34E-13
1500000	3.72E-03	1.10E-14	2.00E-07	1.64E-06	1.47E-05	4.41E-11	2.74E-12
2000000	3.72E-03	7.09E-11	2.00E-07	1.64E-06	1.47E-05	4.91E-09	1.94E-11
2000000	3.72E-03	3.02E-11	2.00E-07	1.64E-06	1.47E-05	1.39E-08	1.04E-10
2400000	4.34E-03	1.50E-11	3.55E-07	2.21E-05	1.73E-06	5.69E-06	4.02E-10
2500000	4.70E-05	4.10E-09	1.22E-06	2.87E-05	1.73E-06	4.71E-07	1.32E-09
2800000	5.71E-05	1.29E-08	3.75E-03	7.24E-03	2.73E-06	4.72E-07	7.60E-09
3000000	5.70E-05	3.91E-08	5.94E-06	4.02E-05	2.95E-05	1.44E-06	8.19E-09
3200000	8.13E-05	5.51E-08	1.01E-06	6.12E-05	3.94E-05	2.27E-06	1.54E-08
3400000	1.09E-04	3.03E-07	4.57E-06	9.92E-05	5.67E-05	7.94E-06	4.46E-08
3500000	1.51E-04	1.44E-07	2.42E-06	1.27E-05	7.32E-05	5.39E-06	3.43E-08
7000000	2.12E-04	1.53E-07	2.37E-05	1.70E-05	1.07E-04	7.70E-06	4.29E-08
4000000	2.45E-04	1.82E-07	7.13E-05	2.34E-05	1.34E-04	9.30E-06	4.95E-08
4200000	3.40E-04	2.00E-07	3.33E-06	2.50E-05	1.59E-04	1.04E-05	5.40E-08
4400000	3.37E-04	2.60E-07	4.40E-05	3.40E-05	1.76E-04	1.13E-05	5.93E-08
4600000	4.43E-04	2.00E-07	1.54E-05	7.03E-05	2.10E-04	1.19E-05	6.31E-08
4800000	4.52E-04	2.44E-07	1.75E-05	1.84E-05	2.33E-04	1.24E-05	6.74E-08
5000000	4.78E-04	2.44E-07	1.75E-05	1.84E-05	2.33E-04	1.24E-05	6.74E-08
5200000	4.91E-04	2.59E-07	3.11E-05	4.65E-05	2.61E-04	1.32E-05	7.89E-08
5400000	5.10E-04	2.57E-07	5.22E-05	7.90E-05	2.67E-04	1.38E-05	8.81E-08
5500000	5.20E-04	2.79E-07	5.32E-05	8.84E-05	2.72E-04	1.39E-05	9.98E-08
5800000	5.28E-04	2.90E-07	5.43E-05	9.94E-05	2.76E-04	1.42E-05	1.13E-07
6000000	5.28E-04	3.07E-07	5.52E-05	1.04E-05	2.79E-04	1.46E-05	1.28E-07
6200000	5.27E-04	3.15E-07	5.52E-05	1.04E-05	2.81E-04	1.49E-05	1.44E-07
6400000	5.40E-04	3.20E-07	5.72E-05	1.14E-05	2.81E-04	1.52E-05	1.60E-07
6500000	5.42E-04	3.20E-07	5.91E-05	1.45E-05	2.82E-04	1.55E-05	1.75E-07
6800000	5.44E-04	3.30E-07	5.90E-05	1.74E-05	2.83E-04	1.58E-05	1.93E-07
7000000	5.40E-04	3.74E-07	6.07E-05	1.92E-05	2.84E-04	1.60E-05	2.10E-07
7200000	5.47E-04	4.00E-07	6.07E-05	5.21E-05	2.84E-04	1.62E-05	2.35E-07
7400000	5.47E-04	4.37E-07	6.08E-05	5.29E-05	2.84E-04	1.63E-05	2.61E-07
7500000	5.48E-04	4.64E-07	6.12E-05	5.43E-05	2.84E-04	1.64E-05	2.87E-07
7900000	5.48E-04	5.44E-07	6.24E-05	5.95E-05	2.84E-04	1.65E-05	3.12E-07
8000000	5.49E-04	5.61E-07	6.33E-05	6.27E-05	2.85E-04	1.66E-05	3.34E-07

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CHUCKLINE MODEL RUN PROGRAM

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K	ALT	H	74	40C	H2O2	N	DT	O3INT	N(O)
1	250000	4.25E+01	7.19E+06	1.17E+09	1.09E+11	4.22E+03	7.23E+11	8.91E+18	8.10E-03
2	250000	2.43E+01	4.72E+06	7.32E+08	1.17E+11	2.02E+03	5.92E+11	8.78E+18	7.84E-03
3	250000	2.77E+01	5.30E+06	7.99E+08	6.37E+10	2.71E+03	4.93E+11	6.37E+18	8.26E-03
4	250000	4.51E+01	8.37E+06	4.72E+09	3.60E+10	7.44E+03	4.73E+11	6.58E+18	9.29E-03
5	300000	5.26E+01	7.97E+06	2.61E+08	1.47E+10	4.45E+03	4.13E+11	8.49E+18	1.06E-02
6	150000	4.35E+01	7.23E+06	1.73E+08	5.67E+09	4.83E+03	4.63E+11	8.48E+18	1.50E-02
7	120000	3.07E+01	7.33E+06	1.12E+08	4.07E+09	1.20E+03	5.97E+11	8.30E+18	2.45E-02
8	140000	1.00E+01	1.22E+06	5.05E+07	5.20E+03	1.82E+04	7.57E+11	8.16E+18	3.84E-02
9	130000	2.37E+01	2.31E+06	3.37E+07	3.63E+08	6.78E+04	1.47E+12	7.94E+18	1.07E-01
10	140000	4.68E+01	5.07E+06	7.70E+07	1.41E+09	7.46E+05	3.33E+12	7.46E+18	4.07E-01
11	200000	3.59E+01	7.22E+06	9.05E+07	1.81E+09	8.81E+05	4.42E+12	6.94E+18	9.68E-01
12	200000	1.25E+01	1.02E+06	1.02E+08	2.62E+09	2.78E+05	5.07E+12	5.73E+18	2.10E+00
13	200000	7.87E+01	1.75E+06	1.19E+08	2.66E+09	5.73E+05	5.37E+12	4.88E+18	4.45E+00
14	200000	5.97E+01	1.33E+06	1.30E+08	2.61E+09	1.06E+07	5.23E+12	2.67E+18	1.12E+00
15	200000	4.74E+01	7.33E+06	1.30E+08	2.67E+09	2.17E+07	4.65E+12	2.63E+18	1.77E+01
16	300000	5.51E+01	4.23E+06	1.22E+08	1.09E+09	4.15E+07	3.71E+12	1.79E+18	7.19E+01
17	320000	1.71E+01	6.13E+06	1.22E+08	9.22E+08	4.82E+07	2.67E+12	1.15E+18	5.31E+01
18	300000	6.39E+01	1.23E+06	1.22E+08	7.35E+08	1.07E+08	1.79E+12	7.12E+17	7.89E+01
19	300000	2.42E+01	1.32E+06	5.93E+07	1.03E+09	1.73E+08	1.07E+12	4.28E+17	1.07E+02
20	300000	5.05E+01	1.33E+06	7.21E+07	4.54E+07	7.70E+08	6.21E+11	2.59E+17	1.27E+02
21	400000	2.85E+01	2.12E+06	7.16E+07	2.07E+08	4.19E+08	3.59E+11	1.61E+17	1.69E+02
22	400000	8.24E+01	2.23E+06	2.61E+07	1.02E+07	6.41E+08	2.18E+11	1.03E+17	1.99E+02
23	400000	2.03E+01	2.21E+06	2.32E+07	8.24E+05	9.76E+08	1.38E+11	6.71E+16	2.21E+02
24	450000	4.06E+01	2.43E+06	1.61E+07	5.14E+06	1.25E+09	8.07E+10	4.50E+16	2.27E+02
25	450000	8.59E+01	1.77E+06	1.61E+07	3.92E+06	4.61E+09	5.73E+10	3.03E+16	2.19E+02
26	500000	1.84E+01	1.55E+06	1.36E+07	2.81E+06	1.02E+09	4.87E+10	2.69E+16	2.00E+02
27	520000	2.75E+01	1.55E+06	1.15E+07	1.93E+06	2.27E+09	4.62E+10	1.42E+16	1.87E+02
28	500000	3.56E+01	4.77E+06	1.01E+07	1.83E+06	2.49E+09	1.80E+10	9.80E+15	1.70E+02
29	500000	2.00E+01	1.04E+06	3.90E+06	1.07E+06	2.71E+09	1.22E+10	6.78E+15	1.50E+02
30	500000	7.80E+01	3.13E+06	7.67E+06	7.80E+05	2.97E+09	8.20E+09	4.73E+15	1.70E+02
31	600000	1.21E+01	1.93E+06	6.67E+06	5.45E+05	7.10E+09	5.55E+09	3.48E+15	1.13E+02
32	620000	1.27E+01	6.53E+06	6.12E+06	7.54E+05	3.70E+09	4.10E+09	2.38E+15	1.05E+02
33	600000	2.09E+01	5.75E+06	4.21E+06	2.66E+05	4.02E+09	3.04E+09	1.66E+15	9.94E+01
34	650000	2.37E+01	4.51E+06	3.45E+06	1.76E+05	4.47E+09	2.70E+09	1.14E+15	9.05E+01
35	680000	4.03E+01	4.23E+06	3.10E+06	9.74E+04	4.55E+09	1.44E+09	7.78E+14	7.63E+01
36	700000	5.75E+01	3.47E+06	2.93E+06	9.14E+04	4.41E+09	8.62E+08	5.90E+14	5.95E+01
37	720000	7.02E+01	3.54E+06	2.91E+06	7.01E+04	4.90E+09	5.13E+08	4.01E+14	5.46E+01
38	730000	1.93E+01	1.13E+06	2.12E+06	7.70E+04	5.82E+09	4.24E+09	2.97E+14	4.95E+01
39	700000	4.77E+01	2.75E+06	1.63E+06	1.57E+04	3.70E+09	3.76E+08	2.21E+14	5.16E+01
40	780000	2.62E+01	1.55E+06	8.07E+05	4.63E+03	5.07E+09	2.73E+08	1.60E+14	5.63E+01
41	800000	3.26E+01	1.12E+06	4.61E+05	1.26E+03	1.77E+10	2.20E+08	1.11E+14	6.15E+01

K	ALT	CL	CL0	MCL	CLM03	DCLX
1	1.3355E+14	5.2270E+10	7.0935E+13	2.2735E+11	1.2304E+09	5.1031E-11
2	5.0300E+12	3.8770E+06	1.3770E+10	5.649E-10	3.9665E+09	5.7000E-10
3	3.5275E+12	2.5950E+16	1.3770E+10	5.649E-10	4.2118E+07	3.1000E-16
4	1.8344E+12	1.3370E+16	1.3400E+13	2.0915E+09	2.7501E+07	1.7000E-10
5	2.8475E+12	3.3355E+16	8.2110E+14	1.7798E+09	9.2728E+06	5.2225E-13
6	2.7807E+12	5.5715E+17	3.3355E+15	1.1144E+14	5.5997E+06	5.2670E-13
7	5.3601E+12	3.3355E+17	5.3735E+14	1.0757E+09	4.9475E+05	1.1000E-16
8	1.3355E+12	2.1439E+15	5.3114E+14	1.0124E+09	4.5705E+05	1.3000E-10
9	7.5715E+12	5.3203E+16	3.3739E+13	1.0655E+09	3.5410E+07	2.4000E-10
10	4.9715E+12	4.7335E+17	6.418E+12	1.2644E+09	4.0755E+08	1.4368E-10
11	3.3775E+12	7.7345E+17	2.3355E+11	9.9248E+09	7.0535E+08	3.9767E-10
12	5.3355E+12	5.3735E+17	4.1215E+11	7.0912E+09	9.6511E+09	6.7536E-10
13	1.0185E+12	1.1018E+14	5.3735E+14	4.8264E+10	9.6929E+08	1.3735E-10
14	1.5345E+12	1.1018E+14	5.3735E+14	4.8264E+10	8.4657E+08	1.6000E-09
15	2.3355E+12	4.2675E+14	1.3455E+10	5.3735E+14	6.7535E+08	2.0000E-09
16	5.3355E+12	7.7345E+17	1.3455E+10	5.3735E+14	4.8037E+09	1.7100E-09
17	2.3355E+12	7.7345E+17	1.3455E+10	5.3735E+14	2.9631E+08	1.0134E-09
18	1.3355E+12	7.7345E+17	1.3455E+10	5.3735E+14	1.4475E+09	6.7075E-10
19	3.3355E+12	1.3355E+12	1.3355E+12	1.3355E+12	5.7825E+17	2.3558E-10
20	5.3355E+12	1.3355E+12	1.3355E+12	1.3355E+12	3.2425E+05	3.6037E-11
21	4.0300E+12	1.3355E+12	1.3355E+12	1.3355E+12	5.7002E+05	8.3851E-12
22	4.2000E+12	1.3355E+12	1.3355E+12	1.3355E+12	4.6058E+09	1.5674E-12
23	4.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	1.1895E+09	7.0194E-13
24	4.5000E+12	1.3355E+12	1.3355E+12	1.3355E+12	1.6817E+09	5.5410E-14
25	4.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	1.6951E+09	1.1362E-14
26	4.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	4.4687E+09	2.4025E-15
27	4.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	8.1950E+09	5.5710E-16
28	4.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	1.4722E+09	1.2702E-16
29	5.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	2.5975E+09	2.8525E-17
30	4.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	4.5711E+09	6.3986E-18
31	6.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	8.6875E+09	1.5413E-18
32	5.2000E+12	1.3355E+12	1.3355E+12	1.3355E+12	1.5895E+09	3.5985E-19
33	6.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	2.7475E+09	7.0984E-20
34	6.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	4.4005E+09	1.6835E-20
35	7.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	8.1799E+06	3.0503E-21
36	7.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	8.7685E+07	5.7125E-22
37	7.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	1.1544E+09	1.0025E-22
38	7.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	1.5694E+08	1.0347E-23
39	7.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	2.1584E+09	3.4523E-24
40	7.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12	3.0077E+10	6.6016E-25
41	8.0000E+12	1.3355E+12	1.3355E+12	1.3355E+12		

K	ALT	4 + 03	04 + 03	402 + 03	W02 + 0	W04 + 0	N02 + 0	FLN + 0	0 + 03	02 + W0
1	200000	7.9413E+00	7.9413E+00	5.4705E+05	1.4673E+02	3.6164E+01	9.8136E+01	4.7055E+00	8.091E+01	7.4835E+16
2	200000	3.8478E+00	3.8478E+00	2.3082E+05	7.7705E+01	2.2645E+01	4.1214E+01	6.6979E-01	2.2102E+01	3.2922E-12
3	400000	2.6717E+00	2.6717E+00	1.6013E+05	6.9322E+01	2.3705E+01	2.2305E+01	6.9632E-01	1.6295E+01	4.2955E-09
4	600000	1.7378E+00	1.7378E+00	6.0795E+04	6.7641E+01	1.3737E+01	1.3987E+01	4.0795E-01	1.3404E+01	1.6987E-06
5	800000	1.2444E+00	1.2444E+00	4.9743E+04	4.9743E+01	1.3878E+01	1.2136E+01	3.6904E-01	1.0559E+01	3.6228E-04
6	1000000	8.2876E-01	8.2876E-01	3.2922E+04	4.5241E+01	1.1801E+01	1.5191E+01	3.1905E-01	1.0917E+01	4.2905E-02
7	1200000	5.7788E-01	5.7788E-01	2.7775E+04	4.7724E+01	1.2877E+01	3.7021E+01	4.1427E-01	1.4506E+01	2.4395E+00
8	1400000	4.0655E-01	4.0655E-01	1.7575E+04	4.7507E+01	9.4477E-02	8.7397E+01	8.7397E+01	7.3107E+01	1.1865E+03
9	1600000	3.1372E-01	3.1372E-01	1.1224E+04	4.1394E+01	5.1845E-01	3.7909E+01	4.6015E+02	1.0458E+03	8.4255E+03
10	1800000	2.4702E-01	2.4702E-01	7.6511E+03	8.4458E+02	5.8555E+00	3.4245E+03	4.6015E+02	1.0458E+03	8.4255E+03
11	2000000	2.0661E-01	2.0661E-01	5.7061E+03	8.2811E+03	2.3555E+01	1.3039E+04	3.1373E+03	4.8776E+03	3.9724E+04
12	2200000	1.7327E-01	1.7327E-01	4.3533E+03	8.2721E+03	7.8900E+01	4.2756E+04	1.1224E+04	1.6454E+04	1.3824E+05
13	2400000	1.4739E-01	1.4739E-01	3.1522E+03	4.1522E+04	2.1075E+02	1.7443E+05	2.7907E+04	4.4728E+04	3.8419E+05
14	2600000	1.2753E-01	1.2753E-01	2.2744E+03	4.3515E+04	7.1164E+02	4.2241E+05	2.8145E+04	1.1566E+05	9.1633E+05
15	2800000	1.1233E-01	1.1233E-01	1.7644E+03	4.0745E+04	4.0170E+02	1.0895E+05	1.1556E+05	2.2713E+05	1.8784E+06
16	3000000	9.7272E-02	9.7272E-02	1.3744E+03	4.0745E+04	5.5702E+03	2.1444E+06	2.7869E+05	3.7900E+05	3.3449E+06
17	3200000	8.2876E-02	8.2876E-02	9.7272E+02	3.5837E+03	1.4547E+04	3.4268E+06	5.7208E+05	5.4674E+05	5.1810E+06
18	3400000	7.0611E-02	7.0611E-02	7.0611E+02	3.2517E+03	3.6244E+04	4.5557E+06	9.9177E+05	6.8933E+05	7.0137E+06
19	3600000	6.0795E-02	6.0795E-02	5.4705E+02	2.7705E+03	3.2517E+03	5.1733E+06	1.6374E+05	7.8202E+05	8.4190E+06
20	3800000	5.2444E-02	5.2444E-02	4.5241E+02	2.4714E+03	1.7351E+04	5.0903E+06	7.2340E+05	8.3204E+05	9.0646E+06
21	4000000	4.5241E-02	4.5241E-02	3.7021E+02	2.0714E+03	3.7021E+03	4.7202E+06	2.5908E+05	8.7918E+05	8.8813E+06
22	4200000	3.9724E-02	3.9724E-02	3.1522E+02	1.7644E+03	3.2517E+03	3.1533E+06	2.5899E+05	9.5217E+05	8.0913E+06
23	4400000	3.4268E-02	3.4268E-02	2.7705E+02	1.4673E+03	2.2645E+03	2.0090E+06	2.7110E+06	1.0227E+06	7.0271E+06
24	4600000	2.9241E-02	2.9241E-02	2.3082E+02	1.1714E+03	1.5151E+03	1.1297E+06	1.6023E+06	1.0495E+06	5.9112E+06
25	4800000	2.4714E-02	2.4714E-02	1.7644E+02	9.7272E+02	1.1714E+03	5.9301E+05	1.308E+06	9.3355E+05	4.9129E+06
26	5000000	2.0714E-02	2.0714E-02	1.3744E+02	8.4458E+02	9.7272E+02	2.9849E+05	5.3249E+05	7.4696E+05	4.1122E+06
27	5200000	1.7644E-02	1.7644E-02	1.0895E+02	7.1164E+02	8.4458E+02	1.9852E+05	3.6952E+05	5.6024E+05	3.4786E+06
28	5400000	1.5151E-02	1.5151E-02	9.7272E+01	6.0795E+01	7.1164E+02	1.4352E+05	2.1755E+05	3.8972E+05	2.9935E+06
29	5600000	1.2877E-02	1.2877E-02	7.0611E+01	5.1845E+01	6.0795E+01	1.0932E+05	1.2185E+05	2.5422E+05	2.6134E+06
30	5800000	1.0917E-02	1.0917E-02	5.4705E+01	4.5241E+01	5.1845E+01	8.4359E+04	6.7124E+04	1.6450E+05	2.3018E+06
31	6000000	9.4477E-03	9.4477E-03	4.1394E+01	3.9724E+01	4.5241E+01	6.2961E+04	3.6482E+04	1.0276E+05	2.0337E+06
32	6200000	8.2876E-03	8.2876E-03	3.2922E+01	3.2922E+01	3.2922E+01	5.233E+04	2.1422E+04	6.5016E+04	1.8036E+06
33	6400000	7.3107E-03	7.3107E-03	2.7775E+01	2.7775E+01	2.7775E+01	4.2672E+04	1.2672E+04	4.2793E+04	1.5835E+06
34	6600000	6.6904E-03	6.6904E-03	2.3082E+01	2.3082E+01	2.3082E+01	3.6084E+04	7.1140E+04	2.5456E+04	1.3940E+06
35	6800000	6.0795E-03	6.0795E-03	1.9852E+01	1.9852E+01	1.9852E+01	3.0842E+04	3.6084E+04	1.2737E+04	1.2525E+06
36	7000000	5.4705E-03	5.4705E-03	1.6013E+01	1.6013E+01	1.6013E+01	2.6134E+04	1.5865E+03	5.3336E+03	1.1483E+06
37	7200000	4.9129E-03	4.9129E-03	1.2877E+01	1.2877E+01	1.2877E+01	2.2182E+04	8.0142E+02	3.0131E+03	1.0020E+06
38	7400000	4.4190E-03	4.4190E-03	1.0895E+01	1.0895E+01	1.0895E+01	1.8672E+04	4.5788E+02	1.6211E+03	9.3031E+05
39	7600000	3.9724E-03	3.9724E-03	9.0646E+00	9.0646E+00	9.0646E+00	1.6211E+04	3.0622E+02	1.1111E+03	8.281E+05
40	7800000	3.5837E-03	3.5837E-03	7.4835E+00	7.4835E+00	7.4835E+00	1.4168E+04	2.3555E+02	8.0636E+02	6.9775E+05
41	8000000	3.2517E-03	3.2517E-03	6.0795E+00	6.0795E+00	6.0795E+00	1.2672E+04	1.9744E+02	5.6441E+02	6.9775E+05
42	8200000	2.9241E-03	2.9241E-03	5.1845E+00	5.1845E+00	5.1845E+00	1.1297E+04	1.6023E+06	2.1632E+12	1.9295E+13
43	8400000	2.6134E-03	2.6134E-03	4.5241E+00	4.5241E+00	4.5241E+00	1.0495E+06	3.4786E+06	2.1632E+12	1.9295E+13
44	8600000	2.3018E-03	2.3018E-03	3.9724E+00	3.9724E+00	3.9724E+00	9.7272E+05	5.9112E+06	2.1632E+12	1.9295E+13
45	8800000	2.0337E-03	2.0337E-03	3.4268E+00	3.4268E+00	3.4268E+00	9.0646E+05	5.9112E+06	2.1632E+12	1.9295E+13
46	9000000	1.8036E-03	1.8036E-03	2.9241E+00	2.9241E+00	2.9241E+00	8.4359E+04	5.9112E+06	2.1632E+12	1.9295E+13
47	9200000	1.6211E-03	1.6211E-03	2.4714E+00	2.4714E+00	2.4714E+00	7.8202E+05	5.9112E+06	2.1632E+12	1.9295E+13
48	9400000	1.4835E-03	1.4835E-03	2.0714E+00	2.0714E+00	2.0714E+00	7.2340E+05	5.9112E+06	2.1632E+12	1.9295E+13
49	9600000	1.3824E-03	1.3824E-03	1.7644E+00	1.7644E+00	1.7644E+00	6.8933E+05	5.9112E+06	2.1632E+12	1.9295E+13
50	9800000	1.308E-03	1.308E-03	1.5151E+00	1.5151E+00	1.5151E+00	6.6904E+05	5.9112E+06	2.1632E+12	1.9295E+13
51	10000000	1.2525E-03	1.2525E-03	1.3940E+00	1.3940E+00	1.3940E+00	6.5016E+05	5.9112E+06	2.1632E+12	1.9295E+13
52	10200000	1.1983E-03	1.1983E-03	1.2877E+00	1.2877E+00	1.2877E+00	6.3249E+05	5.9112E+06	2.1632E+12	1.9295E+13
53	10400000	1.1483E-03	1.1483E-03	1.1865E+00	1.1865E+00	1.1865E+00	6.1633E+05	5.9112E+06	2.1632E+12	1.9295E+13
54	10600000	1.0983E-03	1.0983E-03	1.0895E+00	1.0895E+00	1.0895E+00	6.0137E+05	5.9112E+06	2.1632E+12	1.9295E+13
55	10800000	1.0495E-03	1.0495E-03	1.0020E+00	1.0020E+00	1.0020E+00	5.8788E+05	5.9112E+06	2.1632E+12	1.9295E+13
56	11000000	1.0020E-03	1.0020E-03	9.3031E+00	9.3031E+00	9.3031E+00	5.7555E+05	5.9112E+06	2.1632E+12	1.9295E+13
57	11200000	9.5935E-04	9.5935E-04	8.6904E+00	8.6904E+00	8.6904E+00	5.6441E+05	5.9112E+06	2.1632E+12	1.9295E+13
58	11400000	9.0646E-04	9.0646E-04	8.168E+00	8.168E+00	8.168E+00	5.5441E+05	5.9112E+06	2.1632E+12	1.9295E+13
59	11600000	8.5441E-04	8.5441E-04	7.6511E+00	7.6511E+00	7.6511E+00	5.4544E+05	5.9112E+06	2.1632E+12	1.9295E+13
60	11800000	8.0337E-04	8.0337E-04	7.144E+00	7.144E+00	7.144E+00	5.3705E+05	5.9112E+06	2.1632E+12	1.9295E+13
61	12000000	7.5337E-04	7.5337E-04	6.6511E+00	6.6511E+00	6.6511E+00	5.2905E+05	5.9112E+06	2.1632E+12	1.9295E+13
62	12200000	7.0441E-04	7.0441E-04	6.1705E+00	6.1705E+00	6.1705E+00	5.2145E+05	5.9112E+06	2.1632E+12	1.9295E+13
63	12400000	6.5641E-04	6.5641E-04	5.7061E+00	5.7061E+00	5.7061E+00	5.1424E+05	5.9112E+06	2.1632E+12	1.9295E+13
64	12600000	6.0935E-04	6.0935E-04	5.2517E+00	5.2517E+00	5.2517E+00	5.0743E+05	5.9112E+06	2.1632E+12	1.9295E+13
65	12800000	5.6324E-04	5.6324E-04	4.8061E+00	4.8061E+00	4.8061E+00	5.0102E+05	5.9112E+06	2.1632E+12	1.9295E+13
66	13000000	5.1805E-04	5.1805E-04	4.3739E+00	4.3739E+00	4.3739E+00	4.9491E+05	5.9112E+06	2.1632E+12	1.9295E+13
67	13200000	4.7378E-04	4.7378E-04	3.9533E+00	3.9533E+00	3.9533E+00	4.8900E+05	5.9112E+06	2.1632E+12	1.9295E+13
68	13400000	4.3037E-04	4.3037E-04	3.5441E+00	3.5441E+00	3.5441E+00	4.8329E+05	5.9112E+06	2.1632E+12	1.9295E+13
69	13600000	3.8788E-04	3.8788E-04	3.1458E+00	3.1458E+00	3.1458E+00	4.7775E+05	5.9112E+06	2.1632E+12	1.9295E+13
70	13800000	3.4624E-04	3.4624E-04	2.7575E+00	2.7575E+00	2.7575E+00	4.7239E+05	5.9112E+06	2.1632E+12	1.9295E+13
71	14000000	3.0544E-04	3.0544E-04	2.3795E+00	2.3795E+00	2.3795E+00	4.6714E+05	5.9112E+06	2.1632E+12	1.9295E+13
72	14200000	2.6544E-04	2.6544E-04	2.0113E+00	2.0113E+00	2.0113E+00	4.6205E+05	5.9112E+06	2.1632E+12	1.9295E+13
73	14400000	2.2624E-04	2.2624E-04	1.6633E+00	1.6633E+00	1.6633E+00	4.5705E+05	5.9112E+06	2.1632E+12	1.9295E+13
74	14600000	1.8788E-04	1.8788E-04	1.3378E+00	1.3378E+00	1.3378E+00	4.5214E+05	5.9112E+06	2.1632E+12	1.9295E+13
75	14800000	1.5037E-04	1.5037E-04	1.0337E+00	1.0337E+00	1.0337E+00	4.4739E+05	5.9112E+06	2.1632E+12	1.9295E+13
76	15000000	1.1378E-04	1.1378E-04	7.4835E+00	7.4835E+00	7.				

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K	ALT	H2O2 + OH	H2O2 + OH	HCL + OH	OH4 + OH	OH + NO2	OH + M4O3	OH + OH	M + M02	CL + M02
1	0.	1.109E+04	1.127E+05	5.727E+04	1.095E+06	2.718E+04	1.948E+04	4.711E+01	9.566E+03	4.286E+02
2	100000.	7.332E+03	7.332E+04	1.432E+04	7.404E+04	9.011E+03	3.785E+03	1.432E+01	1.403E+02	1.403E+02
3	500000.	1.527E+03	1.527E+04	5.023E+03	2.750E+04	3.079E+03	1.833E+03	1.149E+01	2.440E+01	5.969E+01
4	500000.	3.982E+03	4.172E+04	2.513E+03	1.045E+05	5.114E+03	6.793E+03	8.347E+00	1.342E+03	2.459E+01
5	800000.	1.246E+03	1.246E+04	8.282E+02	7.452E+04	6.891E+03	1.830E+03	2.164E+00	4.797E+00	8.788E+00
6	400000.	2.331E+03	2.331E+04	1.835E+03	1.398E+04	5.051E+03	6.058E+02	7.597E+01	1.784E+04	3.098E+00
7	120000.	4.234E+03	4.234E+04	1.578E+03	3.557E+03	4.214E+03	3.548E+03	3.133E+01	6.928E+05	1.689E+06
8	140000.	1.340E+03	1.340E+04	7.441E+02	9.464E+02	4.715E+03	1.591E+01	8.503E+02	1.445E+05	8.454E+01
9	150000.	1.394E+03	1.394E+04	1.735E+02	8.973E+02	9.010E+03	5.335E+01	2.883E+01	2.394E+05	2.852E+06
10	180000.	1.73E+03	1.73E+04	1.553E+03	1.230E+03	2.305E+03	2.267E+02	9.806E+01	7.656E+05	1.038E+01
11	200000.	4.205E+03	4.205E+04	3.438E+02	1.369E+03	7.824E+02	4.567E+02	1.927E+00	1.556E+04	1.821E+01
12	220000.	1.736E+03	1.736E+04	7.706E+02	1.398E+03	7.824E+02	4.567E+02	3.405E+00	3.266E+04	2.700E+01
13	240000.	5.74E+03	5.74E+04	3.220E+02	1.373E+03	4.404E+03	8.344E+02	5.212E+00	7.765E+04	3.957E+01
14	260000.	3.676E+03	3.676E+04	3.411E+02	1.372E+03	9.797E+02	8.767E+02	1.187E+01	1.814E+04	5.853E+01
15	280000.	4.753E+03	4.753E+04	3.317E+02	1.417E+03	1.347E+03	8.765E+02	2.460E+01	4.719E+03	9.296E+01
16	300000.	5.378E+03	5.378E+04	3.688E+02	1.495E+03	1.002E+03	8.239E+02	5.576E+01	1.314E+02	1.613E+02
17	320000.	4.234E+03	4.234E+04	7.747E+02	1.651E+03	1.655E+03	7.574E+02	1.394E+02	3.754E+02	2.819E+02
18	340000.	1.723E+03	1.723E+04	1.445E+02	1.585E+03	1.873E+03	6.544E+02	2.018E+02	1.050E+01	4.521E+02
19	360000.	1.899E+03	1.899E+04	1.422E+03	1.579E+03	1.455E+03	5.106E+02	2.945E+02	2.780E+01	6.162E+02
20	380000.	7.083E+03	7.083E+04	1.373E+03	1.370E+03	6.560E+03	7.351E+02	1.063E+03	7.189E+01	7.361E+02
21	400000.	4.649E+03	4.649E+04	1.533E+03	1.075E+03	2.920E+02	1.644E+02	1.533E+03	1.817E+00	9.029E+02
22	420000.	3.17E+03	3.17E+04	1.777E+03	7.777E+02	1.656E+03	5.849E+01	1.737E+03	4.349E+00	8.042E+02
23	440000.	2.561E+03	2.561E+04	1.235E+03	5.269E+02	3.275E+02	1.546E+01	1.653E+03	9.405E+00	7.361E+02
24	460000.	1.342E+03	1.342E+04	9.427E+02	7.403E+02	8.28E+04	4.070E+00	1.386E+03	1.763E+01	6.114E+02
25	480000.	3.17E+03	3.17E+04	5.657E+02	2.250E+02	2.072E+01	2.49E+01	1.069E+03	2.833E+01	4.675E+02
26	500000.	3.65E+03	3.65E+04	1.433E+02	1.433E+02	6.92E+00	2.723E+01	4.226E+02	4.109E+01	3.501E+02
27	520000.	3.37E+03	3.37E+04	8.771E+02	9.815E+01	2.07E+00	5.09E+02	6.151E+02	5.534E+01	2.526E+02
28	540000.	4.45E+03	4.45E+04	2.35E+02	5.74E+01	6.28E+01	4.64E+02	4.715E+02	7.183E+01	1.836E+02
29	560000.	1.715E+03	1.715E+04	1.679E+02	3.710E+01	1.360E+01	7.846E+01	3.737E+02	9.405E+01	1.342E+02
30	580000.	7.327E+03	7.327E+04	1.359E+02	2.0714E+01	5.804E+02	9.517E+04	2.851E+02	1.144E+02	9.499E+01
31	600000.	4.750E+03	4.750E+04	7.373E+01	1.222E+01	1.765E+02	2.361E+04	2.170E+02	1.484E+01	6.671E+01
32	620000.	2.756E+03	2.756E+04	4.750E+01	5.520E+00	5.082E+02	2.255E+05	1.504E+02	1.650E+02	4.439E+01
33	640000.	3.737E+03	3.737E+04	2.845E+01	3.744E+00	1.788E+02	1.050E+05	9.794E+01	1.744E+02	2.844E+01
34	660000.	4.49E+03	4.49E+04	1.701E+01	1.701E+01	3.779E+01	2.158E+05	8.765E+01	1.933E+02	1.872E+01
35	680000.	2.94E+03	2.94E+04	1.204E+01	9.4750E+01	1.072E+04	5.149E+04	5.695E+01	2.496E+02	1.350E+01
36	700000.	2.342E+03	2.342E+04	5.655E+00	5.575E+01	3.407E+01	1.314E+07	5.654E+01	3.791E+02	1.824E+01
37	720000.	1.10E+03	1.10E+04	5.233E+00	4.747E+01	7.757E+00	2.476E+06	4.267E+01	4.751E+02	6.858E+00
38	740000.	3.77E+03	3.77E+04	3.271E+00	1.434E+01	1.674E+05	4.427E+09	3.273E+01	6.039E+02	4.612E+00
39	760000.	1.543E+03	1.543E+04	1.74E+00	5.393E+02	3.562E+02	5.225E+10	1.807E+01	5.774E+02	2.766E+00
40	780000.	4.870E+03	4.870E+04	9.045E+01	1.905E+02	4.717E+08	4.914E+11	8.347E+00	4.519E+02	1.613E+00
41	800000.	4.97E+03	4.97E+04	3.7561E+01	5.104E+03	6.377E+00	3.745E+12	3.483E+00	3.041E+02	9.565E+01

MIXING RATIOS:

[illegible]
$$\begin{aligned} \text{EN2)} &= -1.32174 \times 10^{-1} \\ \text{EN3)} &= -1.46441 \times 10^{-1} \\ \text{EN4)} &= -2.8527 \times 10^{-1} \\ \text{EN5)} &= -0.12317 \\ \text{EN6)} &= -1.09231 \times 10^{-1} \end{aligned}$$
$$\begin{aligned} \text{ECC14} &= -1.469412\text{E}+09 & \text{ECC14} &= -1.46846\text{E}+06 \\ \text{ECC15} &= -2.46726\text{E}+09 & \text{ECC15} &= -9.21821\text{E}+14 \end{aligned}$$

09/07/77

VERSION 6.0 (770214)

CHLDRIFE MODEL TITAN PROGRAM

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K	ALT	MR 00	MR 11	MR 12	MR 30	MR 40	MR 50
1	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	3.1343E+09	2.3378E+14
2	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	3.1343E+09	1.2237E+14
3	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	2.1429E+09	5.8059E+09
4	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.7774E+09	3.0108E+09
5	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.4088E+09	1.7905E+09
6	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.1272E+09	1.1139E+09
7	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	8.9614E+08	1.0404E+09
8	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	7.5377E+08	1.0171E+09
9	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	4.9712E+08	1.1232E+09
10	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	2.8347E+08	1.6969E+09
11	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.5517E+08	1.8273E+09
12	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	7.7111E+07	1.7325E+09
13	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	3.2455E+07	1.5525E+09
14	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.1111E+07	1.2796E+09
15	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	2.7488E+06	1.0327E+09
16	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	4.7650E+05	6.0925E+08
17	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	5.7115E+04	4.2268E+08
18	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	4.3737E+03	4.7257E+08
19	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	3.5691E+02	3.5691E+08
20	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	2.7451E+01	2.6911E+08
21	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.8083E+00	2.0320E+08
22	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.2111E+01	1.5392E+08
23	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.0515E+02	1.1703E+08
24	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.0948E+03	8.9392E+07
25	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.2313E+04	4.9909E+07
26	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.9077E+05	3.3076E+07
27	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	3.4402E+06	4.2249E+07
28	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	6.3278E+07	3.7472E+07
29	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.3072E+08	2.6371E+07
30	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	4.0575E+09	2.0685E+07
31	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.1456E+08	1.6232E+07
32	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	7.6146E+09	1.2806E+07
33	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.2681E+09	1.9034E+07
34	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	4.7713E+10	7.8049E+05
35	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.9372E+10	6.0486E+05
36	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	3.3547E+11	4.6035E+05
37	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	3.3418E+11	3.4979E+05
38	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	1.8411E+11	2.6176E+05
39	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	0.4731E+12	1.9437E+05
40	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	2.4935E+12	4.4272E+05
41	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	3.1202E+12	1.0352E+05
42	200000	2.5797E+09	1.3701E+09	2.8335E+09	3.6165E+10	2.2450E+12	1.0352E+05

K	ALT	NOJ	NOY	CH4
1	20000	0.0275+12	4.73-52+11	3.64-55+12
2	20000	0.0167+12	2.17-72+10	3.10-52+12
3	20000	0.011+12	2.04+12+0	2.77+55+13
4	20000	0.0075+12	4.37-62+09	1.3778+12
5	20000	0.0051+12	2.0490+0	1.5152+12
6	20000	0.0035+12	1.6789+09	1.2752+12
7	20000	0.0025+12	2.2722+09	1.7443+12
8	20000	0.0018+12	2.3603+0	0.6646+12
9	20000	0.0013+12	2.5453+09	5.0735+12
10	20000	0.0009+12	2.6782+13	3.7755+12
11	20000	0.0006+12	2.2102+0	2.4427+12
12	20000	0.0004+12	2.1705+11	1.5923+12
13	20000	0.0003+12	1.1772+11	1.6210+12
14	20000	0.0002+12	1.0738+11	6.4373+11
15	20000	0.0001+12	0.3303+09	4.7765+11
16	20000	0.0001+12	7.2975+09	3.4975+11
17	20000	0.0001+12	5.7946+09	1.5732+11
18	20000	0.0001+12	0.7305+09	0.0055+11
19	20000	0.0001+12	7.3143+09	5.2142+10
20	20000	0.0001+12	2.3132+09	7.0278+10
21	20000	0.0001+12	1.3722+09	1.7745+10
22	20000	0.0001+12	0.7305+09	1.5935+10
23	20000	0.0001+12	0.7312+09	6.5642+09
24	20000	0.0001+12	0.7705+09	1.2510+09
25	20000	0.0001+12	3.7115+08	2.8812+09
26	20000	0.0001+12	2.3903+08	2.0075+09
27	20000	0.0001+12	0.8806+08	1.50-52+09
28	20000	0.0001+12	2.1375+08	1.1556+09
29	20000	0.0001+12	1.3509+08	6.0000+08
30	20000	0.0001+12	1.1325+08	5.5619+08
31	20000	0.0001+12	0.7305+08	5.3295+08
32	20000	0.0001+12	0.7305+08	4.1750+08
33	20000	0.0001+12	0.7305+08	7.0257+07
34	20000	0.0001+12	0.7305+08	2.5735+07
35	20000	0.0001+12	1.3172+07	1.95745+09
36	20000	0.0001+12	0.7305+08	1.45832+09
37	20000	0.0001+12	0.7305+08	4.12585+09
38	20000	0.0001+12	0.7305+08	8.45245+07
39	20000	0.0001+12	0.7305+08	6.2775+07
40	20000	0.0001+12	1.6501+08	4.61512+07
41	20000	0.0001+12	0.7305+08	5.23362+07

NORMAL JOY END.

CASE 2

LAST ITERATION = 7

ALT	CJ02	CJ03	CJ062	CJ063	CJ067	DO3INT	Q4INT	PREVOM	
200000	3.585E-12	2.234E-14	3.135E-10	4.048E-23	3.537E-06	7.216E-11	8.417E-18	2.134E-25	2.676E-06
200001	5.179E-23	2.332E-24	1.539E-20	5.612E-25	1.413E-05	5.025E-11	9.204E-18	1.743E-25	3.077E-06
200002	3.124E-06	3.028E-04	1.135E-21	3.748E-22	1.214E-05	4.389E-11	9.175E-18	1.467E-25	2.817E-06
200003	5.747E-24	7.115E-08	7.395E-24	7.672E-20	1.333E-15	4.372E-11	9.083E-16	1.664E-27	2.305E-06
200004	5.717E-22	2.235E-24	2.284E-19	1.130E-17	1.453E-15	4.103E-11	7.398E-18	4.253E-24	1.458E-06
1000000	3.449E-20	3.735E-24	7.773E-17	9.730E-11	1.535E-05	4.403E-11	7.912E-18	6.292E-24	8.981E-06
1200000	7.185E-11	7.214E-14	1.363E-05	4.414E-14	1.583E-11	5.672E-11	7.810E-18	4.727E-24	5.733E-05
1400000	4.891E-17	7.215E-14	1.251E-17	1.415E-12	4.537E-05	7.105E-11	7.683E-18	3.474E-24	7.071E-05
1600000	4.893E-16	3.241E-12	2.324E-12	1.324E-11	1.631E-09	1.375E-12	7.475E-18	2.431E-24	4.252E-05
1800000	3.465E-24	7.242E-14	1.115E-14	2.091E-10	7.735E-05	7.404E-12	7.037E-18	4.747E-24	7.033E-05
2000000	3.206E-14	3.245E-14	1.132E-10	2.242E-09	1.348E-05	4.056E-12	5.323E-18	1.294E-24	9.453E-06
2200000	2.791E-13	3.239E-14	4.121E-06	2.876E-03	2.306E-09	4.607E-12	5.451E-16	2.217E-23	1.148E-06
2400000	1.072E-12	3.532E-14	3.32E-19	7.635E-05	3.116E-05	4.594E-12	4.485E-18	6.732E-23	1.525E-06
2600000	3.497E-12	3.539E-14	1.471E-08	1.211E-07	4.511E-05	4.871E-12	3.499E-18	4.970E-23	2.090E-06
2800000	4.733E-12	3.739E-14	3.813E-08	3.231E-07	6.432E-05	3.305E-12	2.576E-18	3.639E-23	2.393E-06
3000000	2.629E-11	4.233E-14	3.945E-07	7.345E-07	1.103E-04	7.495E-12	1.790E-18	2.737E-23	4.416E-06
3200000	4.241E-11	4.233E-14	1.545E-17	1.433E-06	1.456E-04	2.612E-12	1.180E-18	2.060E-23	6.610E-06
3400000	3.196E-11	6.115E-14	4.907E-07	2.242E-06	2.907E-04	4.717E-12	4.241E-17	1.252E-23	9.742E-06
3600000	1.127E-10	7.026E-14	3.135E-07	2.804E-06	4.822E-04	1.123E-12	4.524E-17	1.175E-23	1.380E-07
3800000	1.125E-10	1.113E-07	3.101E-07	7.395E-04	7.395E-04	4.674E-11	7.734E-17	8.966E-22	4.845E-07
4000000	2.610E-10	1.610E-03	4.404E-07	4.404E-06	1.288E-03	3.806E-11	1.680E-17	6.858E-22	2.225E-07
4200000	7.144E-10	2.212E-07	4.973E-07	4.937E-06	1.895E-03	2.315E-11	1.061E-17	5.279E-22	2.755E-07
4400000	3.648E-10	2.847E-03	5.342E-07	4.927E-06	4.539E-03	4.906E-11	5.859E-16	4.443E-22	2.271E-07
4600000	3.125E-10	3.745E-07	5.562E-07	5.562E-06	7.477E-03	3.087E-10	4.511E-16	3.173E-22	2.054E-07
4800000	3.241E-10	3.741E-03	3.333E-07	3.366E-07	3.366E-07	5.823E-10	7.320E-16	2.475E-22	1.797E-07
5000000	4.119E-10	4.119E-03	3.253E-07	5.573E-06	7.793E-07	7.876E-11	2.150E-16	1.914E-22	1.564E-07
5200000	5.170E-10	4.119E-03	4.566E-07	5.573E-06	4.923E-03	2.594E-11	1.511E-22	1.351E-22	1.351E-22
5400000	5.170E-10	4.119E-03	4.566E-07	5.573E-06	4.923E-03	2.594E-11	1.511E-22	1.351E-22	1.351E-22
5600000	5.170E-10	4.119E-03	4.566E-07	5.573E-06	4.923E-03	2.594E-11	1.511E-22	1.351E-22	1.351E-22
5800000	5.170E-10	4.119E-03	4.566E-07	5.573E-06	4.923E-03	2.594E-11	1.511E-22	1.351E-22	1.351E-22
6000000	5.170E-10	4.119E-03	4.566E-07	5.573E-06	4.923E-03	2.594E-11	1.511E-22	1.351E-22	1.351E-22
6200000	5.170E-10	4.119E-03	4.566E-07	5.573E-06	4.923E-03	2.594E-11	1.511E-22	1.351E-22	1.351E-22
6400000	5.170E-10	4.119E-03	4.566E-07	5.573E-06	4.923E-03	2.594E-11	1.511E-22	1.351E-22	1.351E-22
6600000	5.170E-10	4.119E-03	4.566E-07	5.573E-06	4.923E-03	2.594E-11	1.511E-22	1.351E-22	1.351E-22
6800000	5.170E-10	4.119E-03	4.566E-07	5.573E-06	4.923E-03	2.594E-11	1.511E-22	1.351E-22	1.351E-22
7000000	5.170E-10	4.119E-03	4.566E-07	5.573E-06	4.923E-03	2.594E-11	1.511E-22	1.351E-22	1.351E-22
7200000	5.170E-10	4.119E-03	4.566E-07	5.573E-06	4.923E-03	2.594E-11	1.511E-22	1.351E-22	1.351E-22
7400000	5.170E-10	4.119E-03	4.566E-07	5.573E-06	4.923E-03	2.594E-11	1.511E-22	1.351E-22	1.351E-22
7600000	5.170E-10	4.119E-03	4.566E-07	5.573E-06	4.923E-03	2.594E-11	1.511E-22	1.351E-22	1.351E-22
7800000	5.170E-10	4.119E-03	4.566E-07	5.573E-06	4.923E-03	2.594E-11	1.511E-22	1.351E-22	1.351E-22
8000000	5.170E-10	4.119E-03	4.566E-07	5.573E-06	4.923E-03	2.594E-11	1.511E-22	1.351E-22	1.351E-22

LAST ITERATION = 7

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AST LTERATION + 1

131

LAST ITERATION + 1

ALT	CJCL03	CJN01	CJN03	CJN02	CJN05	CJCL04	CJCL05L
200001	3.210E-05	1.641E-04	1.448E-07	1.731E-06	1.245E-05	2.242E-27	1.216E-30
200002	3.575E-05	2.197E-06	2.017E-07	1.256E-06	6.012E-05	7.709E-24	1.339E-27
200003	3.616E-05	1.251E-03	3.185E-07	2.641E-06	2.73E-05	1.444E-21	1.302E-24
300001	5.195E-05	3.041E-04	5.713E-07	1.004E-06	6.453E-05	1.826E-19	4.024E-22
400001	6.652E-05	4.131E-04	7.372E-07	2.346E-06	8.523E-05	3.702E-17	7.453E-20
100000	5.024E-05	3.831E-07	3.721E-07	7.341E-06	2.525E-05	7.044E-15	7.365E-18
120001	5.025E-05	1.821E-05	3.835E-07	1.296E-06	6.632E-05	8.816E-14	7.863E-16
140001	5.059E-05	6.225E-04	1.035E-07	3.118E-06	2.713E-05	2.894E-10	1.343E-14
150001	5.072E-05	1.246E-02	1.371E-07	3.117E-06	2.711E-05	6.226E-11	2.904E-13
180001	5.196E-05	1.370E-01	7.371E-07	3.115E-06	2.703E-05	5.181E-11	7.267E-12
200000	5.091E-05	9.137E-01	7.213E-07	2.740E-06	2.735E-05	7.350E-03	2.730E-11
220001	5.144E-05	4.570E-01	7.143E-07	7.215E-06	2.737E-05	1.595E-06	1.497E-10
240001	7.190E-05	1.790E-01	7.033E-07	3.784E-06	2.837E-05	6.030E-08	4.764E-10
250001	7.402E-05	5.630E-01	1.323E-06	3.117E-06	2.901E-05	1.929E-07	1.587E-09
260001	7.988E-05	1.504E-01	6.213E-06	3.284E-06	3.245E-05	8.256E-07	1.348E-09
300001	9.001E-05	3.268E-02	6.792E-06	5.113E-06	3.895E-05	1.21E-06	9.481E-09
320001	1.072E-04	5.945E-01	1.113E-05	7.107E-06	4.243E-05	2.376E-06	1.746E-08
340001	1.248E-04	9.243E-01	1.371E-05	9.377E-06	6.576E-05	7.044E-06	2.639E-08
360001	1.249E-04	1.284E-02	2.333E-05	1.373E-05	6.923E-05	5.938E-06	3.532E-08
380001	3.675E-04	1.611E-01	7.319E-05	1.753E-05	1.175E-04	7.905E-06	1.445E-08
400001	3.684E-04	1.372E-01	3.726E-05	2.433E-05	1.492E-04	9.496E-06	3.143E-08
420001	3.198E-04	2.006E-01	1.313E-05	3.222E-05	1.898E-04	1.371E-05	5.671E-08
440001	4.256E-04	2.204E-02	1.835E-05	4.561E-05	2.131E-04	1.564E-05	5.255E-08
450001	4.505E-04	2.367E-02	1.933E-05	4.094E-05	2.737E-04	1.227E-05	6.500E-08
460001	4.655E-04	2.469E-02	1.935E-05	4.384E-05	2.304E-04	1.227E-05	6.883E-08
500001	3.107E-04	2.535E-02	1.318E-05	4.615E-05	2.641E-04	1.510E-05	7.381E-08
520001	3.095E-04	2.644E-02	2.231E-05	4.848E-05	2.737E-04	1.555E-05	8.453E-08
540001	3.172E-04	2.774E-02	3.372E-05	4.751E-05	2.349E-04	1.388E-05	6.974E-08
560001	3.532E-04	2.342E-02	4.443E-05	5.056E-05	2.844E-04	1.423E-05	1.014E-07
580001	3.806E-04	2.961E-02	5.347E-05	5.113E-05	2.895E-04	1.454E-05	1.151E-07
600001	3.666E-04	3.403E-02	5.546E-05	5.137E-05	2.322E-04	1.493E-05	1.341E-07
620001	3.693E-04	3.204E-02	7.142E-05	5.244E-05	4.730E-04	1.527E-05	1.457E-07
640001	3.722E-04	3.167E-02	7.345E-05	5.244E-05	4.054E-04	1.560E-05	1.614E-07
660001	3.750E-04	3.489E-02	5.732E-05	5.372E-05	2.905E-04	1.589E-05	1.773E-07
680001	3.767E-04	3.623E-02	5.812E-05	5.385E-05	2.371E-04	1.615E-05	1.945E-07
700001	3.780E-04	3.075E-02	5.770E-05	5.359E-05	2.976E-04	1.637E-05	2.143E-07
720001	3.790E-04	4.064E-02	5.853E-05	5.378E-05	2.380E-04	1.655E-05	2.322E-07
740001	3.799E-04	4.476E-02	5.273E-05	5.336E-05	2.392E-04	1.669E-05	2.625E-07
760001	3.802E-04	4.324E-02	6.244E-05	5.412E-05	2.044E-04	1.680E-05	2.887E-07
780001	3.807E-04	5.038E-02	5.272E-05	5.427E-05	2.935E-04	1.689E-05	3.137E-07
800001	3.815E-04	6.071E-02	5.334E-05	5.444E-05	2.933E-04	1.696E-05	3.364E-07

<	ALT	H	74	402	M202	0	73	03INT	0(0)
1	0.	3.2455E+01	2.7173E+06	9.5212E+08	1.6860E+11	2.7378E+13	7.2253E+11	8.4154E+10	9.8849E+03
2	30000.	3.2419E+01	7.2177E+06	9.1453E+08	1.1874E+11	2.9089E+13	5.0225E+11	8.2829E+10	9.9822E+03
3	30000.	3.1675E+01	2.8172E+06	7.5105E+08	7.5654E+10	3.8470E+03	4.8349E+11	8.1779E+10	1.2335E+02
4	30000.	3.1675E+01	2.8172E+06	5.0347E+08	4.4437E+10	4.0241E+03	4.3477E+11	8.4413E+10	1.4768E+02
5	30000.	3.1675E+01	2.8172E+06	4.5399E+06	1.9327E+10	6.3348E+03	4.0992E+11	7.9967E+10	1.7991E+02
6	30000.	3.1675E+01	2.8172E+06	3.1317E+06	1.7439E+09	9.7083E+03	4.4830E+11	7.9108E+10	2.5141E+02
7	120000.	3.2942E+02	5.7377E+06	1.5846E+08	2.7340E+09	1.7745E+04	5.6737E+11	7.8097E+10	4.0431E+02
8	120000.	3.2942E+02	5.7377E+06	8.5578E+07	7.8177E+08	2.5100E+04	7.1137E+11	7.6814E+10	5.8561E+02
9	120000.	3.2942E+02	5.7377E+06	7.8177E+07	0.6107E+08	9.1374E+04	1.3616E+12	7.4741E+10	1.6370E+01
10	120000.	3.2942E+02	5.7377E+06	7.8177E+07	9.2465E+08	1.5586E+05	3.0449E+12	7.0334E+10	5.5891E+01
11	200000.	1.2645E+01	9.3312E+05	9.4705E+07	1.2450E+09	1.2970E+06	4.0499E+12	6.1240E+10	1.1903E+00
12	200000.	1.2645E+01	9.3312E+05	1.3621E+08	1.5888E+09	2.0777E+03	4.6807E+12	5.4525E+10	2.3783E+00
13	200000.	3.4680E+01	1.5745E+06	1.1111E+08	1.8353E+09	6.7049E+06	4.9890E+12	4.9860E+10	4.7421E+00
14	200000.	2.8227E+01	2.8383E+06	1.2485E+08	1.8620E+09	1.3929E+07	4.8228E+12	3.5006E+10	9.3119E+00
15	200000.	2.8377E+00	7.3317E+06	1.2485E+08	1.8620E+09	7.6114E+07	4.9567E+12	2.5766E+10	1.7560E+01
16	300000.	6.1022E+01	1.1502E+07	1.1505E+08	1.5893E+09	4.7446E+07	3.3637E+12	1.7933E+10	3.0728E+01
17	300000.	2.1587E+01	5.3135E+06	3.9503E+07	6.4177E+08	7.9079E+07	2.5124E+12	1.1794E+10	5.1238E+01
18	300000.	3.3714E+01	2.4424E+06	7.8373E+07	2.6863E+08	1.2722E+08	1.7303E+12	7.4413E+10	7.7858E+01
19	300000.	2.7490E+02	1.3313E+07	9.7814E+07	3.0763E+08	1.0841E+08	4.1216E+12	4.5194E+10	1.0885E+02
20	300000.	2.0353E+03	1.3422E+07	4.2367E+07	4.7654E+07	3.0799E+08	0.0605E+11	2.7711E+10	1.4448E+02
21	400000.	3.3375E+07	2.5215E+07	3.2583E+07	2.0775E+07	4.7309E+09	3.8924E+11	1.6702E+10	1.8173E+02
22	400000.	3.5212E+03	2.3455E+07	2.6833E+07	1.3453E+07	7.1477E+08	2.3424E+11	1.1607E+10	2.1357E+02
23	400000.	2.7353E+01	6.0715E+07	2.8633E+07	8.0515E+06	1.0147E+09	1.4343E+11	6.8566E+10	2.3331E+02
24	400000.	3.0685E+01	4.0922E+07	1.8466E+07	5.5603E+06	1.3322E+09	9.0410E+10	4.5102E+10	2.3603E+02
25	400000.	3.2665E+01	4.7938E+07	1.6525E+07	3.8774E+06	1.6893E+09	5.3219E+10	3.0200E+10	2.4405E+02
26	500000.	1.9485E+03	1.5340E+07	1.3472E+07	2.2600E+06	1.2973E+03	3.3749E+11	2.0503E+10	2.0918E+02
27	500000.	2.4316E+03	1.3402E+07	1.1019E+07	1.9405E+06	2.8780E+09	2.5319E+10	1.4036E+10	1.8921E+02
28	400000.	3.1015E+03	1.7235E+07	1.1522E+07	1.4008E+06	2.5577E+09	1.7453E+10	3.5482E+10	7.7181E+02
29	500000.	5.4210E+05	1.3545E+07	0.9308E+06	1.5365E+06	2.7707E+03	1.7099E+10	6.6433E+10	1.5017E+02
30	500000.	7.0216E+09	9.1524E+06	7.8077E+06	1.0300E+05	2.9030E+09	8.1666E+09	4.6183E+10	1.3078E+02
31	600000.	1.1391E+05	7.3384E+06	5.6505E+06	5.0021E+05	3.1974E+09	5.5340E+09	7.2518E+10	1.1311E+02
32	600000.	1.5950E+05	9.5115E+06	5.3802E+06	3.4634E+05	3.8328E+09	4.0316E+09	2.2962E+10	1.0518E+02
33	600000.	2.7705E+06	5.1230E+06	4.1026E+06	1.8064E+05	4.6745E+09	3.1316E+09	1.5778E+10	1.0310E+02
34	600000.	2.3842E+06	5.1230E+06	4.1026E+06	1.8064E+05	3.5302E+09	1.8319E+09	1.0795E+10	7.7656E+01
35	500000.	4.1051E+09	7.3375E+06	7.4747E+06	1.1002E+06	4.2707E+09	1.2344E+09	7.6496E+10	6.9144E+01
36	700000.	5.1284E+05	3.9023E+06	2.9461E+06	7.9534E+04	4.6300E+09	8.8224E+08	5.4694E+10	6.1455E+01
37	700000.	3.7327E+06	5.4732E+06	4.5343E+06	5.2387E+04	5.4211E+09	6.1333E+08	3.9698E+10	5.5078E+01
38	700000.	2.0133E+07	7.0355E+06	2.1681E+06	3.6815E+04	5.7145E+09	4.2066E+08	2.9371E+10	4.9553E+01
39	700000.	1.9940E+07	2.2415E+06	1.4524E+06	1.9305E+04	7.8041E+09	3.7454E+08	2.1859E+10	5.1446E+01
40	700000.	2.6478E+07	1.5465E+06	8.5647E+06	4.2002E+03	1.0103E+10	2.7031E+08	1.5850E+10	5.6106E+01
41	800000.	3.2959E+07	1.7018E+06	4.6400E+06	1.2361E+07	1.7045E+10	2.1912E+08	1.0956E+10	6.1352E+01

K	ALY	N0	N04	UN03	N03	N205	NOX
1	..	5.4983E+14	2.1562E+09	3.9649E+14	4.4290E+06	7.1223E+08	4.4917E+14
2	366637	7.6672E+14	3.2251E+09	1.0202E+15	1.1456E+06	5.1678E+07	2.1740E+14
3	+0000	5.7721E+14	4.1543E+09	7.0513E+14	2.7737E+05	4.5408E+06	9.7841E+09
4	506690	2.8455E+14	2.1005E+09	2.2112E+14	3.3526E+14	6.7463E+05	4.8208E+03
5	300000	7.7222E+14	1.2101E+09	2.3655E+09	3.1012E+14	1.3307E+05	2.8546E+09
6	100000	7.8131E+14	1.2262E+09	1.4200E+14	1.4200E+14	5.0558E+04	1.9528E+03
7	120000	5.6575E+14	1.3505E+09	1.5475E+09	2.2944E+14	2.8151E+04	2.2895E+09
8	400000	1.4107E+14	1.3226E+09	1.5422E+14	2.1827E+14	2.0132E+04	2.7273E+04
9	1500000	1.2767E+14	7.7495E+08	3.6755E+14	7.2022E+14	2.1128E+05	4.7639E+09
10	400000	3.1125E+14	5.8522E+08	8.3853E+14	1.2857E+15	2.7730E+05	9.9028E+09
11	200000	6.9433E+14	3.1265E+09	1.2125E+15	2.3507E+15	7.4753E+06	1.2151E+14
12	200000	6.5113E+14	1.5723E+09	1.0031E+15	5.4522E+14	1.8624E+07	1.2398E+14
13	720000	7.3707E+14	2.2262E+09	3.8024E+14	9.1226E+15	3.3777E+17	1.1630E+14
14	200000	3.7452E+14	2.0362E+09	6.5645E+14	1.4044E+16	7.3484E+07	1.6230E+14
15	240000	4.2402E+14	1.2567E+09	4.2175E+14	2.2178E+14	1.1794E+08	8.6833E+09
16	300000	1.6203E+14	2.3042E+14	2.3042E+14	3.2365E+16	8.7555E+07	7.0840E+09
17	720000	1.5345E+14	4.1133E+09	1.3307E+14	1.7805E+16	7.7092E+07	5.5949E+09
18	300000	1.7502E+14	1.7713E+09	7.3562E+14	1.1432E+16	1.1812E+07	4.3485E+09
19	350000	1.3135E+14	1.7112E+09	3.5742E+14	5.2934E+16	3.7670E+09	7.2880E+09
20	300000	6.1922E+14	6.1922E+09	1.6422E+14	6.7842E+16	5.2752E+05	2.4305E+03
21	400000	1.2077E+14	5.3867E+08	5.4545E+14	1.3379E+16	7.4166E+04	1.7466E+09
22	200000	1.0031E+14	6.0372E+08	6.0445E+14	3.3414E+14	7.8635E+03	1.3186E+09
23	400000	8.6525E+14	3.1123E+09	2.8135E+16	1.2338E+14	7.7630E+02	9.6810E+08
24	450000	6.0427E+14	1.2272E+09	1.3229E+15	3.8439E+17	7.3327E+03	7.6392E+03
25	430000	7.9167E+14	1.5045E+09	7.8426E+15	1.7325E+13	9.9394E+00	5.1466E+08
26	900000	3.7235E+14	2.7342E+09	1.0242E+17	3.2640E+12	5.4445E+01	3.7956E+08
27	500000	2.7775E+14	3.3013E+09	3.1510E+14	9.5195E+11	5.9544E+02	2.7948E+09
28	600000	2.5812E+14	1.2583E+09	9.5592E+14	2.2221E+14	5.2245E+03	2.6432E+03
29	500000	1.8497E+14	3.4752E+09	4.0720E+17	5.2303E+10	4.3465E+04	1.5106E+08
30	500000	4.0415E+14	2.2435E+09	8.4305E+12	1.3557E+14	3.4803E+15	1.6848E+08
31	500000	7.8491E+17	3.4472E+04	2.6150E+11	3.1895E+11	2.4573E+06	7.8550E+07
32	500000	5.6542E+17	3.7342E+04	7.3750E+11	7.0751E+10	1.8602E+07	5.6272E+07
33	640000	3.3775E+17	1.1213E+04	4.9352E+11	1.5848E+12	1.6075E+18	3.0754E+07
34	500000	2.7482E+17	2.4372E+17	8.2802E+10	2.4000E+07	5.5875E+10	2.7503E+07
35	500000	1.3670E+17	1.9515E+13	1.5962E+10	4.3477E+14	2.7757E+11	4.8688E+07
36	700000	1.2597E+17	5.2304E+17	4.2406E+14	5.8649E+17	1.1144E+12	1.2278E+07
37	720000	7.8373E+14	1.1772E+12	4.475E+01	1.0150E+15	4.0177E+14	1.8617E+05
38	700000	4.8512E+16	3.2115E+01	2.4004E+12	1.3687E+14	4.2134E+15	4.8668E+06
39	750000	2.8937E+16	1.7505E+11	4.0175E+07	1.9704E+17	3.6087E+17	2.9005E+05
40	700000	1.5335E+16	1.5652E+03	6.4712E+04	2.5248E+18	9.0854E+19	1.6564E+06
41	800000	8.5750E+16	1.1173E+10	9.3711E+05	2.0793E+19	1.8055E+20	9.0771E+05

K	ALT	CL	CLC	HPL	CLN03	OCLX			
1	9.7579E+03	4.7473E-16	5.9387E+06	1.4032E-12	2.3202E+00	0.549E-10	1.0836E+09	4.4943E-11	1.1000E-09
2	9.1112E+03	7.8352E-16	7.5681E+06	1.6361E-12	1.2383E+00	5.8826E+00	1.9895E+08	9.4515E-12	5.7000E-10
3	5.4610E+03	7.3077E-16	2.6714E+06	1.5814E-12	5.0729E+00	3.5742E-10	5.0732E+07	3.0728E-12	3.1000E-10
4	2.4412E+03	2.5481E-16	1.0277E+06	1.2072E-12	3.2715E+00	1.2777E-10	1.2777E+00	1.2507E-12	1.7000E-10
5	8.0000E+03	2.0945E+03	1.0314E+06	9.0344E-14	1.9856E+00	1.8250E-10	5.7476E+05	5.2027E-13	1.1000E-10
6	1.0000E+03	1.2438E+03	6.7185E+05	7.7146E-14	1.2264E+00	1.4616E-10	2.8483E+06	3.2158E-13	8.4100E-11
7	1210000	1.7821E-16	5.1305E+05	7.4270E-14	1.2036E+00	1.7411E-10	2.9188E+06	4.2222E-13	1.1000E-10
8	1.0000E+03	1.6340E-16	6.7498E+05	7.6246E-14	1.1718E+00	1.9757E-10	5.5725E+06	4.3373E-13	1.1000E-10
9	1500000	7.5021E+03	1.2014E+06	7.0942E-13	1.2374E+00	7.0942E-10	1.9873E+07	3.6248E-12	2.4000E-10
10	8.8000E+03	2.6735E-16	1.1074E+07	3.0412E-12	1.5375E+00	5.5567E-10	1.7264E+08	6.1149E-11	6.0000E-10
11	2000000	1.2258E+04	6.1205E+05	4.747E-11	1.4709E+00	7.3508E-10	3.9502E+09	1.9251E-10	9.5000E-09
12	2.4000E+03	1.5408E+04	1.1833E-14	4.8547E+07	1.1711E+00	8.1484E-10	5.3873E+08	3.7700E-10	1.3000E-09
13	2.0100E+03	2.2677E+04	1.1374E-14	5.3315E+07	6.1152E-11	8.6765E+08	3.3698E-10	5.0944E-10	1.6000E-09
14	2.6000E+03	3.0827E+04	1.1401E-14	6.5586E+07	8.9491E-11	6.3322E+08	8.5335E-10	5.6845E+08	1.8000E-09
15	2.8000E+03	4.5722E+04	1.0394E-14	9.9305E+07	1.7757E-10	4.7950E+08	8.8265E-10	4.6096E+08	2.0000E-09
16	3.0000E+03	7.5588E+04	1.0403E-13	7.7033E+07	1.0401E-10	3.4440E+08	9.5825E-10	3.3016E+08	2.2000E-09
17	3.2000E+03	1.3168E+05	1.0394E-13	3.1912E+07	3.447E-10	3.2156E+08	1.1559E-09	2.0219E+08	2.3000E-09
18	3.4000E+03	2.3473E+05	1.0422E-12	1.0474E+08	4.8430E-10	2.5415E+08	1.1722E-09	9.8280E+07	2.3000E-09
19	3.6000E+03	3.9577E+05	2.0513E-12	4.7915E+08	6.7777E-10	4.9915E+08	1.2457E-09	3.7060E+07	2.4000E-09
20	3.8000E+03	5.7232E+05	5.1533E-12	9.4304E+08	7.8289E-10	5.0320E+08	1.2884E-09	1.0554E+07	2.4000E-09
21	4.0000E+03	8.5030E+05	7.3055E-12	6.9370E+07	7.7537E-10	1.2317E+09	1.3679E-09	2.8808E+06	2.4000E-09
22	4.2000E+03	1.3415E+06	1.6522E-11	4.7155E+07	6.5277E-10	1.0209E+09	1.5048E-09	4.2026E+05	2.4000E-09
23	4.4000E+03	1.1075E+06	2.1457E-11	2.5475E+07	4.9225E-10	8.6255E+07	1.5715E-09	6.0881E+04	2.4000E-09
24	4.6000E+03	1.6635E+06	2.7145E-11	1.3157E+07	3.3433E-10	7.4345E+07	1.8265E-09	8.5071E+03	2.4000E-09
25	4.8000E+03	2.5017E+06	3.1613E-11	6.5574E+06	2.1539E-10	5.8895E+07	1.4051E-09	1.2224E+03	2.4000E-09
26	5.0000E+03	4.2476E+06	3.5813E-11	7.3660E+06	1.4451E-10	4.7322E+07	2.0123E+09	1.9867E+02	2.4000E-09
27	5.2000E+03	7.0105E+06	3.7363E-11	7.9615E+06	9.1205E-11	3.0709E+07	2.0596E-09	7.3350E+01	2.4000E-09
28	5.4000E+03	1.1334E+07	4.0345E-11	9.0222E+06	6.4138E-11	3.2714E+07	2.1884E-09	6.1756E+00	2.4000E-09
29	5.6000E+03	1.8175E+07	4.2737E-11	1.6303E+06	4.7108E-11	4.4182E+07	2.1668E-09	1.1164E+00	2.4000E-09
30	5.8000E+03	2.8236E+07	4.5191E-11	2.4709E+06	2.6425E-11	1.0235E+07	2.1191E-09	1.9820E-01	2.4000E-09
31	6.0000E+03	4.2712E+07	4.7730E-11	1.2304E+06	1.7177E-11	1.1937E+07	2.1267E-09	3.5067E-02	2.4000E-09
32	6.2000E+03	6.6717E+07	4.7705E-11	6.8335E+06	1.1752E-11	1.2008E+07	2.1307E-09	6.7217E-03	2.4000E-09
33	6.4000E+03	1.0211E+08	4.9453E-11	7.5474E+06	8.7305E-12	9.4149E+06	2.1320E-09	1.2593E-03	2.4000E-09
34	6.6000E+03	1.5205E+08	5.2222E-11	1.1768E+06	5.1557E-12	7.3777E+06	2.1500E-09	2.0312E+00	2.4000E-09
35	6.8000E+03	2.2015E+08	5.4135E-11	9.1327E+06	3.4795E-12	5.0838E+06	2.1351E-09	3.3777E-05	2.4000E-09
36	7.0000E+03	3.2642E+08	5.7133E-11	4.4410E+06	2.2474E-12	4.2040E+06	2.1343E-09	4.9573E-06	2.4000E-09
37	7.2000E+03	4.8202E+08	6.0133E-11	2.0205E+06	1.4437E-12	3.2773E+06	2.1324E-09	7.0138E-07	2.4000E-09
38	7.4000E+03	6.9606E+08	6.3605E-11	1.1335E+06	9.4036E-13	2.4519E+06	2.1294E-09	9.2489E-08	2.4000E-09
39	7.6000E+03	1.0333E+09	7.1272E-11	5.8101E+06	5.8128E-13	1.8115E+06	2.1178E-09	1.2767E-08	2.4000E-09
40	7.8000E+03	1.5205E+09	7.4666E-11	3.4414E+06	3.4632E-13	1.3146E+06	2.0929E-09	1.7916E-09	2.4000E-09
41	8.0000E+03	2.2015E+09	7.8193E-11	2.1307E+06	4.8193E-13	9.3117E+05	2.0748E-09	2.5122E-10	2.4000E-09

[illegible]

INTEGRATED LOSS F73 07046

1006E+11	5.9520E+11	A 5518E+10	3.0097E+12	3.3665E+12	3.0006E+12	2.4102E+12	1.9774E+13
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K	ALT	H2O + MV	4-7 + OLR	CH4 + O1D	MNO3 + MV	CO + OH	NO + M02	JH2O2+H2O2	CL + CH4
1	0.	1.4189E+01	1.5143E+06	5.9592E+01	5.0007E+03	7.3548E+05	2.7354E+05	4.4862E+05	4.1093E+04
2	0.00000	1.0000E+01	1.0000E+06	8.2324E+01	5.1564E+03	8.6989E+05	2.4346E+05	5.3571E+05	2.3793E+04
3	0.00000	1.0000E+01	6.4119E+05	8.3370E+01	2.6993E+03	5.0007E+05	1.2256E+05	3.9323E+05	1.0307E+04
4	6.00000	1.0000E+01	1.0000E+06	8.1002E+01	1.4288E+03	7.6226E+05	5.3116E+04	2.4922E+05	4.3242E+03
5	0.00000	1.9145E+01	1.1777E+05	8.0074E+01	8.3947E+02	1.7166E+05	3.0310E+04	1.1387E+05	1.5841E+03
6	1.00000	2.4130E+01	1.1544E+04	8.0742E+01	5.4584E+02	8.0742E+04	1.5361E+04	6.7097E+04	5.8322E+02
7	12.00000	2.7102E+01	1.4216E+04	1.1377E+02	5.9575E+02	7.7004E+04	1.1896E+04	1.5925E+04	3.2898E+02
8	14.00000	3.3888E+01	1.5339E+03	1.4077E+02	5.8211E+02	1.5288E+04	8.3355E+03	4.3854E+03	1.5531E+02
9	15.00000	4.4031E+01	1.5239E+03	2.6645E+02	1.3076E+02	9.4744E+02	6.0319E+03	2.1444E+02	2.1444E+02
10	16.00000	1.4121E+02	3.1148E+03	5.2258E+02	3.9885E+03	7.5377E+03	6.0725E+03	5.4722E+03	4.6731E+02
11	20.00000	5.0007E+02	4.5339E+03	7.9502E+02	4.3059E+03	5.0712E+03	6.4522E+03	7.0021E+03	5.5515E+02
12	22.00000	2.6924E+02	6.7487E+03	1.0220E+03	5.1033E+03	4.1833E+03	7.5318E+03	1.0025E+04	5.5350E+02
13	24.00000	7.7035E+02	9.5515E+03	1.3070E+03	6.5407E+03	7.0796E+03	9.9655E+03	1.2425E+04	5.1935E+02
14	25.00000	1.1974E+02	1.3468E+04	1.4177E+03	1.4022E+04	4.1832E+03	1.4773E+04	1.3819E+04	5.0100E+02
15	26.00000	7.1170E+02	1.3738E+04	1.8933E+03	1.7563E+04	4.8174E+03	2.0576E+04	1.5811E+04	5.0809E+02
16	33.00000	3.0455E+02	6.3113E+04	2.0224E+03	1.5364E+04	5.7387E+03	2.4382E+04	1.1792E+04	5.6378E+02
17	32.00000	1.0545E+03	2.3374E+04	2.0242E+03	1.4822E+04	7.6555E+03	2.4954E+04	5.3362E+03	7.5185E+02
18	33.00000	1.1204E+03	2.3182E+04	2.0303E+03	1.4822E+04	7.6555E+03	2.4954E+04	5.3362E+03	7.5185E+02
19	35.00000	1.0731E+03	7.4435E+04	1.4706E+03	8.4575E+03	9.0562E+03	1.6349E+04	2.9538E+03	8.1493E+02
20	38.00000	3.6620E+02	3.1406E+04	1.4274E+03	4.0018E+03	7.8649E+03	1.2220E+04	1.6243E+03	8.0965E+02
21	40.00000	8.3719E+02	3.7283E+04	8.4945E+02	2.2444E+03	6.8794E+03	9.1305E+03	1.0107E+03	7.2175E+02
22	42.00000	8.0755E+02	2.8600E+04	5.7232E+02	8.0832E+02	5.4173E+03	6.3352E+03	7.3436E+02	5.6727E+02
23	44.00000	3.0223E+02	2.7759E+01	3.9006E+02	2.4606E+02	4.2379E+02	4.9565E+03	5.7338E+02	4.0764E+02
24	46.00000	1.0823E+02	1.3535E+04	2.0533E+02	6.8304E+01	2.0467E+03	3.4369E+03	4.4542E+02	2.7633E+02
25	48.00000	4.9787E+02	1.7471E+04	1.5519E+02	1.8868E+01	7.4765E+03	2.762E+03	3.3779E+02	1.7900E+02
26	50.00000	5.3534E+02	0.7416E+03	1.0970E+02	5.5886E+01	1.6636E+03	1.4510E+03	2.5476E+02	1.1311E+02
27	52.00000	5.5473E+02	6.9472E+07	7.7308E+01	1.6493E+00	1.2948E+03	8.933E+02	1.8745E+02	6.8309E+01
28	54.00000	7.2245E+02	4.2483E+03	5.0584E+01	5.1655E+01	1.0450E+03	5.4336E+02	1.1870E+02	4.4729E+01
29	55.00000	4.6617E+02	3.4377E+03	3.3953E+01	1.4196E+01	8.6042E+02	3.3100E+02	1.0658E+02	2.4463E+01
30	51.00000	3.1703E+02	2.3436E+03	2.2454E+01	4.9149E+01	5.9446E+02	1.3387E+02	7.8393E+01	1.4215E+01
31	51.00000	3.4019E+02	4.5951E+07	1.5349E+01	1.4703E+02	5.4300E+04	1.297E+02	5.7085E+01	8.2257E+00
32	62.00000	7.7148E+02	1.0830E+03	1.1140E+01	4.3407E+03	4.4088E+02	5.8474E+01	3.6218E+01	4.5394E+00
33	50.00000	5.0416E+02	5.0957E+02	8.5222E+00	4.1600E+03	2.6445E+02	2.7081E+01	1.9118E+01	2.4924E+00
34	55.00000	5.6202E+02	7.0037E+02	5.0045E+00	3.7246E+00	2.1385E+02	1.6310E+01	1.8917E+01	1.2686E+00
35	43.00000	6.3235E+02	1.3437E+07	3.4680E+01	1.0209E+04	1.4077E+02	9.7361E+00	1.2706E+01	6.5672E-01
36	70.00000	7.8184E+02	1.4112E+02	2.3300E+00	2.5845E+05	5.6241E+02	4.122E+00	8.5241E+00	3.2671E-01
37	72.00000	3.1956E+02	5.2552E+01	1.5810E+00	6.4202E+06	7.2466E+02	1.8757E+00	5.8338E+00	1.6024E-01
38	74.00000	8.7755E+02	2.6813E+01	1.6745E+00	1.4490E+06	8.3730E+02	8.2680E+01	3.8650E+00	7.7049E-02
39	70.00000	7.1905E+02	1.3138E+01	0.2229E+01	2.7579E+02	8.1743E+02	2.586E+01	1.6171E+00	4.0197E-02
40	73.00000	8.0832E+02	2.8726E+01	6.8420E+01	4.5113E+08	7.1500E+02	7.8212E+02	5.1021E+01	2.2689E-02
41	80.00000	7.2481E+02	7.8039E+02	5.2203E+01	5.0820E+09	5.0712E+02	1.8006E+02	1.3459E+01	1.3686E-02

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K	ALT	MR 03	F01	F12	CMJUL	C0L4	C0LX
1	0.	2.918E-08	1.312E+09	3.615E+10	7.174E+09		4.429E+10
2	100000.	2.004E-08	1.581E+09	2.254E+09	2.734E+09		1.258E+10
3	200000.	2.958E-08	1.239E+09	2.542E+09	2.142E+09		5.126E+09
4	300000.	3.250E-08	1.055E+09	2.000E+09	1.734E+09		3.221E+09
5	400000.	3.767E-08	1.149E+09	1.606E+09	1.408E+09		1.902E+09
6	500000.	5.133E-08	6.521E+08	1.230E+09	1.127E+09		1.279E+09
7	600000.	8.212E-08	3.285E+08	1.001E+09	8.878E+08		1.207E+09
8	700000.	1.133E-07	1.958E+08	8.051E+08	7.833E+08		1.174E+09
9	800000.	1.310E-07	2.335E+08	6.301E+08	4.959E+08		1.248E+09
10	900000.	1.474E-07	1.566E+08	3.750E+08	2.813E+08		1.281E+09
11	2000000.	2.024E-07	3.334E+07	2.379E+08	1.523E+08		1.087E+09
12	3000000.	3.267E-07	4.454E+07	1.303E+08	8.042E+07		1.757E+09
13	4000000.	4.932E-07	2.175E+07	8.051E+07	4.340E+07		1.576E+09
14	5000000.	8.563E-07	8.134E+06	4.373E+07	2.765E+07		1.270E+09
15	6000000.	9.352E-07	2.363E+06	2.193E+07	1.148E+07		1.419E+09
16	7000000.	8.823E-07	5.289E+05	1.025E+07	5.301E+06		7.913E+08
17	8000000.	9.325E-07	9.337E+04	7.497E+06	2.517E+06		6.050E+08
18	9000000.	8.192E-07	1.455E+04	1.800E+06	1.603E+06		4.520E+08
19	35000000.	0.332E-06	2.139E+03	7.817E+05	7.059E+05		3.450E+08
20	33000000.	5.504E-06	2.702E+02	3.235E+05	1.840E+05		2.597E+08
21	40700000.	4.230E-06	4.108E+01	1.142E+05	7.614E+04		1.959E+08
22	40000000.	3.403E-06	9.772E+00	6.387E+04	3.244E+04		1.483E+08
23	40000000.	2.734E-06	1.117E+00	2.998E+04	1.480E+04		1.128E+08
24	40000000.	4.204E-06	1.220E+01	1.452E+04	7.339E+03		8.614E+07
25	49000000.	1.410E-06	3.235E-01	7.739E+03	3.947E+03		6.639E+07
26	59000000.	1.632E-06	1.353E-02	4.275E+03	2.312E+03		5.194E+07
27	32000000.	1.533E-06	7.323E-03	2.702E+03	1.459E+03		4.076E+07
28	30000000.	1.243E-06	1.267E-03	1.405E+03	9.607E+02		3.219E+07
29	30000000.	1.047E-06	4.378E-04	8.459E+02	6.692E+02		2.536E+07
30	30000000.	8.068E-07	1.544E-04	5.974E+02	4.744E+02		1.930E+07
31	63000000.	7.705E-07	6.305E-05	3.254E+02	3.639E+02		1.563E+07
32	62000000.	7.188E-07	2.798E-05	2.137E+02	2.545E+02		1.237E+07
33	64000000.	7.094E-07	1.268E-05	1.399E+02	1.951E+02		9.666E+06
34	60000000.	5.343E-07	2.152E-06	8.316E+01	1.425E+02		7.519E+06
35	64000000.	4.028E-07	7.107E-06	6.245E+01	1.071E+02		5.827E+06
36	73000000.	4.920E-07	1.521E-06	4.344E+01	7.958E+01		4.436E+06
37	72000000.	7.907E-07	3.305E-07	3.014E+01	2.907E+01		3.360E+06
38	74000000.	3.631E-07	5.144E-07	2.100E+01	1.656E+01		2.521E+06
39	75000000.	3.862E-07	2.944E-07	1.477E+01	7.198E+00		1.872E+06
40	74000000.	7.202E-07	1.757E-07	1.150E+01	2.325E+00		1.175E+06
41	80000000.	4.530E-07	1.355E-07	7.247E+00	1.671E+00		9.973E+05

K	ALT	N20	NOX	CH4
1	0.	5.067E+12	1.07E+10	3.616E+17
2	20000.	5.267E+12	2.174E+10	3.127E+17
3	40000.	4.124E+12	3.781E+09	4.4321E+13
4	60000.	3.167E+12	1.820E+09	1.265E+13
5	80000.	2.714E+12	1.46E+09	1.592E+13
6	100000.	2.175E+12	1.328E+09	1.674E+13
7	120000.	1.710E+12	2.289E+13	1.0049E+13
8	140000.	1.465E+12	2.273E+09	8.534E+12
9	150000.	3.916E+11	4.769E+09	5.863E+12
10	160000.	5.272E+11	3.120E+09	3.692E+12
11	200000.	4.012E+11	1.315E+09	2.395E+12
12	240000.	2.528E+11	1.213E+10	1.535E+12
13	280000.	1.552E+11	1.153E+10	9.847E+11
14	320000.	3.283E+10	1.230E+10	6.136E+11
15	360000.	5.314E+10	3.567E+09	7.8501E+11
16	400000.	2.922E+10	7.180E+09	2.330E+11
17	450000.	1.557E+10	7.99E+09	1.4407E+11
18	500000.	8.111E+09	4.385E+09	6.296E+10
19	550000.	4.213E+09	7.280E+09	4.823E+10
20	600000.	2.615E+09	1.75E+09	2.785E+10
21	650000.	1.189E+09	1.756E+09	1.020E+10
22	700000.	6.572E+08	1.319E+09	9.650E+09
23	750000.	3.754E+08	1.570E+08	5.038E+09
24	800000.	2.248E+08	2.342E+08	3.851E+09
25	850000.	1.365E+08	5.146E+08	2.622E+09
26	900000.	8.797E+07	3.207E+08	1.873E+09
27	950000.	5.767E+07	2.794E+08	1.332E+09
28	1000000.	3.033E+07	2.363E+08	1.054E+09
29	1050000.	2.796E+07	1.576E+08	8.069E+08
30	1100000.	1.916E+07	1.524E+08	6.361E+08
31	1150000.	1.365E+07	7.950E+07	4.847E+08
32	1200000.	3.948E+06	5.342E+07	3.627E+08
33	1250000.	7.297E+06	7.376E+07	2.963E+08
34	1300000.	8.381E+06	6.753E+07	2.300E+08
35	1350000.	3.569E+06	1.608E+07	1.779E+08
36	1400000.	2.906E+06	1.278E+07	1.353E+08
37	1450000.	2.131E+06	7.817E+06	1.024E+08
38	1500000.	1.572E+06	1.868E+06	7.689E+07
39	1550000.	1.130E+06	2.307E+06	5.704E+07
40	1600000.	8.152E+05	1.661E+06	4.282E+07
41	1650000.	5.527E+05	3.171E+05	3.036E+07

NORMAL FOR LND.